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**Numerical Methods for Determining  
Streamlines and Isopressures  
for Use in Fluid-Flow Studies**



**UNITED STATES DEPARTMENT OF THE INTERIOR**

Report of Investigations 7621

**Numerical Methods for Determining  
Streamlines and Isopressures  
for Use in Fluid-Flow Studies**

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## CONTENTS

	<u>Page</u>
Abstract.....	1
Introduction.....	1
Isopressures.....	3
General procedure.....	3
Location of successive points.....	4
Vector models.....	13
Lookup and computation procedure.....	15
Streamlines.....	17
Orthogonality.....	17
Computer solution for streamline intersection.....	19
MAIN program, subroutines, and operating details.....	20
MAIN program and data preparation.....	20
Locating index on isopressure line--subroutine LOCATE.....	25
Circle equation between isopressure points--subroutine QUAD...	32
Irregular, discontinuous, and extreme conditions-- subroutine BOUND.....	33
Input data and results.....	36
Concluding statement.....	52
References.....	53
Appendix A.--Nomenclature for isopressure program.....	54
Appendix B.--Nomenclature for streamline program.....	57

## ILLUSTRATIONS

1. Schematics for solution of polynomial constants.....	4
2. Schematic flow diagram for isopressure MAIN program.....	8
3. Schematics for vector models.....	13
4. Schematic flow diagram for subroutine LOOKUP.....	16
5. Schematics for intersection of orthogonal lines.....	18
6. Schematic flow diagram for streamline MAIN program.....	23
7. Schematic flow diagram for subroutine LOCATE.....	27
8. Schematic flow diagram for subroutine STRM.....	31
9. Calculated isopressure lines and streamlines for 7-spot element.....	35

## TABLES

1. Isopressure MAIN program with explanatory comments.....	5
2. Indexes for vector models used in lookup for isopressures.....	14
3. Block data subprogram containing vector-model and other built-in data.....	15
4. Program for subroutine LOOKUP with explanatory comments.....	15
5. Program for subroutine POLCON with explanatory comments.....	17
6. Streamline MAIN program with explanatory comments.....	21
7. Program for subroutine LOCATE with explanatory comments.....	26
8. Program for subroutine STRM with explanatory comments.....	28
9. Program for subroutine QUAD with explanatory comments.....	33

## TABLES--Continued

	<u>Page</u>
10. Program for subroutine BOUND with explanatory comments.....	34
11. Listings of function subprograms used in subroutine STRM.....	37
12. Pressure input data for isopressure program.....	38
13. Input data for streamline program.....	43
14. Streamline coordinates calculated by stream program.....	50

# NUMERICAL METHODS FOR DETERMINING STREAMLINES AND ISOPRESSURES FOR USE IN FLUID-FLOW STUDIES

by

R. V. Higgins<sup>1</sup> and A. J. Leighton<sup>2</sup>

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## ABSTRACT

A numerical method is presented to calculate the isopressure (isobar) lines and streamlines for an oilfield from the pressure distribution. A knowledge of these lines is useful in the study of the flow of fluids in underground reservoirs, especially for those containing gaseous and/or liquid hydrocarbons. This work was done primarily to enable determination of the shape factors needed in the calculation of petroleum reservoir performance. However, it has application for the flow of water in aquifers, or electricity or heat in odd-shaped geometry.

Techniques previously developed were used to calculate the pressure distribution. From this pressure distribution, the isopressure lines were calculated accurately by the method presented in this paper. Then by successively projecting orthogonal lines from one isopressure line to another, the streamlines are determined. From the coordinates of the isopressures and the streamlines, the shape factors can then be determined by a published method.

Computer methods are presented to calculate the streamlines and isopressures for any well-spacing pattern existing within a field with multiple wells. The method reproduces the flow net for several well configurations having extensive geometrical variations. Such information provides the petroleum engineer with data from which he can compute oil recoveries for different patterns and thereby maximize the recovery of hydrocarbons from the reservoir.

## INTRODUCTION

The use of isopressures<sup>3</sup> and streamlines in flow of fluids and electricity has been most useful in the past. These lines have been determined either by sophisticated mathematical methods for uniform patterns or by

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<sup>1</sup>Research supervisor.

<sup>2</sup>Petroleum engineer.

<sup>3</sup>In this report the term "isopressure" refers to a line or contour marking locations in a reservoir having the same pressure and is used synonymously with "isobar."

electrical techniques for uniform or nonuniform configuration. In oilfields the patterns often are not symmetrical, and the numerical method presented here is most useful. However, the main interest with this paper is primarily in the development of the lines to determine shape factors (geometric resistivity).

The authors (3)<sup>4</sup> have previously shown by their method, which uses shape factors, that one may determine quickly the waterflood potential of a normal pattern flood. The shape factors for several normal patterns have been published (1). In a field, often the patterns differ from the normal. There is no convenient published way to put in the parameters and end up with isopressures, streamlines, and the shape factor values for nonnormal patterns. This paper will accomplish the calculation of isopressures and streamlines for use in reservoir studies.

The isopressures and the streamlines, even without the shape factors, are usable information to guide the reservoir engineer about future drilling as related to poorly drained areas. With the use of the shape factors and the authors' (3) previously published methods, much more quantitative information can be obtained to guide the operator.

The winning of more oil from reservoirs should be aided by the information contained in the report. This Report of Investigations also will enable the Bureau of Mines Higgins-Leighton method to be expanded to include more reservoir configurations. This should aid in deciding the best locations of in-filled wells so as to maximize recovery of oil from the Nation's reserves.

A CDC 6600<sup>5</sup> was used in making the calculations. This size computer was used because of the access convenience. Since the storage required for the programs presented is not excessive, smaller computers can be used. FORTRAN IV was used to program the instructions.

An early search of the literature did not disclose a convenient method to determine streamlines of nonsymmetrical patterns. Muskat (8), Hurst (6), and Prats (9) have presented methods to determine streamlines for patterns that are symmetrical. Even for them, the mathematics used are more for scientists than petroleum engineers, and the working details are not published. The method presented here will determine the streamlines for any pattern, symmetrical or nonsymmetrical. Every engineer has been instructed some time or another in the mathematics used. Much ingenuity is required in getting all the components together and instructing the computer through a program to process the complex logic. After the method was developed but before the manuscript was completed, Le Blanc and Caudle (7) published a method based on the mathematics of potential flow. Their method has a different approach. The authors of this paper have not thoroughly investigated the merits of the

---

<sup>4</sup>Underlined numbers in parentheses refer to items in the list of references preceding the appendixes.

<sup>5</sup>Reference to specific makes of equipment is for identification only and does not imply endorsement by the Bureau of Mines.

two methods, since the one presented here was satisfactory. Also, the results are directly usable in this Bureau of Mines series of reservoir calculation methods.

## ISOPRESSURES

### General Procedure

In the determination of the coordinates of an isopressure line, the line is started at a point of known pressure on an edge and projected stepwise throughout the field. In the iterative technique (5) used to determine the input pressure distribution, the pressures are calculated at the coordinates of a grid. The stepwise determination of each point for an isopressure contour proceeds as follows: (1) The line is extended into the pattern by means of vector models to determine direction and lookup statements to locate the next point in relation to the grid, (2) the constants of a second-order polynomial equation passing through the pressure points are calculated, and (3) then the coordinates of a point on the isopressure contour are determined by solving the equation. A third-order polynomial equation was also tried, but it did not improve the fit.

The usual procedure for calculating the constants of a second-order polynomial equation is by the use of simultaneous equations. To reduce the computer time, the constants were determined by short formulas. This was possible since the distance between any adjacent grid points is the same and was assumed to be 1.0. This equal distance is a carryover from the iterative technique (5) of determining the pressure distribution. The origin for the coordinates for the polynomial equation representing the pressure relationship to geometry was at the grid point in question. This is illustrated in figure 1. The equation for interpolating is  $P = a_1 + a_2x + a_3x^2$ .

When  $x = 0.0$ ,

$$P_2 = a_1; \quad (1)$$

when  $x = 1$ ,

$$P_3 = P_2 + a_2 + a_3; \quad (2)$$

and when  $x = -1$ ,

$$P_1 = P_2 - a_2 + a_3. \quad (3)$$

Eliminating  $a_2$  from equations 2 and 3,

$$a_3 = \frac{P_3 + P_1}{2} - P_2. \quad (4)$$

Eliminating  $a_3$  from equations 2 and 3,

$$a_2 = \frac{P_3 - P_1}{2}. \quad (5)$$

Thus the constants,  $a_1$ ,  $a_2$ , and  $a_3$ , for the second-order polynomial used to interpolate for the isopressures are easily obtained by use of equations 1, 4, and 5.

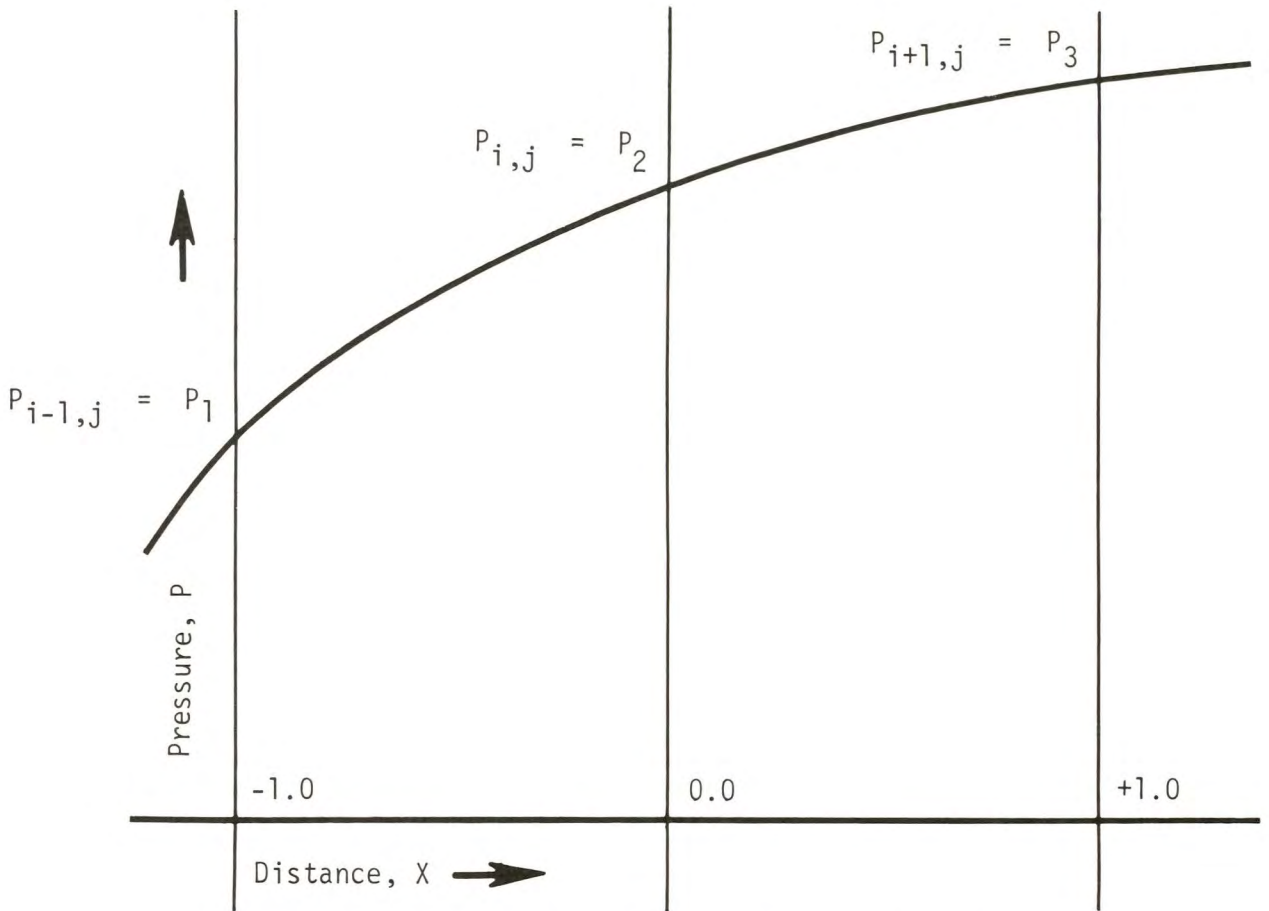


FIGURE 1. - Schematics for Solution of Polynomial Constants.

The pressures for this report were calculated at uniform grid points. This permitted the use of a polynomial for which the constants could be solved without the use of a quadratic equation and the test for the correct plus or minus value. Also, the quadratic occasionally results in sinusoid values between the intermediate points. If a nonuniform grid were used, a quadratic solution for the constants would be required for the solution for the constants for the polynomial.

#### Location of Successive Points

The program is written so as to advance the calculations for an isopressure line, one grid position at a time. The grid points, between which the isopressure values lie, are located by sets of vector models and a lookup subroutine. The FORTRAN statements for the MAIN program are listed with explanatory comments in table 1 and the flow diagram is shown in figure 2.

TABLE 1. - Isopressure MAIN program with explanatory comments

```

C   MAIN PROGRAM FOR ISOPRESSURE CALCULATION.

    DIMENSION Y(101), X(101), XSAVE(101), YSAVE(101)
    INTEGER XUP, YUP, TEST(101,101)
    COMMON/AQUI/ P(101,101), XUP, YUP, NWELL, IADD(4,5), IPLUS(4,5,4),
1 ICALL(5,4), WORD(10)
    LOGICAL FIT, FORK

C   INITIALIZATION AND ROUTING TO START A PRESSURE LINE.
    READ 1030, ((P(I, J), J = 1, YUP), I = 1, XUP)
1030 FORMAT ( 12F6.2 )
    PRINT 1031, ((P(I, J), I = 1, XUP), J = 1, YUP)
1031 FORMAT ( 2(20F6.2/), 13F6.2 )
    DO 10 I = 1, XUP
    DO 10 J = 1, YUP
10 TEST(I, J) = 0
    Sets Test(I,J) to zero. After coordinates of an isopressure point are determined,
    coordinates of the nearest grid point are recorded so as to avoid duplication or
    excessive isopressure density.

12 DO 700 KK= 1, 5
    PRINT 4000, (( TEST(IN, JN), IN = 1, XUP), JN = 1, YUP )
4000 FORMAT ( 1H1 ( / 53I2 ) )
    PRINT 1050, WORD(KK)
1050 FORMAT ( 1H1 50X, A10 )
    GO TO ( 20, 20, 30, 30, 15 ), KK
    Print label for the edge or infill at which a group of isopressure lines
    start.
    Routing to go where the initializations are made according to the one
    of the four edges or the sweep of entire pattern for missing values. 1/

15 I = XUP
    J = YUP
16 I = I - 1
18 J = J - 1
    IGO = 1
    IF ( TEST( I, J) .EQ. 1) GO TO 650
    ITAL = 1
    NEND = 1
    GO TO 40
    Start infill at a corner.
    Move to left one column.
    Move up one row.
    Routing index for first part of an infill line.
    If an isopressure line is near point I,J, bypass calculation.

20 NEND = YUP - 1
    GO TO 40
    One less than highest y value because top or bottom edge values will be used later for starting isopressure values.

30 NEND = XUP - 1
40 DO 700 LID = 1, NEND
    IF ( KK.EQ.5 ) GO TO 80
    ITAL = 1
    GO TO ( 60, 60, 70, 70 ), KK
    Set tally for isopressure points to 1.
    Routing according to edge used.

60 J = YUP - LID
    IF ( KK.EQ.1 ) I = XUP
    IF ( KK.EQ.2 ) I = 1
    GO TO 80
    Starts at index reduced by one because first value for an isopressure line is the pressure at the
    edge; starts at bottom right at one less than the highest y index. When KK=1, starts at right
    edge; when KK=2, starts at left edge.

70 I = XUP - LID
    IF ( KK.EQ.3 ) J = 1
    IF ( KK.EQ.4 ) J = YUP
80 IF ( TEST(I, J).EQ.1 ) GO TO 700
    AVP = P(I, J)
    Y(ITAL) = J
    X(ITAL) = I
    TEST(I, J) = 1
    I reduced by 1 to move over to next left column.
    When KK = 3, the isopressure starts at the top edge and proceeds downward.
    When KK = 4, the isopressure starts at the bottom edge and proceeds upward.
    If the isopressure value is near a previously calculated one, Go to 700 to bypass calculation.
    Sets pressure value for line.
    Y coordinate for an isopressure point.
    X coordinate for an isopressure point.
    Shows that an isopressure line is at or near this grid point.

```

1/ When KK = 1, right edge; 2, left edge; 3, top; 4, bottom; and 5, sweep internal area for infill of sparse regions.

TABLE 1. - Isopressure MAIN program with explanatory comments--Continued

<p>C    CALCULATIONS TO EXTEND PRESSURE LINE.</p> <p>100   DO 500 K = 1, 100              IM = X(ITAL) + 0.5              JM = Y(ITAL) + 0.5              IF (ITAL .GT. 1) GO TO 200              IB = IM + IADD(1, KK)              IE = IM + IADD(2, KK)              JB = JM + IADD(3, KK)              JE = JM + IADD(4, KK)              GO TO ( 360, 360, 430, 430, 360 ), KK</p> <p>200   IF ( (X(ITAL) - X(ITAL-1)) .GE. 0.0 .AND. (Y(ITAL-1) - Y(ITAL))              1 .GE. 0.0)    L = 1              IF ((X(ITAL) - X(ITAL-1)) .LE. 0.0 .AND. (Y(ITAL-1) - Y(ITAL))              1 .GE. 0.0)    L = 2              IF ( (X(ITAL) - X(ITAL-1)) .LE. 0.0 .AND. (Y(ITAL-1) - Y(ITAL))              1 .LE. 0.0)    L = 3              IF ( (X(ITAL) - X(ITAL-1)) .GE. 0.0 .AND. (Y(ITAL-1) - Y(ITAL))              1 .LE. 0.0)    L = 4</p> <p>      DO 300 M = 1, 5              IB = IM + IPLUS(1, M, L)              IE = IM + IPLUS(2, M, L)              JB = JM + IPLUS(3, M, L)              JE = JM + IPLUS(4, M, L)              IF (ICALL(M, L) .EQ. 2) GO TO 260              FORK = .TRUE.              CALL       LOOKUP (IB, IE, JB, JE, IP3, AVP, IT, JT, TEST, FIT, FORK)              IF (FIT) GO TO 480              GO TO 300              FORK = .FALSE.              CALL       LOOKUP (IB, IE, JB, JE, JP3, AVP, IT, JT, TEST, FIT, FORK)              IF (FIT) GO TO 380              CONTINUE              GO TO 510              FORK = .FALSE.              CALL       LOOKUP (IB, IE, JB, JE, JP3, AVP, IT, JT, TEST, FIT, FORK)              IF ( .NOT.FIT ) GO TO 510              CALL POLCON ( P(IT, JP3-2), P(IT, JP3-1), P(IT, JP3), AVP, YY )              ITAL = ITAL + 1              X ( ITAL ) = IT              Y ( ITAL ) = YY + FLOAT(JP3-1)              IF ( YY.LE.0.5 ) TEST(IT, JP3-1) = 1              IF ( YY.GT.0.5 ) TEST(IT, JP3) = 1              IF ( IT.LE.1.OR.IT.GE.XUP .OR. Y(ITAL).LE.1..OR.Y(ITAL).GE.              * FLOAT(YUP ) ) GO TO 510              GO TO 500              FORK = .TRUE.              CALL       LOOKUP (IB, IE, JB, JE, IP3, AVP, IT, JT, TEST, FIT, FORK)              IF ( .NOT.FIT ) GO TO 510</p>	<p>DO statement to extend isopressure line.          Nearest grid point.          Nearest grid point.          Bypass initializations.          Set indexes at edge for initial lookup. The IADD values give the starting and ending x's for the x range.          Provides the y range for the first lookup.</p> <p>The following calculations are to continue isopressure line already started.</p> <p>L = 1    Up and to the right.          L = 2    Up to the left.          L = 3    Down and to left.          L = 4    Down and to right.</p> <p>Picks various grid lines according to value of L which denotes the direction a pressure vector is moving. Without these, the lookup could reverse the direction.</p> <p>Test if the lookup is to be on an x or y coordinate.          Provides for lookup on x coordinate.          If true, a successful lookup on a x coordinate.          Continued looking.</p> <p>Provides for lookup on y coordinate.          If true, a successful lookup on a y ordinate.</p> <p>The following calculations are for the initiation of an isopressure line.          Initial lookup on y coordinate.          If lookup unsuccessful, terminate and go to routing for a new line.          Interpolate on y line.          Advance ITAL count.          X coordinate lies on an x line.          Interpolated value plus the base is the y coordinate.          Nearest y ordinate of the grid has a isopressure value.          If coordinates of isopressure lie outside the grid, go to 510 to terminate line.          To advance the isopressure line.</p> <p>Initial lookup on an x line.</p>	
--	--	--

TABLE 1. - Isopressure MAIN program with explanatory comments--Continued

```

480 CALL POLCON ( P(IP3-2,JT), P(IP3-1,JT), P(IP3,JT), AVP, XX )      Interpolate on x.
    ITAL = ITAL +1
    Y(ITAL) = JT
    X(ITAL) = XX + FLOAT (IP3-1)
    IF ( XX.LE.0.5 ) TEST(IP3-1,JT) = 1
    IF ( XX.GT.0.5 ) TEST(IP3,JT) = 1
    IF ( X(ITAL).LE.1..OR.X(ITAL).GE.FLOAT(XUP) .OR. JT.LE.1.OR.
* JT.GE.(YUP ) ) GO TO 510
    Y ordinate of isopressure point.
    Interpolated value plus base is the x coordinate.
    The nearest grid point has an isopressure point already determined nearby.
500 CONTINUE
    If coordinates of isopressure lie outside the grid go to 510 to terminate.
    Return to test for extended isopressure coordinates.

C   ROUTING AND DATA MANIPULATION TO COMPLETE INFILL LINES.
510 IF ( ITAL.LT.2 ) GO TO 600
    IF ( KK.NE.5 ) GO TO 590
    GO TO ( 520, 550 ), IGO
    If only the starting isopressure value, to to 600.
    If not the last sweep, go to 590 for a printing of coordinates.
    Routing to process first or second section of infill line.
520 IGO = 2
    ITTAL = ITAL
    DO 530 IN = 1, ITTAL
    XSAVE(IN) = X(IN)
    YSAVE(IN) = Y(IN)
    Reindexes coordinates of first section of isopressure line.
530 X(1) = XSAVE(2)
    Y(1) = YSAVE(2)
    X(2) = XSAVE(1)
    Y(2) = YSAVE(1)
    Reverses coordinates.
    ITAL = 2
    GO TO 100
550 ITALM2 = ITAL - 2
    DO 560 IN = 1, ITALM2
    XSAVE(ITTAL+IN) = X(ITAL-IN+1)
    YSAVE(ITTAL+IN) = Y(ITAL-IN+1)
    Reindexes coordinates of second section of isopressure line.
560 ITAL = ITALM2 + ITTAL
    DO 580 IN = 1, ITAL
    LN = IN - (ITAL-ITTAL)
    IF ( LN.LE.0 ) LN = IN + ITTAL
    X(IN) = XSAVE(LN)
    Y(IN) = YSAVE(LN)
    Total number equals sum of first and second sections.
    Final indexing for all points in isopressure line.
580 Y(IN) = YSAVE(LN)

C   OUTPUT COORDINATES OF PRESSURE LINE AND ROUTING TO NEXT SITUATION.
590 PRINT 2000, AVP, ITAL, X(1), Y(1), X(ITAL), Y(ITAL)
2000 FORMAT ( / F15.5, I8, 2(5X, 2F10.3 ) )
C   PUNCH 2000, AVP, ITAL, X(1), Y(1), X(ITAL), Y(ITAL)
    PRINT 2001, (X(N), Y(N), N = 1, ITAL )
    Identification card for isopressure line.
2001 FORMAT ( 10F10.3 )
C   PUNCH 2002, (X(N), Y(N), N = 1, ITAL )
2002 FORMAT ( 8F10.3 )
C   PUNCH 2000
    IF ( KK.EQ.5 .AND. I.EQ.1.AND.J.EQ.1 )
    IPRINT 4000, (( TEST(IN, JN), IN = 1, XUP), JN = 1, YUP )
    At end of calculation, all test values should equal 1.
600 GO TO ( 700, 700, 700, 700, 650 ), KK
650 CONTINUE
    IF ( J.GT.1 ) GO TO 18
    J = YUP + 1
    IF ( I.GT.1 ) GO TO 16
    Routing for sweep on infill.
700 CONTINUE
    STOP
    END

```



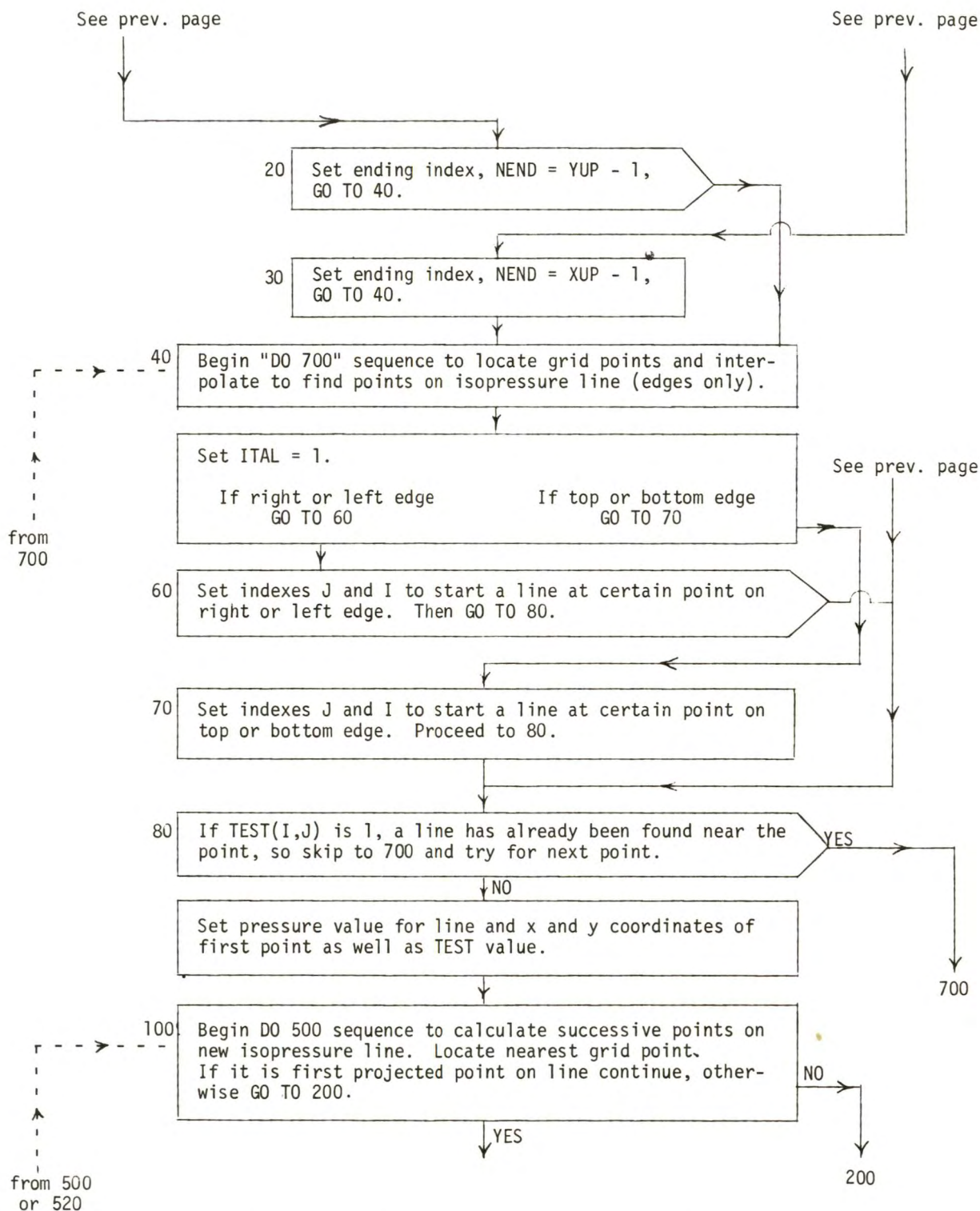


FIGURE 2. - Schematic Flow Diagram for Isopressure MAIN Program.—Continued

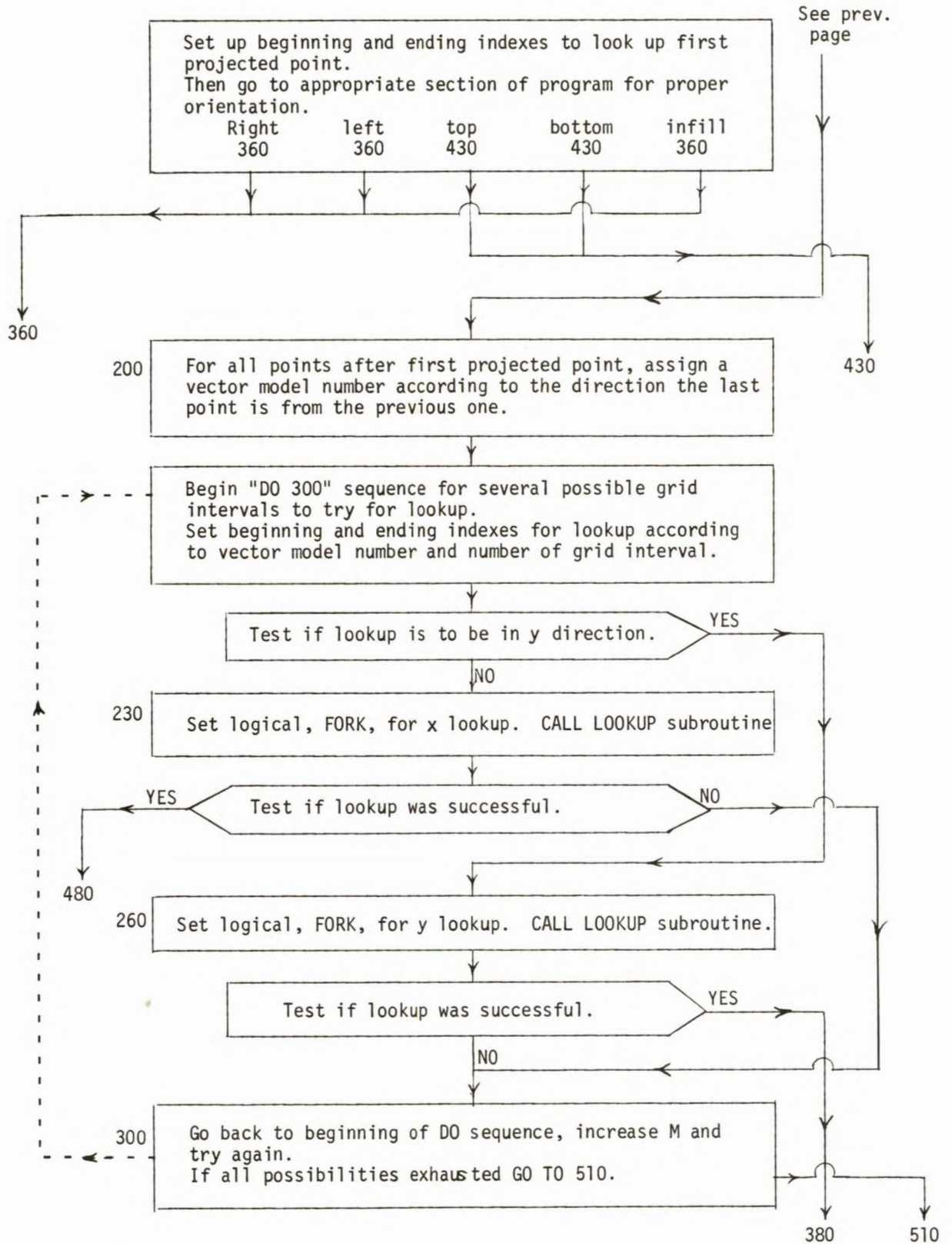


FIGURE 2. - Schematic Flow Diagram for Isopressure MAIN Program.-Continued

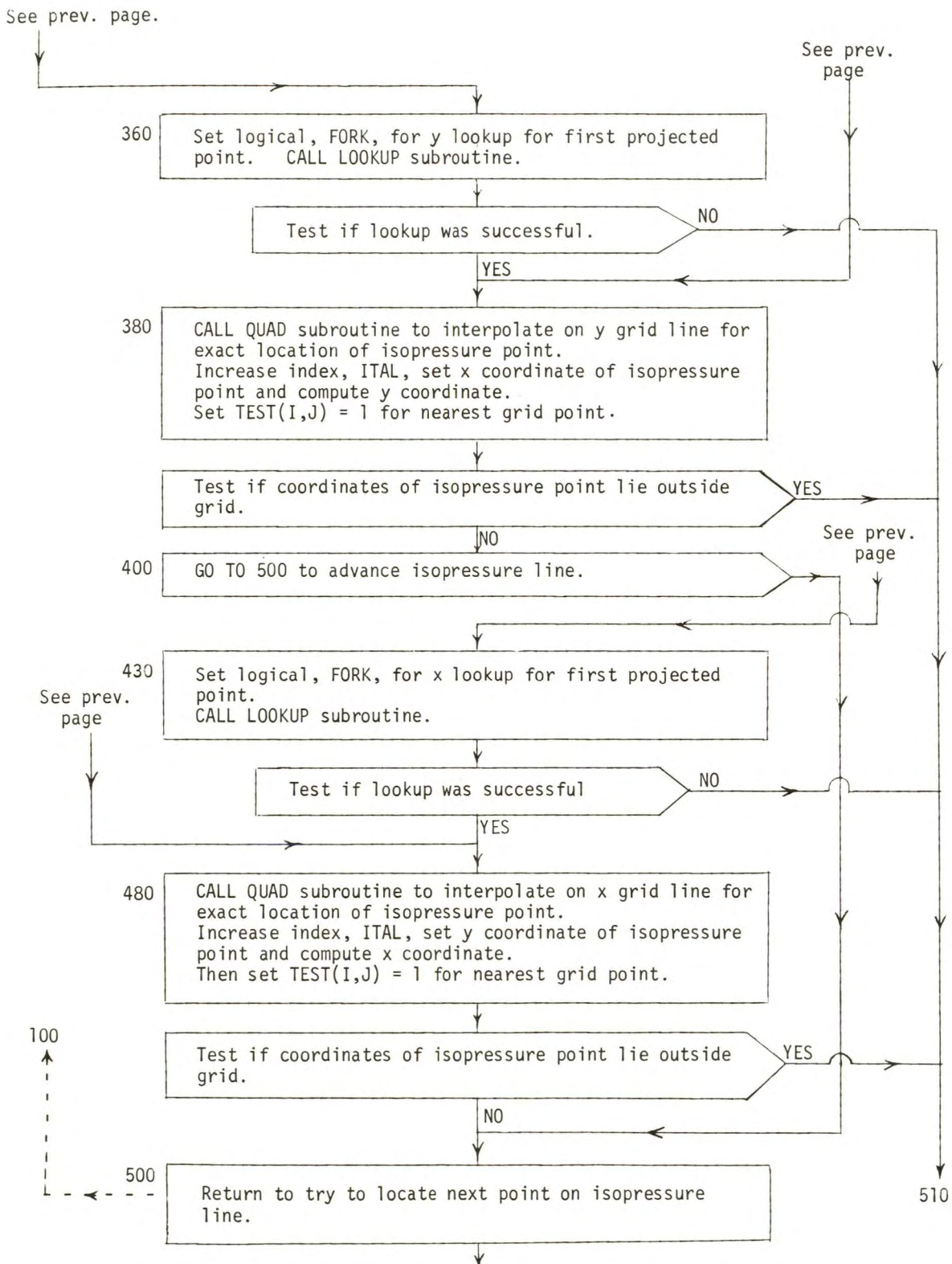


FIGURE 2. - Schematic Flow Diagram for Isopressure MAIN Program.—Continued

See prev. page

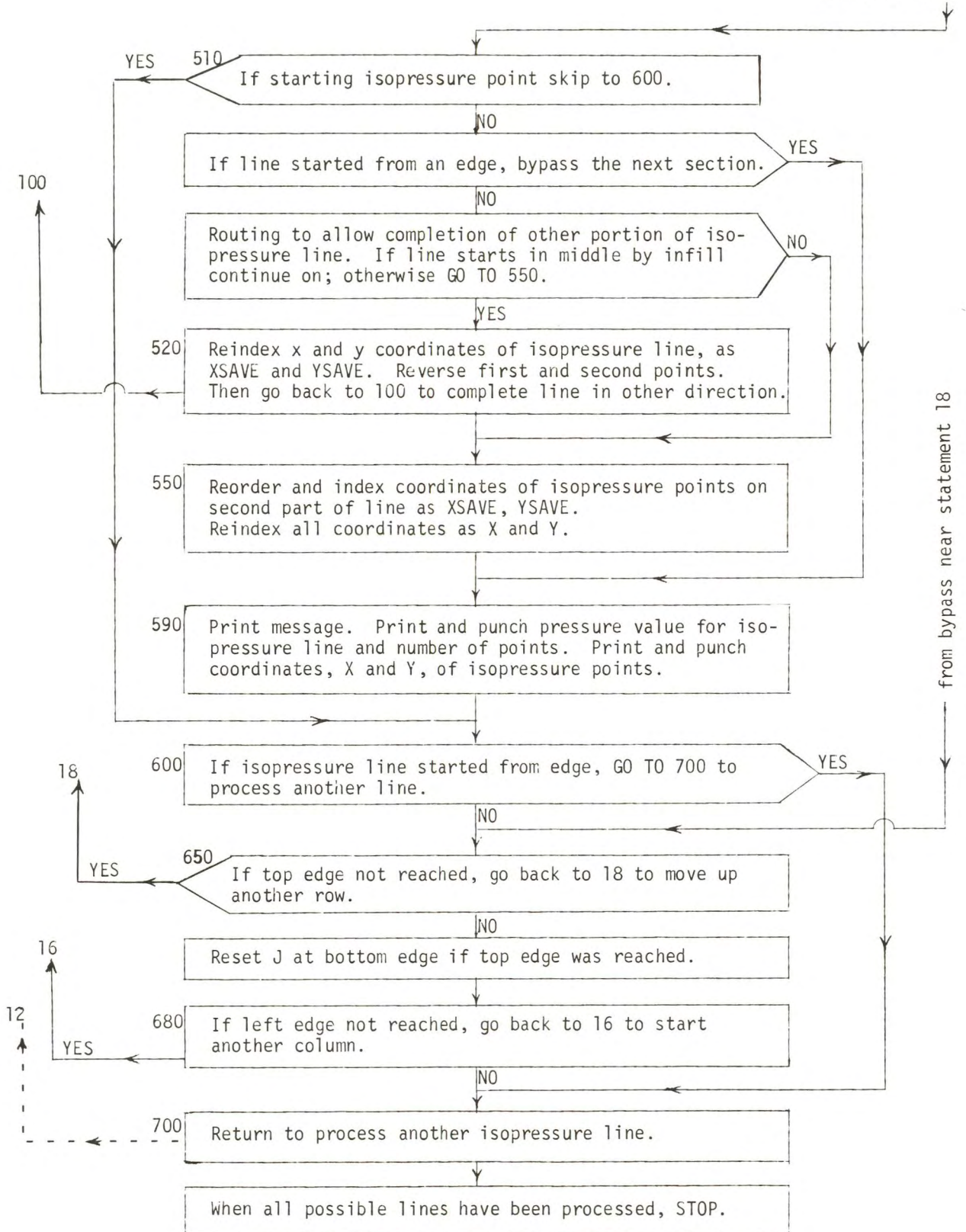


FIGURE 2. - Schematic Flow Diagram for Isopressure MAIN Program.—Continued

Vector Models

Experience has shown that the succeeding isopressure point may lie as many as three grid points away from the last one, or the line may start curving backwards. These types of locations complicate the computer logic. As a result, four vector models are used to find the proper direction. These

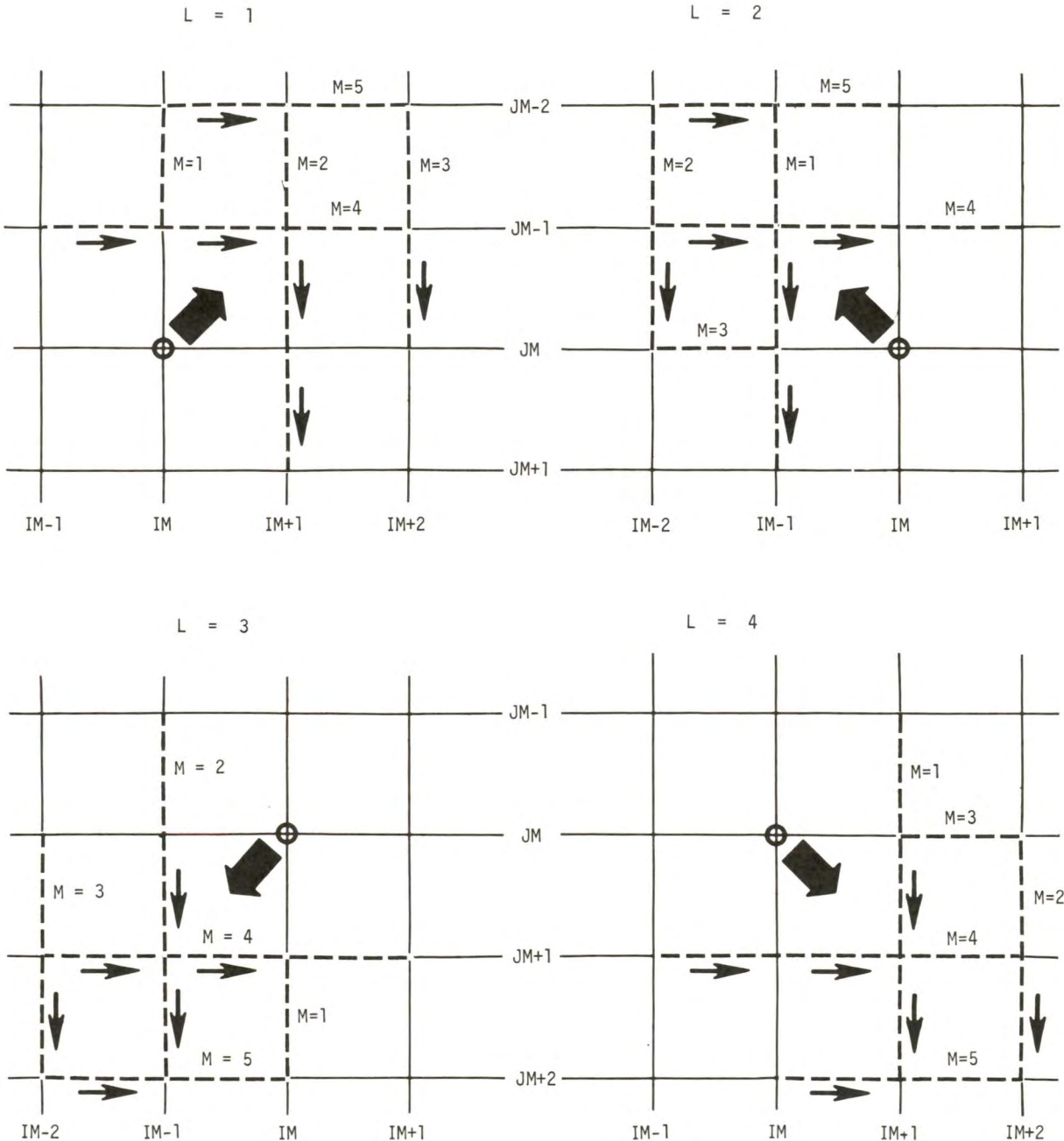


FIGURE 3. - Schematics for Vector Models.

models depend upon the direction the last isopressure is advancing; that is, up, down, right, or left. Also, the models have been designed so as to avoid locating an isopressure point that would start the line going backward. The models so chosen have worked satisfactorily for all the pressure grids that the authors have tested.

The choice of vector model is made by four computer statements beginning at 200 in the program. These tests determine the direction in which the last calculated isopressure line segment is moving. The assumption is that the lookup for pressures between which the isopressure lies will continue to be in a forward direction. Nevertheless, enough pressures at grid points are included in the model for an extensive range of angles, except in the reverse direction. Experience has shown that this is necessary.

After the direction has been determined by the computer test, the model index number is assigned to L. With this value of L, the DO 300 M = 1,5 etc.-sequence picks the grid lines and ranges of lookup on the grids.

The models are shown in figure 3 for the indexes of L and M. The large arrow shows the model direction. The dash lines are the portions of the grid asked for by the indexes and the small arrows denote the extended range built into the lookup subroutine. The values of indexes L and M are in the COMMON statement and are listed in table 2. The BLOCK DATA subprogram listed in table 3 contains the same data in a form usable by the computer. As can be seen in figure 3, no lookup is requested in the reverse direction.

TABLE 2. - Indexes for vector models used in lookup for isopressures

A IPLUS values that designate the grid points					Model No. L
Grid point selection, M					
1	2	3	4	5	
		PLUS			
0 0-1-1 -1-1-1 1	1 1-1 1 -2-2-1 0	2 2-1 0 -2-2 0 0	-1 1-1-1 -2 0-1-1	0 1-2-2 -2-1-2-2	1 2
0 0 2 2 1 1 0 2	-1-1 0 2 2 2 1 2	-2-2 1 2 1 1 0 0	-2 0 1 1 -1 1 1 1	-2-1 2 2 0 1 2 2	3 4

B ICALL values that designate the X or Y coordinate selected for lookup					Model No. L
1	2	3	4	Model Section, M	
1 2 3 4 5	1 2 3 4 5	1 2 3 4 5	1 2 3 4 5	X or Y, ICALL <sup>1</sup>	
2 2 2 1 1	2 2 1 1 1	2 2 2 1 1	2 2 1 1 1		

<sup>1</sup>When the index is 1, the lookup is on the X coordinate; when 2, the Y coordinate.



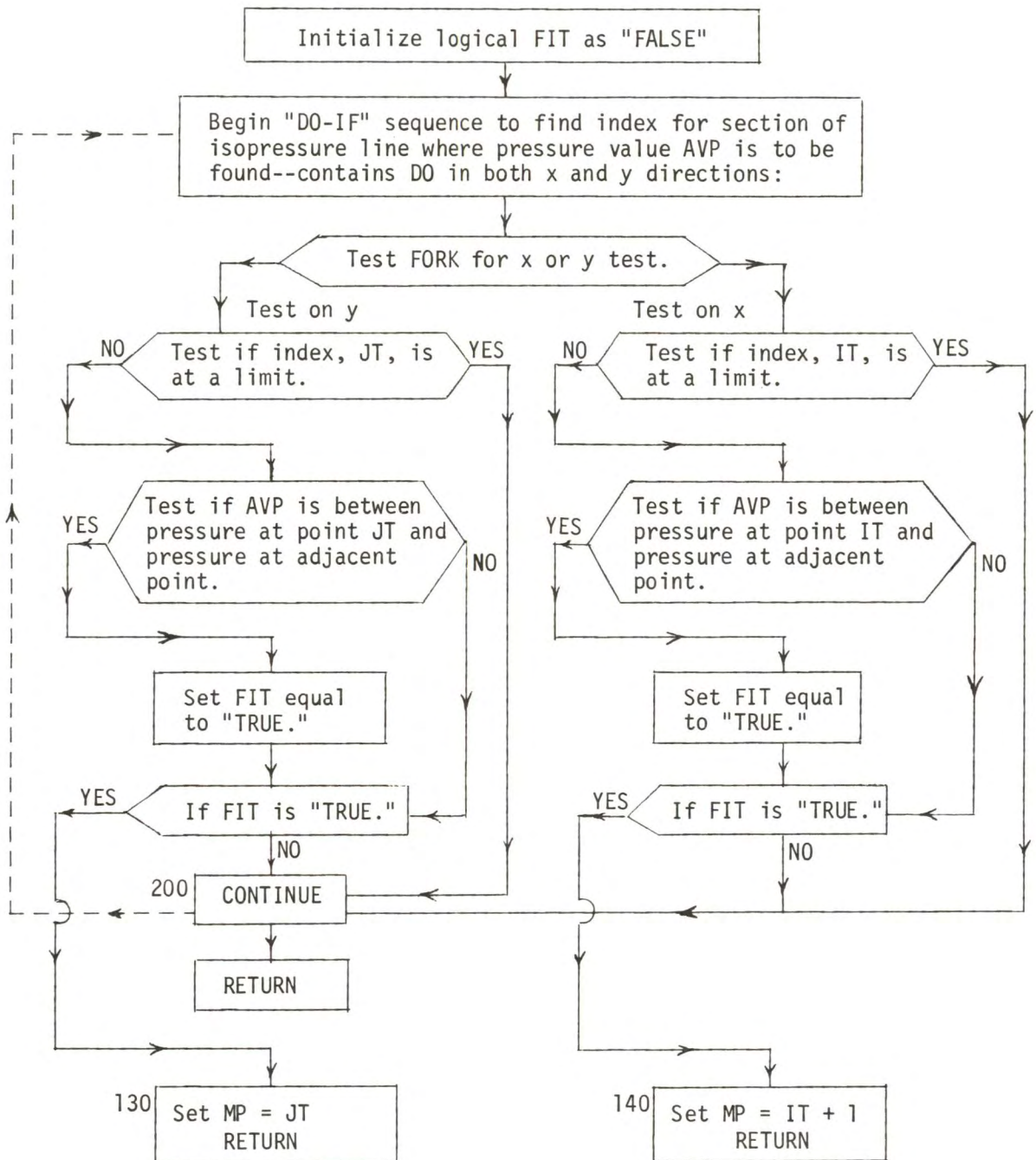


FIGURE 4. - Schematic Flow Diagram for Subroutine LOOKUP.

POLCON, listed in table 5, solves for the constants of the polynomial, then solves for the location in the grid where the isopressure value intersects. The exact coordinate value is then computed. The coordinate value in the

opposite direction is that for the intersected grid line. These values are indexed and stored for subsequent output.

TABLE 5. - Program for subroutine POLCON with explanatory comments

```

SUBROUTINE POLCON ( P1, P2, P3, AVP, YY )

  A = (P3 + P1) / 2.0 - P2
  B = (P3 - P1) / 2.0
  C = P2 - AVP
  IF ( P2.EQ.P3 ) GO TO 90
  IF ( ABS(A).LE.0.0000001 ) GO TO 80

  D = B**2 - 4.0* A*C
  PP = -B/(2.0*A)
  Q = SQRT (ABS(D))/(2.0*A)
  R1 = PP+Q
  R2 = PP-Q
  BPOR = (AVP-P2) / (P3-P2)
  DR1 = ABS (BPOR -R1)
  DR2 = ABS (BPOR -R2)
  IF (DR1 .LE. DR2 ) YY =R1
  IF (DR2 .LT. DR1) YY= R2
  RETURN

80 YY = - C / B
  RETURN

90 YY = 0.
  RETURN

END

```

Calculates constants of quadratic equation.

Function is zero.  
Function is linear.

Roots of quadratic equation.

Determines which root is correct.

Function is linear.

Function is zero.

Isopressure lines are computed starting from all four edges of the network according to the value of control index KK (KK = 1 through KK = 4). To fill in possible sparse areas, the grid is scanned by infill procedure (KK = 5). Any grid point without a nearby isopressure contour (denoted by TEST [I,J] = 0) will have a line started and projected to an edge. The 500 series of statements in the MAIN program are to complete such infill lines in the opposite direction.

The core storage required for the isopressure program is 23,600 words, and the CPU time for the 7-spot example is 15 seconds on the CDC 6600.

## STREAMLINES

### Orthogonality

The principles of orthogonality were used to determine the streamlines from the isopressure contours, since the streamlines are at right angles to isopressure lines at the points of intersection. The schematics of the procedure are shown in figure 5. A perpendicular from the intersection of the streamline and the lower or "first" isopressure contour is projected to the upper or second isopressure contour. A tangent line to the upper isopressure at this point is determined. From a point on this tangent line, a perpendicular is dropped such that it will intersect the perpendicular from the lower isopressure-line point, midway for both perpendiculars. The perpendiculars will be of equal length and therefore equidistant from the tangent line to the upper isopressure contour and the streamline intersection with the lower isopressure.

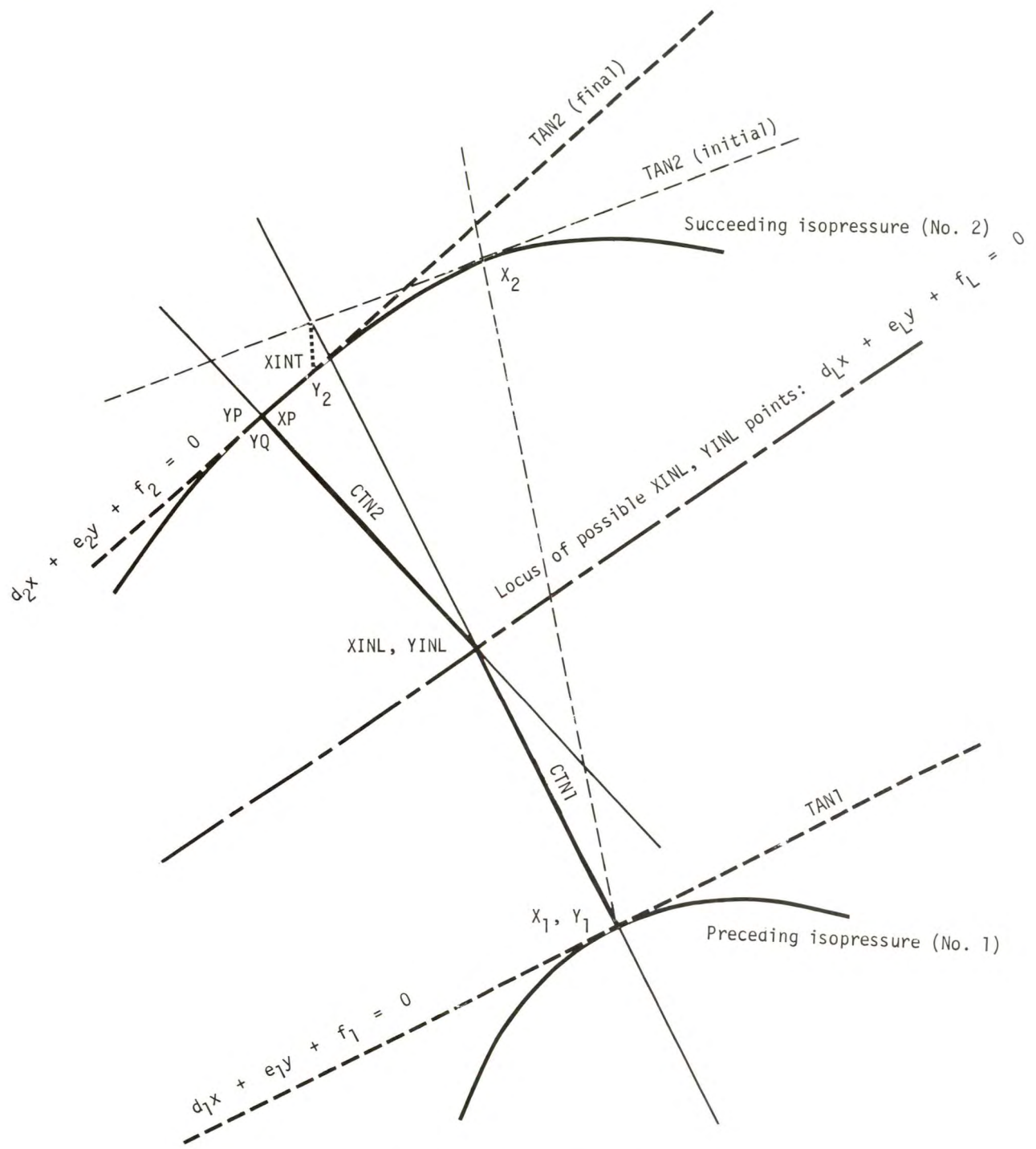


FIGURE 5. - Schematics for Intersection of Orthogonal Lines.

The point on the tangent line, from which this perpendicular is dropped, is seldom on the upper isopressure line, but the place where the perpendicular crosses the isopressure line is the starting point for the calculation of another tangent and perpendicular. The second iteration usually approaches coincidence for all practical purposes. However, the program permits 10 iterations.

This procedure has created streamlines that are (1) circles and (2) ellipses from the isopressures that are orthogonal to the circles and ellipses (as well as reproducing the streamlines for a 7-spot pattern). Therefore, the method must be basically sound; that is, a circle and an ellipse are known configurations. A method that accurately reproduces a known configuration as a streamline should successfully calculate more complex configurations.

The equation for the perpendicular distance  $d_1$  from a line whose normal-form equation is  $Ax + By + C = 0$  to the point  $x_1, y_1$  is

$$d_1 = \frac{A_1 x_1 + B_1 y_1 + C_1}{\pm \sqrt{A_1^2 + B_1^2}}, \quad (6)$$

wherein the sign of the radical is opposite the sign of  $C_1$ . Since the calculations are always in the same quadrant, no change of sign is necessary. The  $A_1, B_1,$  and  $C_1$  are the constants of the equation of a line from which the perpendicular is drawn. The perpendicular is used to determine the tangent to a point on a contour line. Similarly, the equation for the distance for the second perpendicular is

$$d_2 = \frac{A_2 x_1 + B_2 y_1 + C_2}{\pm \sqrt{A_2^2 + B_2^2}}. \quad (7)$$

Equations 6 and 7 are equated and solved for an equation in  $x_1$  and  $y_1$ . The resulting equation is the locus of the equidistance points. With the equation for the perpendicular from the lower isopressure line and the equation of the locus, the values of  $x_1$  and  $y_1$  at the intersections of the perpendiculars can be calculated. Then the value of  $x_2$  and  $y_2$  at the point from where the perpendicular was dropped can be calculated. The value of  $x_2$  is substituted in the equation for the upper isopressure segment. If the resulting  $y_3$  lies near enough to  $y_2$  by a predetermined amount,  $x_2$  and  $y_3$  are the coordinates of the point of the streamline passing through the isopressure line. Otherwise, another iteration is made. The foregoing is explained in detail in the next section.

#### Computer Solution for Streamline Intersection

The stepwise procedure for the computer program to solve for the coordinates of the intersection of a streamline and succeeding isopressure line is as follows (see fig. 5):

1. Estimates  $x$  coordinate,  $X_2$ , of intersection and looks up on succeeding isopressure line to determine index for the three surrounding points. (See subroutine LOCATE.)
2. Computes constants for the circle equation through the points.
3. Calculates slope and intercept of straight line (TAN2 initial) tangent to isopressure curve using derivative equation. Also computes

slope and intercept of normal line (CTN1) and tangent line (TAN1) to preceding isopressure.

4. Solves equation for intersection of the normal (CTN1) and TAN2 lines to obtain abscissa of intersection. (XINT.)

5. Redetermines indexes and constants for points on succeeding isopressure around XINT (see steps 1 and 2).

6. Calculates slope and intercept of new TAN2 line passing through XINT.

7. Using determinants and the normal equations for TAN1 and TAN2 lines, solves for equation of locus of points equidistant from the two lines. Then solves this equation for intersection of locus line with CTN1 line (XINL, YINL).

8. Using this point and slope of line normal to TAN2 (CTN2), computes intercept of CTN2 line.

9. Then solves for intersection of normal and tangent lines using equation similar to that used for step 4.

10. Calculates ordinate of intersection using tangent line equation and isopressure curve equation.

11. If the ordinate values are sufficiently close, prints out and goes on to next point. Otherwise, goes back to step 2 and repeats computations.

### MAIN Program, Subroutines, and Operating Details

#### MAIN Program and Data Preparation

The MAIN program for calculating streamlines between an input-output well couplet is listed in table 6. The schematic flow diagram is shown in figure 6.

The first card carries the integer variables that control the data processing and computations. The first value, NLINE, is the number of isopressure lines to be used in the calculations. NSTREAM is the number of streamlines to be calculated and NINT provides for skipping some of the isopressure points to start a streamline. NSTART is the index of the isopressure line from which the streamlines are extended initially. This line is in the radial area near the injection well and contains sufficient points to start all the streamlines required. The remaining integers on the first card (IFLAG), if not zero, direct the program to one of the boundary options in subroutine BOUND.

TABLE 6. - Streamline MAIN program with explanatory comments

```

C   MAIN PROGRAM FOR STREAMLINE CALCULATION.

COMMON / FIELD / XA(70,70), YA(70,70), XS(70), YS(70), LGO
DIMENSION NITAL(70), IFLAG(20)

C   READ IN COORDINATES OF ISOPRESSURE LINES AND OTHER DATA.
1000 READ 1000, MLINE, NSTREAM, NINT, MSTART, (IFLAG(I), I=1, NSTREAM)
      FORMAT (20I3 )
      DO 10 M = 1, MLINE
      READ 1001, AVP, NITAL
      1001 FORMAT (F15.5, I10)
      PRINT 1001, AVP, NITAL
      NITAL(M) = NITAL
      READ 1002, (XA(N,M), YA(N,M), N = 1, NITAL)
      1002 FORMAT (8F10.3)
      PRINT 1002, (XA(N,M), YA(N,M), N = 1, NITAL)
      10 CONTINUE

C   START DO STATEMENT FOR A STREAMLINE.
DO 100 IS = 1, NSTREAM, NINT
  IF ( IFLAG(IS).EQ.1 ) GO TO 95
  X1 = XA(IS, MSTART)
  Y1 = YA(IS, MSTART)

  LGO = 1
  IPTAL = 2
  XS(2) = X1
  YS(2) = Y1
  NP3 = IS
  IF ( (IS+1).GE.NSTREAM .AND. NSTREAM.GT.2 ) NP3 = NSTREAM - 2
  CALL QUAD ( NP3, MSTART, A1, B1, R1 )
  MLNM2 = MLINE - 2

C   DO STATEMENT FOR A POINT ON STREAMLINE.
DO 80 MP = MSTART, MLNM2
  IF ( MP.EQ.MSTART ) GO TO 50
  A1 = A2
  B1 = B2
  R1 = R2

50 NE = NITAL(MP+1)
  MP1 = MP+1
  JTAG = 0
  CALL LOCATE ( IS, MP1, NE, NP3, X1, Y1, IPTAL, X2, JTAG )
  IF ( LGO.EQ.2 ) GO TO 92

  CALL QUAD ( NP3, MP1, A2, B2, R2 )

  CALL STRM (A1, B1, R1, A2, B2, R2, X1, Y1, XP, YQ, MP1,
1 NE, NP3, IS, IPTAL, X2, JTAG )
  IF ( LGO.EQ.2 ) GO TO 92

```

Indexes pertaining to whole flow net.

Pressure and number of points on isopressure line.

Index number of points on isopressure line.  
X and Y coordinates of points on isopressure line.

Go to 85 to handle boundary condition.  
Set starting point of streamline for projection.

Index starting point leaving room for X and Y at injection well.

Determine constants for equation of isopressure line from which  
streamline is extended ("First isopressure").

After first segment of streamline is calculated, reset  
equation constants.

Determine index for section of second isopressure probably  
intersected.

Constants for equation of second isopressure.

Calculates projected normals and coordinates of intersection  
with isopressure line.  
Bypasses indexing if no intersection found.

TABLE 6. - Streamline MAIN program with explanatory comments--Continued

<pre> IPTAL = IPTAL + 1 XS(IPTAL) = XP YS(IPTAL) = YQ IF (IFLAG(IS).EQ.2) CALL BOUND (IFLAG, IPTAL, MSTART, MLINE, 1 NTAL, NITAL, IS ) X1 = XS(IPTAL) Y1 = YS(IPTAL) 80 CONTINUE GO TO 90 </pre>	<p>Indexes point of intersection as a point on streamline. Handles diagonal boundary.</p>
<pre> 85 CALL BOUND ( IFLAG, IPTAL, MSTART, MLINE, NTAL, NITAL, IS ) GO TO 92 </pre>	<p>Handles vertical boundary.</p>
<pre> C SET INITIAL AND FINAL POINTS ON STREAMLINE . 90 IPTAL = IPTAL + 1 XS(IPTAL) = XA(1, MLINE) YS(IPTAL) = YA(1, MLINE) 92 XS(1) = XA(1,1) YS(1) = YA(1,1) </pre>	<p>Coordinates of point near production well. Coordinates of point near injection well.</p>
<pre> C PUNCH OUTPUT FOR SHAPE FACTOR PROGRAM. IN = MOD(IS+1, 2) + 1 PUNCH 3000, (XS(IP), IP = 1, IPTAL, IN ) 3000 FORMAT ( 7F10.4 ) PUNCH 3000, (YS(IP), IP = 1, IPTAL, IN ) PUNCH 3000 </pre>	<p>Every other value on every other streamline is omitted because it is in interior of cell.</p>
<pre> C PRINT OUT VALUES FOR STREAMLINE. 95 PRINT 2010, IS 2010 FORMAT ( *1 STREAMLINE * I2 / * XS YS * ) DO 100 IP = 1, IPTAL 100 PRINT 2011, XS(IP), YS(IP) 2011 FORMAT ( 2F10.3 ) </pre>	
<pre> STOP END </pre>	

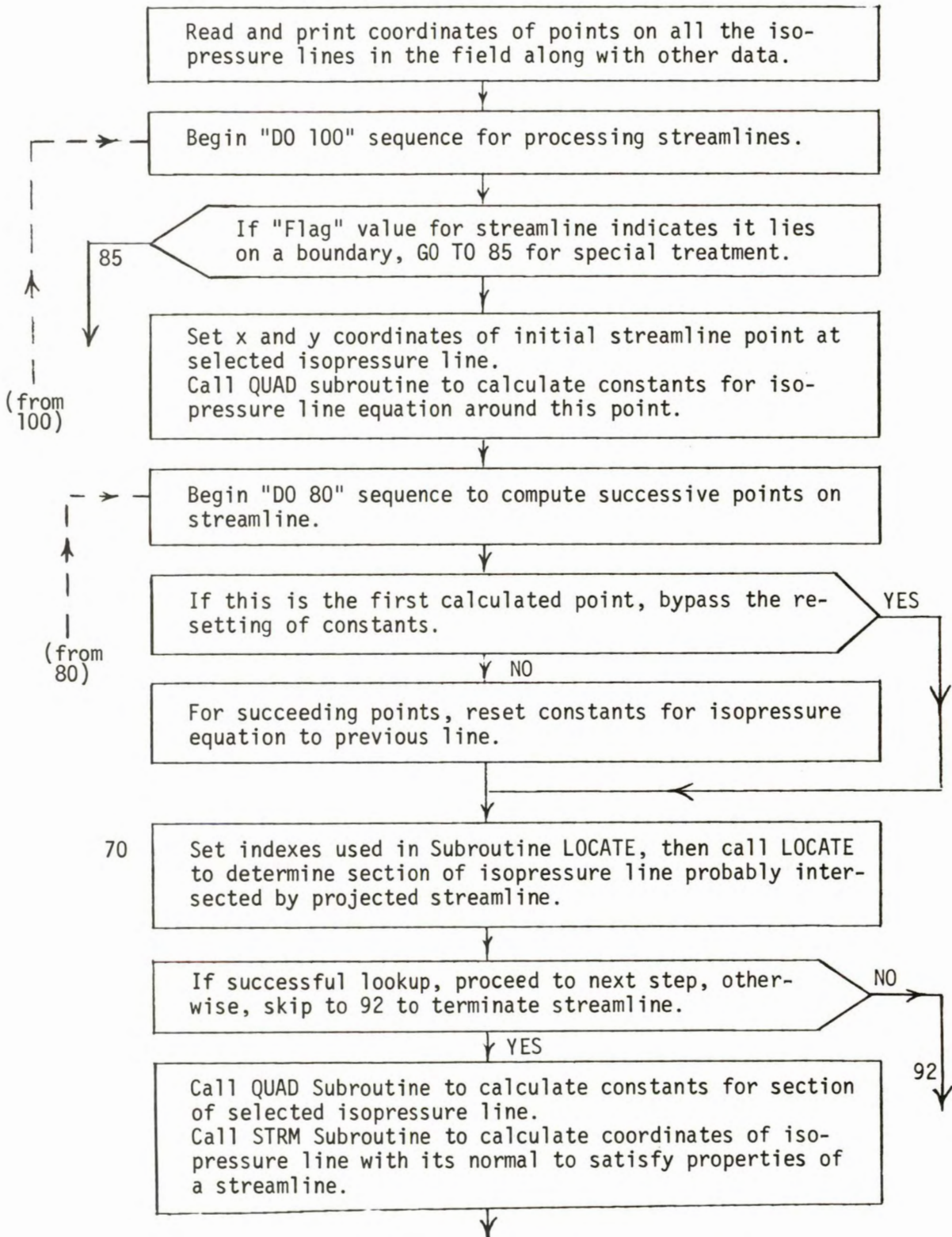


FIGURE 6. - Schematic Flow Diagram for Streamline MAIN Program.

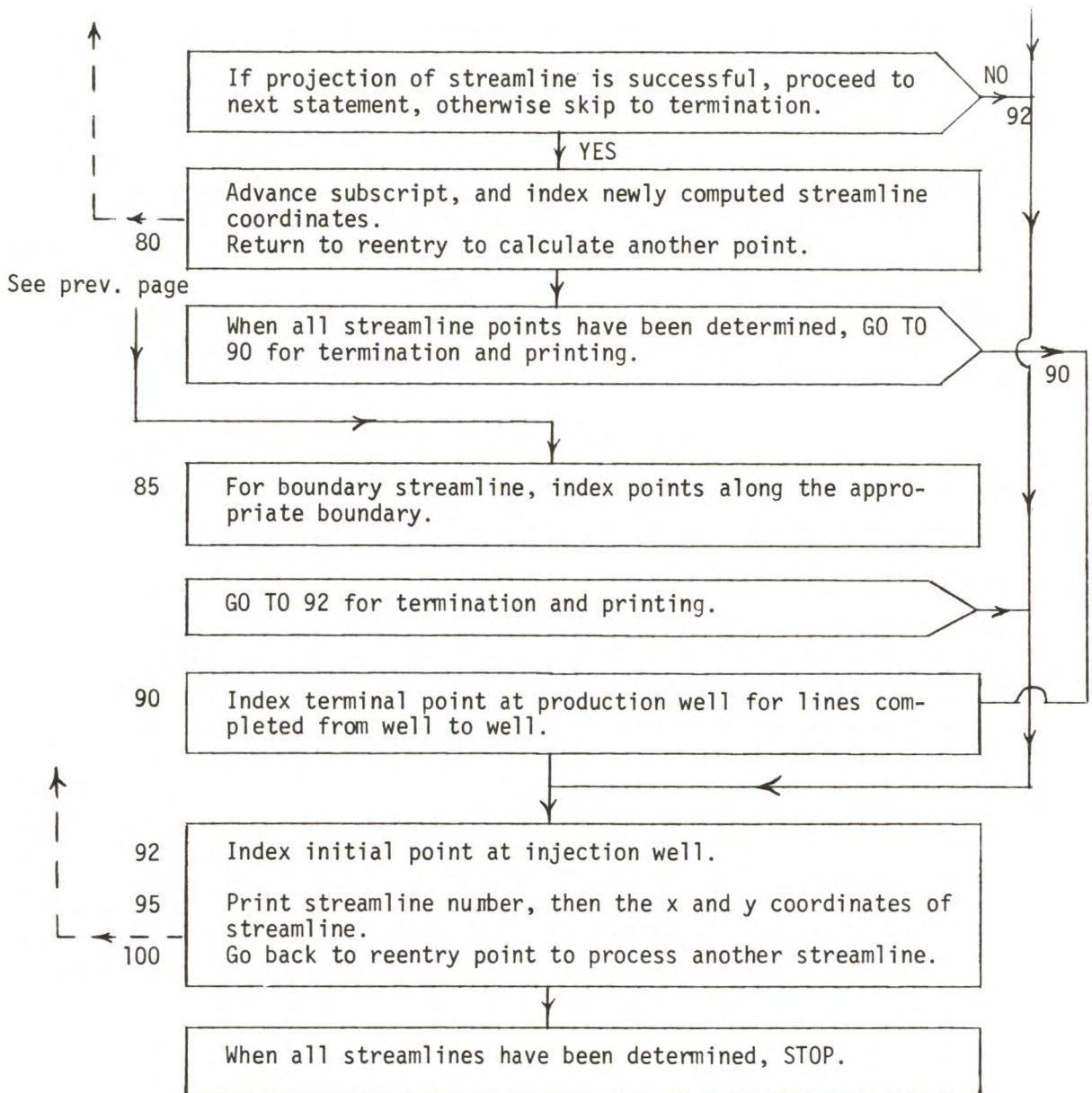


FIGURE 6. - Schematic Flow Diagram for Streamline MAIN Program.—Continued

The remaining data are the sets of isopressure coordinates determined using the isopressure program. The first or header card of each set contains the pressure, number of points, and the beginning and ending x and y coordinates of the isopressure line. The remaining cards contain the coordinates of all the points. Included is a one-value set each for the input and output wells. For the example presented in this paper, the data in the right side of the field (KK = 1) were used because a plot<sup>6</sup> of those isopressure lines

<sup>6</sup>The plot was made quickly and accurately by machine from data punched from computer memory.

showed apparently adequate coverage of the pattern element. If a higher density of lines in an area is desired, additional lines can be selected from data determined using the infill sweep ( $KK = 5$ ) by aid of a complete plot and the data on the header card for each isopressure line.

For each streamline, the program processed the first projected point. Then in the DO 80 statement, each succeeding point is determined and the streamline is continued until the last isopressure line is intersected unless the calculation is terminated. The program then adds the coordinates of the input well and, if the streamline is complete, adds the coordinates of the output well. After all the streamlines have been determined, the coordinates are punched on cards and printed out according to the input format required by the shape factor calculation program published in Report of Investigations 6760 (2) or Report of Investigations 7111 (4).

#### Locating Index on Isopressure Line--Subroutine LOCATE

The index of the nearest point on an isopressure line intersected by a streamline is determined by use of the "IF" statements in subroute LOCATE, shown in table 7. The first set of IF statements attempts to locate a pair of isopressure points having x coordinates on either side of the estimated intersection. If this fails, the second set attempts a lookup along the y axis. When an index is found, the other coordinate is tested for closeness to insure that the points located are not on another section of the isopressure line.

When the isopressure line has a steep slope, it is frequently necessary to increase the streamline's estimated x coordinate to locate an intersection. The x increment is estimated initially in the first statements of the subroutine, and if necessary, the value is further increased. The flow diagram for the subroutine is shown in figure 7.

The procedure to obtain the orthogonal streamlines previously explained is programed in subroutine STRM shown in table 8. The flow diagram is in figure 8.

TABLE 7. - Program for subroutine LOCATE with explanatory comments

```

SUBROUTINE LOCATE ( IS, MP, NE, NP3, X1, Y1, IPTAL, X2, JTAG )
COMMON / FIELD / XA(70,70), YA(70,70), XS(70), YS(70), LGO

NR = 1
NFM1 = NE - 1
IF (IPTAL.LE.2 ) DEL = (X1-XA(1,1)) / SQRT ((X1-XA(1,1))**2 +
1 (Y1-YA(1,1))**2 )
IF (IPTAL.GT.2 ) DEL = XS(IPTAL) - XS(IPTAL-1)
IF ( JTAG.GT. 0 ) DEL = 0
XT = X1 + DEL * 0.7
NNN = 0

10 CONTINUE
DO 20 NT = NR, NEM1
IF (XA(NT,MP) .LE. XT.AND.XT.LT.XA(NT+1, MP)) GO TO 50
IF (XA(NT,MP) .GE. XT.AND.XT.GT.XA(NT+1, MP)) GO TO 50
20 CONTINUE
DO 30 NT = NR, NFM1
IF (YA(NT,MP) .LE. Y1.AND.Y1.LT.YA(NT+1, MP)) GO TO 60
IF (YA(NT, MP).GE. Y1.AND.Y1.GT.YA(NT+1, MP)) GO TO 60
30 CONTINUE

36 NR = 1
NNN = NNN + 1
IF ( NNN.GE.10) GO TO 90
40 XT = XT + DFL/5.0
GO TO 10

50 IF (IPTAL.LE.2 ) YS(IPTAL-1) = YS(IPTAL)
YTEST = YS(IPTAL) + (YS(IPTAL) - YS(IPTAL-1) )
IF ( ABS(YA(NT,MP)-YTEST).GT.3.0 ) GO TO 80
GO TO 70

60 IF (IPTAL.LE.2 ) XS(IPTAL-1) = XS(IPTAL)
XTTEST = XS(IPTAL) + (XS(IPTAL) - XS(IPTAL-1) )
IF ( ABS(XA(NT,MP)-XTTEST).GT.1.5 ) GO TO 80
XT = XA(NT,MP)

70 NP3 = NT
IF ( NP3.GT.(NE-2) ) NP3 = NE - 2
X2 = XT
RETURN

80 NR = NT + 1
IF ( NR.LE.NEM1 ) GO TO 10
GO TO 36

90 PRINT 9000, NE, MP
9000 FORMAT ( *1 FAILURE TO LOCATE NE= * I3, * MP= * I3 )
LGO = 2
RETURN
END

```

Estimate of "step-out" on x equals unit grid length  
(not shown) times cosine of streamline angle from well.

Subsequently use previous x difference.  
In lookup from STRM, do not step out.  
"Stepout" probably only goes part way.

Lookup in x direction.

Lookup in y direction.

Start at beginning of pressure line with increased stepout.  
Advance counter on "stepout" increase.  
If more than 10 tries, probably cannot be located. Go to 90 to  
print message and return.

If located on x, check approximate y location.

If located on y, check approximate x location.  
If located on y, an x value is needed.

Set index of nearby point;  
change if too near end of pressure line.

Advance starting index of lookup to try another portion of line.  
If at end of line, go through steps to increase stepout and  
repeat lookup.

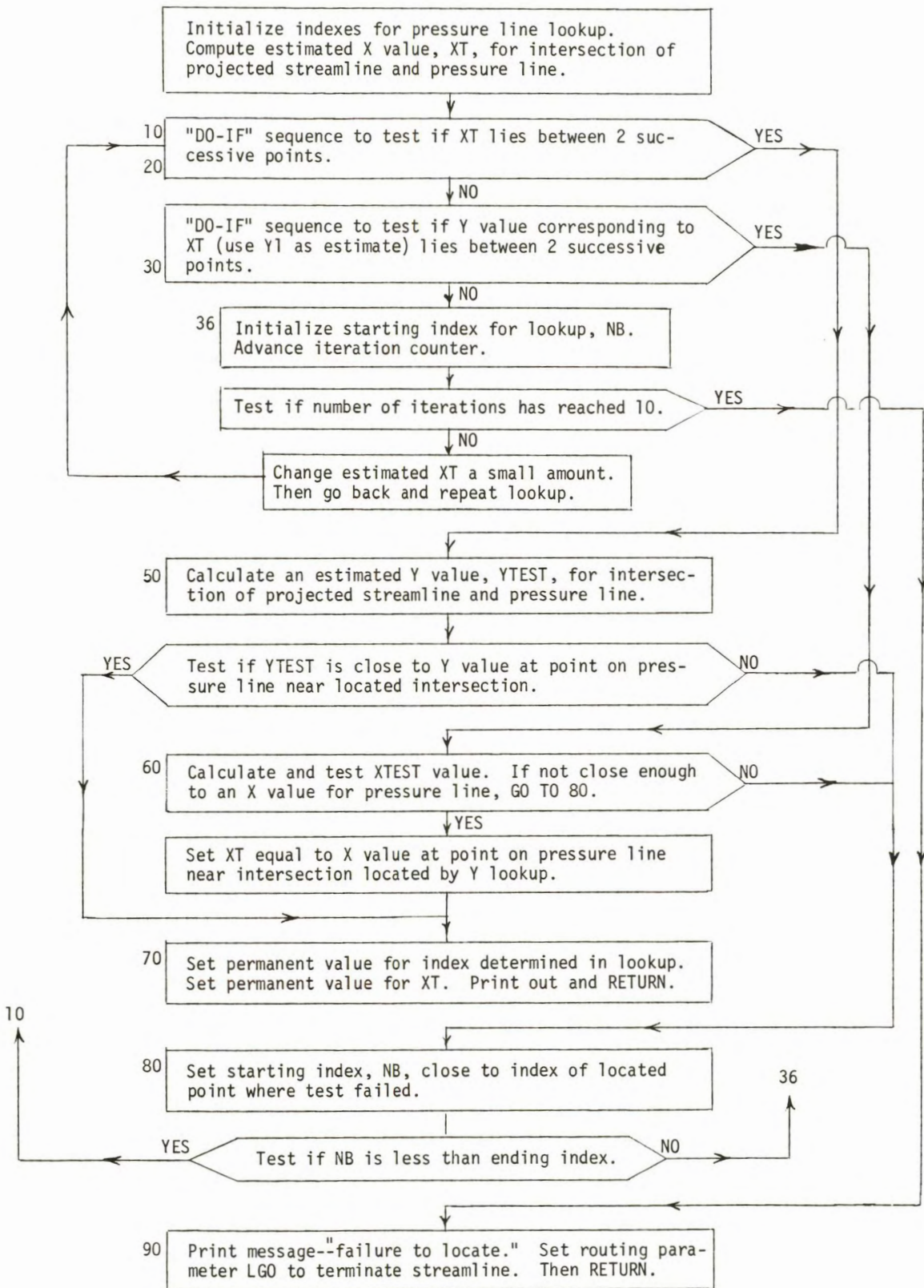


FIGURE 7. - Schematic Flow Diagram for Subroutine LOCATE.

TABLE 8. - Program for subroutine STRM with explanatory comments

```

SUBROUTINE STRM (A1, B1, R1, A2, B2, R2, X1, Y1, XP, YQ, MP,
1 NE, NP3, IS, IPTAL, X2, JTAG )
COMMON / FIELD / X (70,70), Y (70,70), XS(70), YS(70), LGO

C   FUNCTION DEFINITIONS
CTN (TANN) = -1.0/TANN           Cotangent from tangent.
AS ( Y , TANN, X ) = Y - TANN * X   Y intercept in a linear equation.

C   CALCULATES FIRST VALUE OF INTERSECTION
TAN1 =TN(A1, R1, X1, Y1, Y1, B1 )   Tangent to isopressure line (previous or No. 1) at coordinates of streamline.1/
IF ( ABS(TAN1).GT.1.0E+4 ) GO TO 92
AS1 = AS ( Y1, TAN1, X1 )           Y intercept for tangent.
CTN1 = CTN(TAN1)                   Cotangent.
ACTN1 = AS ( Y1, CTN1, X1 )         Y intercept for cotangent equation.
TAN2 = TN(A2, R2, X2, Y(NP3,MP), Y(NP3+1,MP), B2 )   Tangent to isopressure line (succeeding or No. 2) at nearly the same X as for
isopressure No. 1.
IF ( ABS(TAN2).GT.1.0E+4 ) GO TO 94   Test if isopressure No. 2 is vertical.
Y2 = Y VALUE ( A2, B2, R2, X2, Y(NP3,MP), Y(NP3+1,MP) )   Value of Y for isopressure No. 2 at nearly the same X as for isopressure No. 1.
AS2 = AS ( Y2, TAN2, X2 )           Value of Y intercept for equation of tangent to isopressure No. 2.
XINT = ( ACTN1 - AS2 ) / ( TAN2 - CTN1 )   Value of X where the cotangent for isopressure No.1 intersects the tangent to
isopressure No. 2.
ITER = 0
JTAG = 1
CALL LOCATE ( IS, MP, NE, NP3, XINT, Y1, IPTAL, X2, JTAG )   Verify or refine lookup of section of isopressure line at inter-
section.
XINT = X2

50 CALL QUAD ( NP3, MP, A2, B2, R2 )   Obtains constants of circle equation for improved position on isopressure No. 2.
IF ( (R2**2 - (XINT-A2)**2 ) .LE.0.0 ) GO TO 85   Test if x value falls outside of circle comprising section of isopressure line.

C   CALCULATES ITERATED VALUE FOR INTERSECTION
60 TAN2 =TN(A2, R2, XINT, Y(NP3,MP), Y(NP3+1,MP), B2 )   New tangent at the improved location.
IF ( ABS(TAN2).GT.1.0E+4 ) GO TO 94   Tests if isopressure line No. 2 is vertical.
Y2 = Y VALUE ( A2, B2, R2, XINT, Y(NP3,MP), Y(NP3+1,MP) )   Value of Y at point of intersection of perpendicular (cotangent) from
isopressure No. 1 to isopressure No. 2 at improved location.
AS2 = AS ( Y2, TAN2, XINT )           New Y intercept for tangent equation at foregoing point.
DM1 = SQRT ( TAN1 ** 2 + 1.0 )         Denominator of equation for length of a perpendicular from a line -
isopressure No. 1.
DM2 = SQRT ( TAN2 ** 2 + 1.0 )         Denominator of equation for length of a perpendicular from a line -
isopressure No. 2.

```

TABLE 8. - Program for subroutine STRM with explanatory comments--Continued

ASD1 = AS1 / D M1  
 ASD2 = AS2 / D M2  
 TAND1 = TAN1 / D M1  
 TAND2 = TAN2 / D M2

Denominators are divided into coefficients of numerator terms of the equation for the length of perpendiculars from a line. In the equation

$$d_1 = \frac{a_1 x_1 + b_1 y_1 + c_1}{\sqrt{a_1^2 + b_1^2}}$$

$$DM1 = \sqrt{(TAN1)^2 + (-1.0)^2}$$

$$a_1 = TAN1 \quad a_2 = TAN2$$

$$b_1 = -1.0 \quad b_2 = -1.0$$

$$c_1 = AS1 \quad c_2 = AS2$$

YD1 = -1.0 / DM1  
 YD2 = -1.0 / DM2

$d_1 = -d_2$  therefore  $\frac{a_1 x_1 + b_1 y_1 + c_1}{DM1} = \frac{-a_2 x_2 - b_2 y_2 - c_2}{DM2}$  or  $\frac{a_1 x_1}{DM1} + \frac{a_2 x_1}{DM2} + \frac{b_1 y_1}{DM1} + \frac{b_2 y_1}{DM2} + \frac{c_1}{DM1} + \frac{c_2}{DM2} = 0$

ASC = ASD1 + ASD2  
 TANC = TAND1 + TAND2

or  $TANC * X1 + YC * Y1 + ASC = 0$ , the equation of the locus of the equal perpendiculars.

$$-TANC * X - YC * Y = ASC \quad \text{equation of locus}$$

YC = YD1 + YD2

$$-CTN1 * X + (1) * Y = ACTN1 \quad \text{equation of first cotangent}$$

C FINDS VALUES OF X AND Y AT INTERSECTION OF LOCUS AND COTANGENT  
 C NUMBER 1 BY DETERMINANTS.

DEM = ( -TANC - (-CTN1 \* (-YC)) )

$$XINL = x = \frac{\begin{vmatrix} f_1 & e_1 \\ f_2 & e_2 \end{vmatrix}}{\begin{vmatrix} d_1 & e_1 \\ d_2 & e_2 \end{vmatrix}}, \text{ where } DEM = \begin{vmatrix} d_1 & e_1 \\ d_2 & e_2 \end{vmatrix}, \text{ and } YINL = y = \frac{\begin{vmatrix} d_1 f_1 \\ d_2 f_2 \end{vmatrix}}{DEM}$$

XINL = ( ASC - (-YC) \* ACTN1 ) / DEM

YINL = (-TANC \* ACTN1 - ASC \* (-CTN1)) / DEM

C FINDS THE VALUE OF X AND Y ON TANGENT NUMBER 2.

CTN2 = CTN ( TAN2 )

Cotangent.

ACTN2 = AS ( YINL, CTN2, XINL )

Y intercept using coordinates of y and x at the point junction of the two cotangents.

XP = ( ACTN2 - AS2 ) / ( TAN2 - CTN2 )

Value of x at the base of perpendicular from the tangent to isopressure No. 2. This perpendicular intersects the perpendicular from isopressure No. 1 so that the length of perpendiculars are equal.

YP = AS2 + TAN2 \* XP

Value of y at the same point for x above.

IF ( (R2\*\*2 - (XP - A2)\*\*2) .LE.0.0 ) GO TO 85

Test if x value is outside of circle.

YQ = Y VALUE ( A2, B2, R2, XP, Y(NP3,MP), Y(NP3+1,MP) )

Value of y using isopressure line equation corresponding to x above.

C TESTS Y VALUES FOR CONVERGENCE AND PREPARES TO ITERATE IF REQUIRED

IF ( ABS(YP-YQ) .LT. 0.0100 ) LGO = 1

If YP from perpendiculars is close enough to isopressure No. 2, return; otherwise another iteration is made.

IF ( ABS(YP - YQ) .LT. 0.0100) RETURN

TABLE 8. - Program for subroutine STRM with explanatory comments--Continued

70	XINT = XP TAN2 = TN(A2, R2, XP, Y(NP3,MP), Y(NP3+1,MP), B2 ) IF ( ABS(TAN2).GT.1.0E+4 ) GO TO 94	Tangent at calculated point. Test if isopressure line is vertical.
	ITER = ITER + 1 IF ( ITER .GT. 10 ) GO TO 90	Advance iteration counter and proceed if less than 10.
	CALL LOCATE ( IS, MP, NE, NP3, XINT, YQ, IPTAL, X2, JTAG ) GO TO 50	Locate index of isopressure line section and go to 50 to complete another iteration.
C PROVISIONS FOR HANDLING IRREGULAR SITUATIONS		
85	PRINT 8500	
8500	FORMAT ( * ABSCISSA INCOMPATABLE WITH CIRCLE EQUATION * ) LGO = 2 RETURN	x value falls outside of circle comprising section of isopressure line.
90	PRINT 9000	
9000	FORMAT ( * FAILURE TO CONVERGE * ) LGO = 2 RETURN	If 10 iterations do not provide convergence on an intersection, there is probably an error in data.
92	YQ = Y1 + .01 GO TO 95	Horizontal streamline directed slightly upward.
94	YQ = Y1 - .01	Horizontal streamline directed slightly downward.
95	XP = X(NP3,MP) LGO = 1 RETURN	
	END	

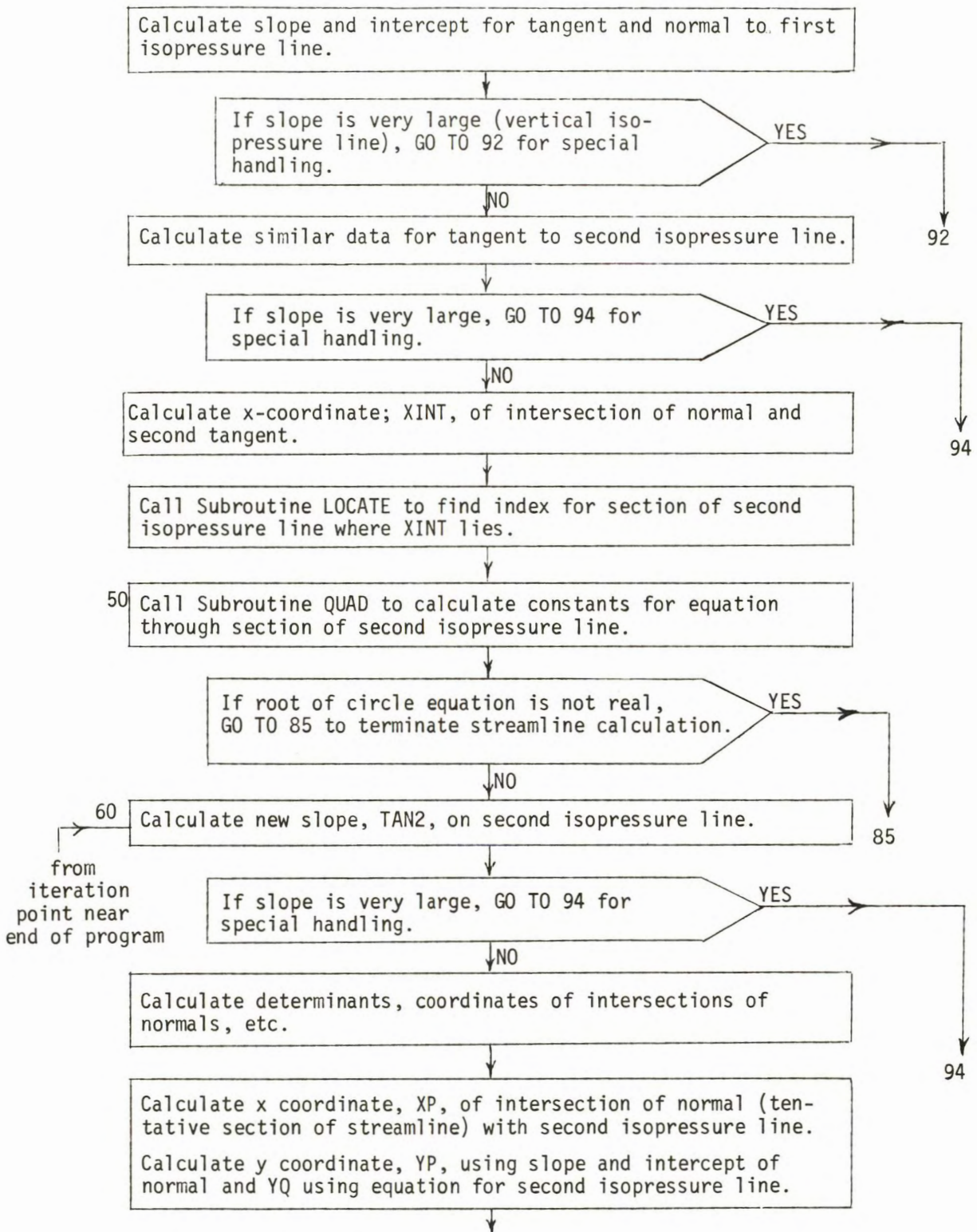


FIGURE 8. - Schematic Flow Diagram for Subroutine STRM.

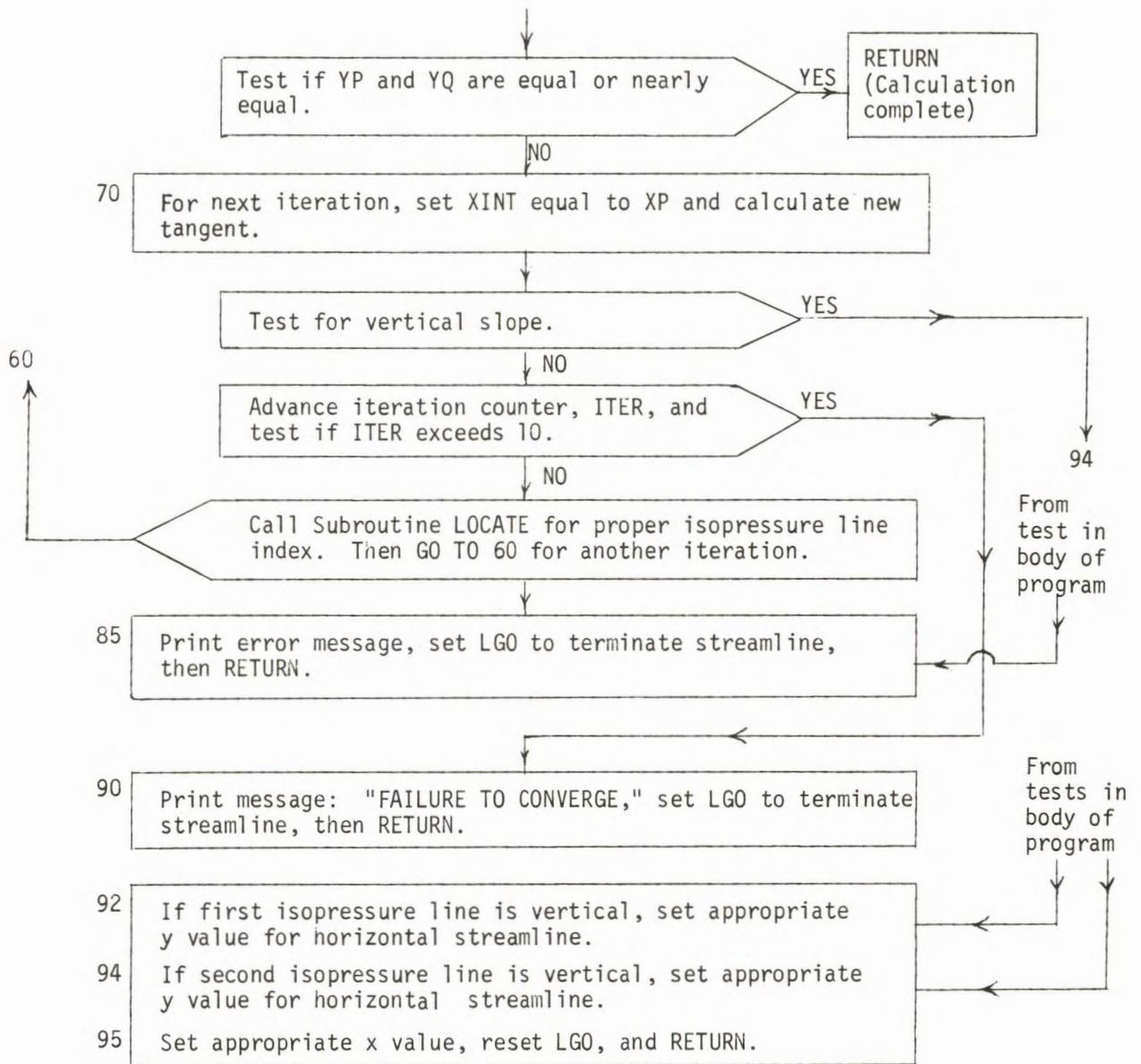


FIGURE 8. - Schematic Flow Diagram for Subroutine STRM.—Continued

Circle Equation Between Isopressure Points--  
Subroutine QUAD

Subroutine QUAD solves for the constants of the equation of circle passing through the three points near the intersection. This subroutine is listed in table 9. This type of equation was used because of the circular shape of isopressures around wells and because the previously used quadratic equation proved occasionally to interpolate nonmonotonically for a steep-sloping isopressure line.

TABLE 9. - Program for subroutine QUAD with explanatory comments

```

SUBROUTINE QUAD ( NP3, MP, A, B, R )
COMMON / FIELD / X (70,70), Y (70,70), XS(70), YS(70), LG0

DELX12 = X(NP3,MP) - X(NP3+1,MP)
DELX23 = X(NP3+1,MP) - X(NP3+2,MP)
DELY12 = Y(NP3,MP) - Y(NP3+1,MP)
DELY23 = Y(NP3+1,MP) - Y(NP3+2,MP)
DXSQ12 = X(NP3,MP)**2 - X(NP3+1,MP)**2
DXSQ23 = X(NP3+1,MP)**2 - X(NP3+2,MP)**2
DYSQ12 = Y(NP3,MP)**2 - Y(NP3+1,MP)**2
DYSQ23 = Y(NP3+1,MP)**2 - Y(NP3+2,MP)**2

IF ( DELX12.F0.0. ) DELX12 = 0.1E-10
IF ( DELY12.F0.0. ) DELY12 = 0.1E-10
IF ( DELY23.F0.0. ) DELY23 = 0.1E-9

B = ( DELX23*(DXSQ12+DYSQ12) - DELX12*(DXSQ23+DYSQ23) ) /
1 2.0 / (DELY12*DELX23 - DELY23*DELX12)
A = (DXSQ12 + DYSQ12 - 2.0*B*DELY12) / 2.0 / DELX12
X1 = X(NP3,MP)
Y1 = Y(NP3,MP)
R = SQRT((X1-A)**2 + (Y1-B)**2 )
IF ( R.GT.1.0E+5 ) R = R + 1.0

RETURN
END

```

Differences used to solve for constants.

Constants A, B, and R to satisfy  
 $R^2 = (X - A)^2 + (Y - B)^2$   
for X and Y at points IP3, IP3+1, and IP3+2.

#### Irregular, Discontinuous, and Extreme Conditions-- Subroutine BOUND

The principal use of the isopressure and streamline programs presented in this paper is for determination of the potentiometric flow net for any field. Before the streamline calculation can be started, the destination (output well) of each prospective streamline must be determined by aid of a plot of the isopressure lines. Each streamline starts at one of the points on the starting isopressure line (indexed NSTART), and all the isopressures to be intersected on the way to the output well can be grouped. A separate run should be made for each group of streamlines (input-output well couplet) and its group of isopressure lines. The selections can be made by aid of a plot of all the isopressures and the data on each isopressure line's header card.

In addition to using read-in points on the starting isopressure line, additional points may be selected. One or more points should be chosen at or near the streamline dividing any two injection-production-well couplets. When the exact location of the dividing streamline is not known, nearby streamlines can be calculated from estimated starting points. Then the procedure can be repeated with the adjusted starting point until the true dividing line is traced. A plot of these neighboring streamlines will reveal that the streamlines surrounding a dividing streamline will either approach a boundary or diverge abruptly to one or the other output well.

Subroutine BOUND in table 10 is a compilation of statements designed to accomplish the foregoing procedure and to handle other irregular situations. The subroutine was designed for the basic element of 7-spot pattern which is the example used in this paper. For any other flow net, many of the statements would be different.

TABLE 10. - Program for subroutine BOUND with explanatory comments

```

SUBROUTINE BOUND ( IFLAG, IPTAL, MSTART, MLINE, NTAL, NITAL, IS )
COMMON / FIELD / XA(70,70), YA(70,70), XS(70), YS(70), LGO
DIMENSION NITAL(70), IFLAG(20)

IF ( IFLAG(IS).GT.1 ) GO TO 20

C   SETS VALUES FOR VERTICAL BOUNDARY.
  IPTAL = 1
  DO 10 M = MSTART, MLINE
    IPTAL = IPTAL + 1
    XS(IPTAL) = XA(IS, M)
    YS(IPTAL) = YA(IS, M)
  10 CONTINUE
  RETURN

20 IF ( YS(IPTAL) .LE. 46.198 ) GO TO 25

C   ADJUSTS VALUES TO COINCIDE WITH LOWER DIAGONAL LINE.
  DELTA = XS(IPTAL) * 1.7308 - YS(IPTAL)
  IF ( ABS(DELTA) .LE. 0.01 ) RETURN
  XS(IPTAL) = XS(IPTAL) - 0.43316 * DELTA
  YS(IPTAL) = YS(IPTAL) + 0.25028 * DELTA
  RETURN

C   ADJUSTS VALUES TO COINCIDE WITH UPPER DIAGONAL LINE.
25 DELTA = 61.622 - 0.57777*XS(IPTAL) - YS(IPTAL)
  IF ( ABS(DELTA) .LE. 0.01 ) RETURN
  XS(IPTAL) = XS(IPTAL) + 0.25028 * DELTA
  YS(IPTAL) = YS(IPTAL) + 0.43316 * DELTA
  RETURN

END

```

These XA and YA values are on vertical boundary of element.

Tests if above or below corner of element.

Difference between ordinate of diagonal line (lower) from injection well and calculated ordinate.  
Adjust XS by cosine of diagonal angle times difference.  
" YS " sine " " " " " " " " " " " "

Difference between ordinate of diagonal line (upper) to production well and calculated ordinate.  
Adjust XS and YS as described above.

Streamline number 1 shown in figure 9 is the connecting streamline between the injection and production wells in the element. Because the streamline is vertical and is at the ends of the isopressure lines, its path did not follow the straight vertical line but drifted outside the element. The first section of subroutine BOUND sets all the values of streamline 1 to the coordinates of the vertical line.

No other irregularities were encountered until the dividing streamline (No. 7) was run. Previous trial runs which showed mirror images confirmed the necessary symmetry. In the example, however, the exact location of the dividing streamline and its starting point were calculated analytically. As each point on this streamline was determined, a test in subroutine BOUND compared the point's coordinates with the corresponding point on the actual boundary. If the two points differed appreciably, the calculated point was adjusted until it coincided with the analytical point.

In the area of widest spacing of isopressure lines, streamline 7 terminated in subroutine LOCATE, owing to inability to locate an intersection with the proper isopressure line. The coordinates of the last point were used as the starting point for the second straight line (streamline 7b), and the computer run was restarted. A dummy point was selected to aid in estimating the distance for the first projection. Then streamline 7b to the output well was computed and adjusted in the same manner as 7a. It was necessary to change the first IF statement in subroutine LOCATE for processing 7b by deleting the denominator of the expression. The statement then reads "IF (IPTAL,LE.2) DEL = (X1-XA(1,1) )". This procedure is to estimate the initial "stepout," DEL, based on the "pseudo" initial x coordinate read in (XA(1,1) = 22,000). The foregoing procedure could have been avoided by inserting some of the isopressure lines from the infill (KK = 5) determination.

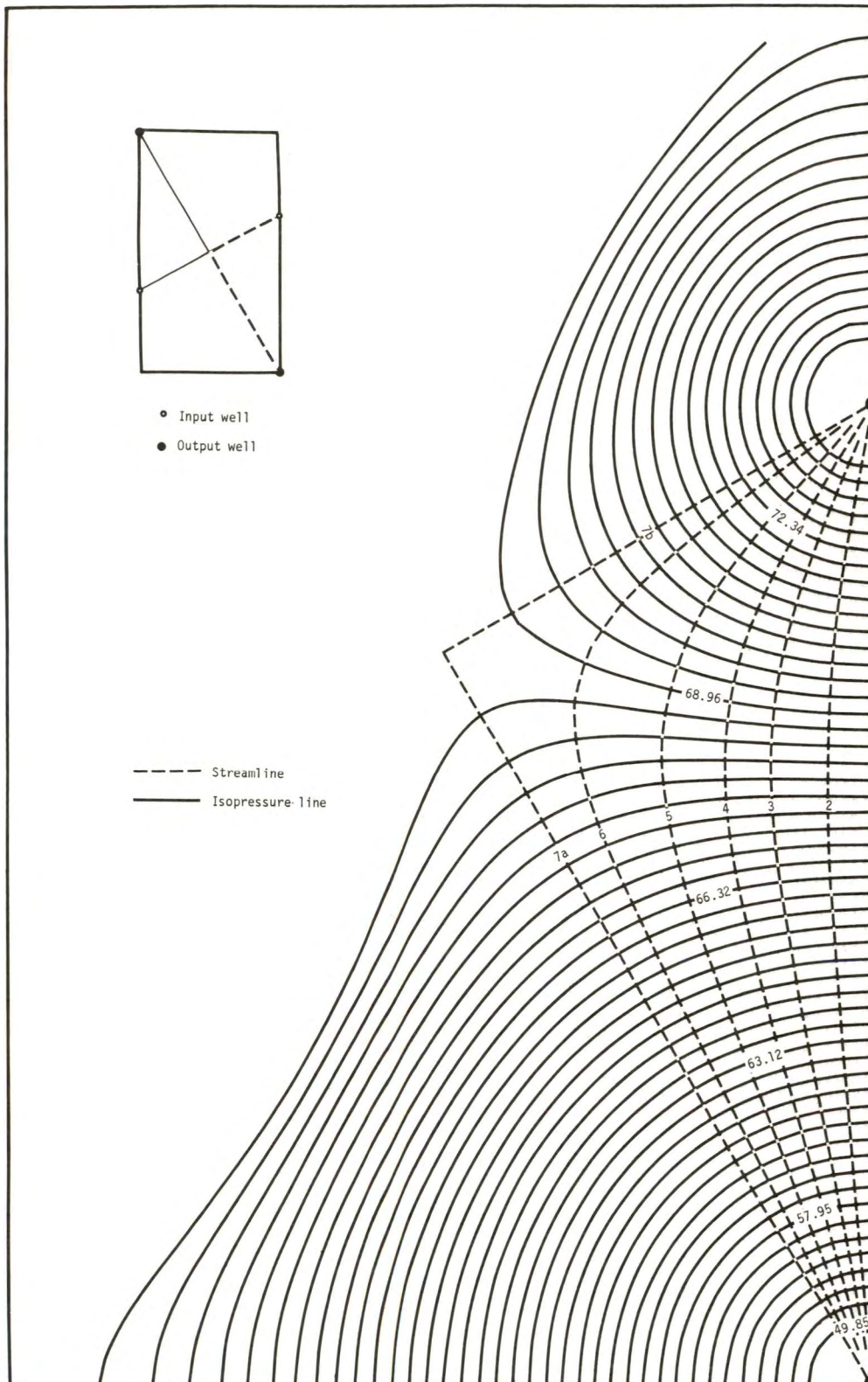


FIGURE 9. - Calculated Isopressure Lines and Streamlines for 7-Spot Element. Sketch in upper left corner shows relative locations of the wells.

It was done to illustrate the flexibility of the method and the use of plotting and restarting.

Two function subprograms used in subroutine STRM are listed in table 11.

#### Input Data and Results

The input data for determining isopressure lines are the pressures at points on a grid. For the example used in this paper, the pressures are on a 90- by 27-unit grid superimposed on a four-well pattern which is the smallest unit to produce a 7-spot element. The configuration is shown in the upper left hand section of figure 9. The pressures, shown in table 12, were calculated using a previously published method by the authors (5).

The x and y coordinates of each isopressure line calculated by the program are shown in table 13. The values are for the section started along the right side ( $KK = 1$ ) and cover the smallest unit, or element, of a 7-spot pattern. The pressure value, AVP, number of points on the isopressure line, ITAL, and the x and y coordinates of the beginning and end of the line are printed and punched on a "header" card before each set of coordinates. All these data are used as input to the streamline program.

Table 14 contains the coordinates of the streamlines determined by the streamline program. Streamline 1 is along the right vertical boundary and streamlines 2 through 6 move through the element upward and to the left. Streamline 7 is the dividing streamline between the element and its mirror images and is shown as 7a and 7b in its two-component, straight-line sections. The first value of 7b ( $x = 22.000$ ,  $y = 48.911$ ) is the dummy value and should be ignored. Figure 9 is a plot of the isopressure lines and streamlines for the element. The flow net obtained using these methods agrees well with that obtained by complex higher mathematics or by potentiometric models. For the example given in the report, the calculated flow net duplicated the published one (8) well within the accuracy of the potentiometric model.

The core storage required for the streamline program is 13,000 words, and the CPU time for the 7-spot example is 5 seconds on the CDC 6600.

TABLE 11. - Listings of function subprograms used in subroutine STRM<sup>1</sup>

```

FUNCTION TN ( A, R, X, V1, V2, B )
TN = ( X - A ) /      SQRT ( R**2 - (X-A)**2 )
IF ((V1+V2)/2.0 .GT. B ) TN = - TN
IF ( ABS(TN) .EQ. 0. )  TN = 0.1E-10

RETURN
END

```

```

FUNCTION YVALUE ( A, B, R, X, V1, V2 )
TERM =                SQRT ( R**2 - (X-A)**2 )
IF ((V1+V2)/2.0 .LE. B ) TERM = - TERM
YVALUE = B + TERM

RETURN
END

```

<sup>1</sup>These functions give values of first derivative (tangent) and ordinate for circle equation representing isopressure line.

TABLE 12. - Pressure input data for isopressure program

26.00	38.50	44.17	47.51	49.85	51.65	53.11	54.34	55.41	56.35	57.19	57.95	58.64	59.28	59.87	60.42	60.93	61.42	61.87	62.30
62.71	63.10	63.47	63.82	64.16	64.48	64.79	65.08	65.36	65.64	65.90	66.15	66.38	66.61	66.83	67.04	67.23	67.42	67.59	67.76
67.91	68.05	68.18	68.31	68.41	68.51	68.59	68.67	68.72	68.77	68.80	68.82	68.83							
38.50	41.92	45.33	48.02	50.12	51.81	53.22	54.42	55.47	56.39	57.23	57.98	58.67	59.30	59.89	60.44	60.95	61.43	61.89	62.31
62.72	63.11	63.48	63.83	64.17	64.49	64.80	65.09	65.37	65.64	65.90	66.15	66.39	66.61	66.83	67.04	67.24	67.42	67.60	67.76
67.92	68.06	68.19	68.31	68.42	68.51	68.60	68.67	68.73	68.78	68.81	68.83	68.84							
44.17	45.33	47.22	49.11	50.80	52.27	53.54	54.66	55.65	56.54	57.34	58.08	58.75	59.37	59.95	60.49	61.00	61.47	61.92	62.35
62.75	63.14	63.50	63.85	64.19	64.51	64.81	65.11	65.39	65.66	65.92	66.17	66.40	66.63	66.85	67.06	67.25	67.44	67.61	67.78
67.93	68.08	68.21	68.33	68.44	68.54	68.62	68.69	68.75	68.80	68.83	68.85	68.86							
47.51	48.02	49.11	50.40	51.70	52.91	54.02	55.02	55.94	56.77	57.53	58.23	58.89	59.49	60.05	60.58	61.07	61.54	61.99	62.40
62.80	63.18	63.55	63.89	64.23	64.54	64.85	65.14	65.42	65.69	65.95	66.19	66.43	66.66	66.88	67.08	67.28	67.46	67.64	67.80
67.96	68.10	68.24	68.36	68.47	68.56	68.65	68.72	68.78	68.83	68.86	68.88	68.89							
49.85	50.12	50.80	51.70	52.68	53.66	54.60	55.48	56.31	57.07	57.78	58.45	59.06	59.64	60.18	60.70	61.18	61.64	62.07	62.48
62.87	63.25	63.60	63.95	64.27	64.59	64.89	65.18	65.46	65.73	65.98	66.23	66.47	66.70	66.91	67.12	67.31	67.50	67.68	67.85
68.00	68.15	68.28	68.40	68.51	68.61	68.69	68.77	68.83	68.88	68.91	68.93	68.94							
51.65	51.81	52.27	52.91	53.66	54.45	55.24	56.00	56.73	57.43	58.08	58.70	59.28	59.83	60.35	60.84	61.31	61.75	62.18	62.58
62.96	63.33	63.68	64.02	64.34	64.65	64.95	65.24	65.51	65.78	66.03	66.28	66.52	66.74	66.96	67.16	67.36	67.55	67.73	67.89
68.05	68.19	68.33	68.45	68.57	68.66	68.75	68.83	68.89	68.93	68.97	68.99	69.00							
53.11	53.22	53.54	54.02	54.60	55.24	55.89	56.55	57.20	57.82	58.42	58.99	59.54	60.06	60.55	61.02	61.46	61.89	62.30	62.69
63.06	63.42	63.77	64.10	64.42	64.72	65.02	65.30	65.57	65.84	66.09	66.34	66.57	66.80	67.01	67.22	67.42	67.61	67.78	67.95
68.11	68.26	68.39	68.52	68.63	68.73	68.82	68.90	68.96	69.01	69.04	69.07	69.07							
54.34	54.42	54.66	55.02	55.48	56.00	56.55	57.12	57.69	58.24	58.79	59.31	59.82	60.30	60.77	61.21	61.64	62.05	62.44	62.82
63.19	63.53	63.87	64.19	64.51	64.81	65.10	65.38	65.65	65.91	66.16	66.40	66.64	66.86	67.08	67.29	67.49	67.67	67.85	68.02
68.18	68.33	68.47	68.60	68.71	68.81	68.91	68.98	69.05	69.10	69.13	69.15	69.16							
55.41	55.47	55.65	55.94	56.31	56.73	57.20	57.69	58.18	58.68	59.17	59.65	60.11	60.57	61.00	61.43	61.83	62.23	62.60	62.97
63.32	63.66	63.98	64.30	64.61	64.90	65.19	65.47	65.73	65.99	66.24	66.48	66.71	66.94	67.15	67.36	67.56	67.75	67.93	68.10
68.26	68.42	68.56	68.80	68.91	69.00	69.08	69.15	69.20	69.24	69.26	69.27								
56.35	56.40	56.54	56.77	57.07	57.43	57.82	58.24	58.68	59.12	59.56	60.00	60.43	60.85	61.26	61.65	62.04	62.41	62.78	63.13
63.47	63.79	64.11	64.42	64.72	65.01	65.29	65.56	65.82	66.08	66.33	66.57	66.80	67.02	67.24	67.45	67.65	67.84	68.02	68.19
68.36	68.51	68.66	68.79	68.91	69.02	69.11	69.19	69.26	69.31	69.35	69.38	69.39							
57.19	57.23	57.34	57.54	57.78	58.08	58.42	58.79	59.17	59.56	59.96	60.36	60.75	61.14	61.52	61.90	62.26	62.62	62.96	63.30
63.62	63.94	64.25	64.55	64.84	65.12	65.40	65.66	65.92	66.18	66.42	66.66	66.89	67.11	67.33	67.54	67.74	67.93	68.12	68.29
68.46	68.62	68.76	68.90	69.02	69.14	69.24	69.32	69.39	69.45	69.49	69.51	69.52							
57.95	57.98	58.08	58.24	58.45	58.70	58.99	59.31	59.65	60.00	60.36	60.72	61.08	61.44	61.80	62.14	62.49	62.82	63.16	63.48
63.79	64.09	64.39	64.68	64.97	65.24	65.51	65.77	66.03	66.28	66.52	66.76	66.99	67.21	67.43	67.64	67.84	68.04	68.23	68.40
68.57	68.73	68.89	69.03	69.16	69.27	69.37	69.46	69.54	69.59	69.64	69.66	69.67							
58.64	58.67	58.75	58.89	59.06	59.28	59.53	59.81	60.11	60.43	60.75	61.08	61.41	61.74	62.07	62.40	62.72	63.04	63.36	63.66
63.96	64.26	64.55	64.83	65.10	65.37	65.64	65.90	66.15	66.39	66.63	66.87	67.09	67.32	67.53	67.75	67.95	68.15	68.34	68.52
68.70	68.86	69.02	69.16	69.30	69.42	69.52	69.62	69.70	69.76	69.80	69.83	69.84							
59.28	59.30	59.37	59.49	59.64	59.83	60.05	60.30	60.56	60.84	61.14	61.44	61.74	62.05	62.36	62.66	62.97	63.27	63.57	63.86
64.15	64.43	64.71	64.98	65.25	65.51	65.77	66.02	66.27	66.51	66.75	66.98	67.21	67.43	67.65	67.86	68.07	68.27	68.46	68.65
68.83	69.00	69.16	69.31	69.45	69.58	69.69	69.79	69.87	69.94	69.99	70.01	70.03							
59.87	59.89	59.95	60.05	60.18	60.35	60.54	60.76	61.00	61.25	61.52	61.79	62.07	62.36	62.64	62.93	63.21	63.50	63.78	64.06
64.33	64.60	64.87	65.14	65.39	65.65	65.90	66.15	66.39	66.63	66.87	67.10	67.32	67.55	67.77	67.98	68.19	68.39	68.59	68.78
68.97	69.15	69.31	69.47	69.62	69.75	69.87	69.98	70.07	70.14	70.19	70.22	70.23							
60.42	60.44	60.49	60.58	60.70	60.84	61.02	61.21	61.42	61.65	61.89	62.14	62.40	62.66	62.93	63.19	63.46	63.73	64.00	64.26
64.52	64.78	65.04	65.29	65.55	65.79	66.04	66.28	66.52	66.76	66.99	67.22	67.45	67.67	67.89	68.10	68.32	68.52	68.73	68.92
69.12	69.30	69.48	69.64	69.80	69.94	70.07	70.18	70.28	70.36	70.41	70.45	70.46							
60.94	60.95	61.00	61.08	61.18	61.31	61.46	61.64	61.83	62.03	62.25	62.48	62.72	62.96	63.21	63.46	63.71	63.96	64.21	64.47
64.71	64.97	65.21	65.46	65.70	65.94	66.18	66.42	66.65	66.89	67.12	67.35	67.57	67.80	68.02	68.24	68.45	68.66	68.87	69.07
69.27	69.47	69.65	69.83	69.99	70.15	70.28	70.41	70.51	70.60	70.66	70.70	70.71							
61.42	61.44	61.48	61.54	61.64	61.75	61.89	62.04	62.22	62.40	62.60	62.81	63.03	63.25	63.49	63.72	63.96	64.19	64.43	64.67
64.91	65.15	65.39	65.62	65.86	66.09	66.33	66.56	66.79	67.02	67.25	67.47	67.70	67.92	68.15	68.37	68.59	68.80	69.02	69.23
69.43	69.63	69.83	70.02	70.20	70.36	70.51	70.65	70.77	70.86	70.93	70.97	70.98							

TABLE 12. - Pressure input data for isopressure program--Continued

61.88	61.89	61.93	61.99	62.07	62.18	62.30	62.44	62.59	62.77	62.95	63.14	63.34	63.55	63.76	63.98	64.20	64.42	64.63	64.88
65.10	65.33	65.56	65.79	66.02	66.25	66.47	66.70	66.93	67.15	67.38	67.60	67.83	68.05	68.28	68.50	68.72	68.95	69.17	69.39
69.60	69.81	70.02	70.22	70.41	70.59	70.76	70.91	71.04	71.14	71.22	71.27	71.28							
62.31	62.32	62.36	62.41	62.49	62.58	62.69	62.81	62.96	63.11	63.28	63.45	63.64	63.83	64.03	64.23	64.44	64.65	64.87	65.08
65.30	65.52	65.74	65.96	66.18	66.40	66.62	66.84	67.06	67.29	67.51	67.73	67.96	68.18	68.41	68.64	68.86	69.09	69.32	69.55
69.77	70.00	70.22	70.43	70.64	70.84	71.03	71.19	71.34	71.46	71.55	71.60	71.62							
62.72	62.74	62.76	62.81	62.88	62.96	63.06	63.18	63.31	63.45	63.60	63.76	63.93	64.11	64.30	64.49	64.68	64.88	65.08	65.29
65.49	65.70	65.91	66.12	66.34	66.55	66.77	66.98	67.20	67.42	67.64	67.86	68.09	68.31	68.54	68.77	69.00	69.24	69.47	69.71
69.94	70.18	70.42	70.65	70.88	71.10	71.31	71.50	71.66	71.80	71.91	71.97	71.99							
63.12	63.12	63.15	63.19	63.26	63.33	63.42	63.53	63.65	63.77	63.91	64.06	64.22	64.39	64.56	64.73	64.92	65.10	65.30	65.49
65.69	65.88	66.09	66.29	66.50	66.70	66.91	67.12	67.34	67.55	67.77	67.99	68.22	68.44	68.67	68.90	69.14	69.38	69.62	69.87
70.12	70.37	70.62	70.88	71.13	71.37	71.61	71.82	72.02	72.18	72.31	72.39	72.41							
63.49	63.50	63.52	63.56	63.62	63.69	63.77	63.86	63.97	64.09	64.22	64.36	64.50	64.65	64.81	64.98	65.15	65.33	65.50	65.69
65.87	66.07	66.26	66.45	66.65	66.85	67.05	67.26	67.47	67.68	67.90	68.12	68.34	68.57	68.80	69.03	69.27	69.52	69.77	70.03
70.29	70.56	70.83	71.11	71.38	71.65	71.92	72.17	72.40	72.60	72.75	72.85	72.88							
63.85	63.86	63.88	63.91	63.96	64.03	64.10	64.19	64.29	64.39	64.51	64.64	64.77	64.91	65.06	65.22	65.38	65.54	65.71	65.88
66.06	66.24	66.43	66.61	66.81	67.00	67.20	67.40	67.60	67.81	68.02	68.24	68.46	68.69	68.92	69.16	69.40	69.65	69.92	70.18
70.46	70.74	71.03	71.33	71.64	71.94	72.25	72.54	72.82	73.06	73.26	73.38	73.43							
64.19	64.20	64.22	64.25	64.30	64.36	64.42	64.50	64.59	64.69	64.80	64.91	65.04	65.17	65.31	65.45	65.60	65.76	65.91	66.08
66.24	66.42	66.59	66.77	66.95	67.14	67.33	67.53	67.73	67.93	68.14	68.36	68.58	68.80	69.03	69.28	69.52	69.78	70.05	70.33
70.61	70.92	71.23	71.55	71.89	72.24	72.58	72.94	73.27	73.58	73.82	73.99	74.05							
64.53	64.53	64.55	64.58	64.62	64.67	64.73	64.80	64.89	64.98	65.08	65.18	65.30	65.42	65.55	65.68	65.82	65.96	66.11	66.27
66.43	66.59	66.76	66.93	67.10	67.28	67.47	67.66	67.85	68.05	68.26	68.47	68.69	68.91	69.15	69.39	69.64	69.90	70.18	70.46
70.76	71.08	71.41	71.76	72.13	72.52	72.93	73.34	73.75	74.14	74.48	74.71	74.80							
64.85	64.85	64.87	64.90	64.93	64.98	65.03	65.10	65.17	65.26	65.34	65.44	65.55	65.66	65.78	65.90	66.03	66.17	66.30	66.45
66.60	66.76	66.91	67.08	67.24	67.42	67.60	67.78	67.97	68.16	68.36	68.57	68.79	69.01	69.24	69.49	69.74	70.01	70.29	70.58
70.89	71.23	71.58	71.96	72.36	72.79	73.25	73.75	74.25	74.76	75.23	75.58	75.72							
65.16	65.16	65.18	65.20	65.23	65.27	65.33	65.38	65.45	65.52	65.61	65.70	65.79	65.89	66.01	66.12	66.24	66.36	66.50	66.63
66.77	66.92	67.07	67.22	67.38	67.55	67.72	67.90	68.08	68.27	68.47	68.67	68.88	69.10	69.34	69.58	69.83	70.10	70.38	70.68
71.01	71.35	71.72	72.12	72.56	73.03	73.56	74.13	74.76	75.43	76.10	76.66	76.92							
65.46	65.46	65.47	65.50	65.52	65.56	65.61	65.66	65.72	65.79	65.86	65.95	66.03	66.13	66.22	66.33	66.44	66.56	66.68	66.81
66.94	67.08	67.22	67.36	67.52	67.68	67.84	68.01	68.19	68.37	68.56	68.76	68.97	69.19	69.42	69.66	69.91	70.18	70.46	70.77
71.09	71.45	71.83	72.25	72.71	73.23	73.81	74.47	75.22	76.10	77.07	78.05	78.64							
65.75	65.75	65.77	65.78	65.81	65.84	65.88	65.93	65.99	66.04	66.11	66.18	66.27	66.35	66.44	66.54	66.64	66.74	66.86	66.97
67.10	67.23	67.36	67.50	67.65	67.79	67.95	68.11	68.29	68.46	68.65	68.84	69.05	69.26	69.49	69.72	69.97	70.24	70.53	70.83
71.16	71.52	71.91	72.34	72.82	73.36	73.98	74.70	75.58	76.66	78.04	79.80	81.56							
66.04	66.04	66.05	66.07	66.09	66.12	66.15	66.20	66.24	66.30	66.35	66.42	66.49	66.57	66.65	66.74	66.83	66.93	67.03	67.14
67.25	67.37	67.50	67.63	67.77	67.91	68.06	68.22	68.38	68.55	68.73	68.92	69.11	69.32	69.54	69.77	70.02	70.28	70.56	70.87
71.19	71.55	71.94	72.38	72.86	73.41	74.04	74.79	75.72	76.92	78.64	81.56	88.00							
66.32	66.32	66.33	66.34	66.36	66.38	66.42	66.45	66.49	66.54	66.59	66.65	66.71	66.78	66.86	66.93	67.02	67.11	67.20	67.30
67.41	67.51	67.63	67.75	67.88	68.02	68.16	68.30	68.46	68.62	68.80	68.98	69.17	69.37	69.58	69.81	70.05	70.31	70.59	70.88
71.20	71.55	71.94	72.36	72.84	73.37	73.99	74.71	75.58	76.66	78.05	79.80	81.56							
66.59	66.59	66.60	66.61	66.63	66.65	66.67	66.71	66.74	66.78	66.82	66.88	66.93	66.99	67.05	67.13	67.20	67.28	67.36	67.46
67.55	67.65	67.76	67.87	67.99	68.12	68.25	68.39	68.54	68.69	68.86	69.03	69.21	69.41	69.61	69.83	70.07	70.32	70.58	70.87
71.18	71.52	71.89	72.30	72.75	73.26	73.83	74.48	75.23	76.10	77.07	78.04	78.64							
66.86	66.86	66.87	66.87	66.89	66.90	66.93	66.95	66.98	67.01	67.05	67.09	67.14	67.19	67.25	67.31	67.38	67.45	67.52	67.60
67.69	67.78	67.88	67.98	68.10	68.21	68.34	68.47	68.61	68.75	68.91	69.07	69.25	69.43	69.63	69.84	70.07	70.30	70.56	70.84
71.14	71.46	71.81	72.19	72.61	73.07	73.59	74.15	74.71	75.43	76.10	76.66	76.92							
67.12	67.13	67.13	67.14	67.15	67.16	67.17	67.20	67.22	67.25	67.28	67.31	67.35	67.39	67.44	67.49	67.55	67.61	67.67	67.75
67.82	67.91	68.00	68.09	68.19	68.30	68.41	68.54	68.67	68.81	68.95	69.11	69.27	69.45	69.63	69.84	70.05	70.28	70.52	70.78
71.06	71.37	71.69	72.05	72.43	72.84	73.29	73.77	74.27	74.77	75.23	75.58	75.71							
67.39	67.39	67.39	67.39	67.40	67.41	67.42	67.44	67.45	67.47	67.50	67.52	67.55	67.59	67.63	67.67	67.72	67.77	67.83	67.89
67.95	68.03	68.11	68.19	68.28	68.38	68.49	68.60	68.72	68.85	68.99	69.13	69.29	69.45	69.63	69.82	70.02	70.23	70.46	70.71
70.97	71.25	71.55	71.87	72.22	72.58	72.97	73.36	73.76	74.14	74.47	74.70	74.79							
67.65	67.65	67.65	67.65	67.65	67.66	67.66	67.67	67.68	67.70	67.71	67.73	67.75	67.78	67.81	67.84	67.88	67.92	67.97	68.02
68.08	68.14	68.21	68.29	68.37	68.46	68.55	68.66	68.76	68.88	69.01	69.15	69.29	69.45	69.61	69.79	69.97	70.17	70.39	70.62
70.86	71.12	71.39	71.68	71.98	72.30	72.63	72.96	73.27	73.57	73.81	73.97	74.03							



TABLE 12. - Pressure input data for isopressure program--Continued

74.79	74.70	74.47	74.14	73.76	73.36	72.97	72.58	72.22	71.87	71.55	71.25	70.97	70.71	70.46	70.23	70.02	69.82	69.63	69.45
69.29	69.13	68.99	68.85	68.72	68.60	68.49	68.38	68.28	68.19	68.11	68.03	67.95	67.89	67.83	67.77	67.72	67.67	67.63	67.59
67.55	67.52	67.50	67.47	67.45	67.44	67.42	67.41	67.40	67.39	67.39	67.39	67.39	67.39	67.39	67.39	67.39	67.39	67.39	67.39
75.71	75.58	75.23	74.77	74.27	73.77	73.29	72.84	72.43	72.05	71.69	71.37	71.06	70.78	70.52	70.28	70.05	69.84	69.63	69.45
69.27	69.11	68.95	68.81	68.67	68.54	68.41	68.30	68.19	68.09	68.00	67.91	67.82	67.75	67.67	67.61	67.55	67.49	67.44	67.39
67.35	67.31	67.28	67.25	67.22	67.20	67.17	67.16	67.15	67.14	67.13	67.13	67.12	67.12	67.12	67.12	67.12	67.12	67.12	67.12
76.92	76.66	76.10	75.43	74.77	74.15	73.59	73.07	72.61	72.19	71.81	71.46	71.14	70.84	70.56	70.30	70.07	69.84	69.63	69.43
69.25	69.07	68.91	68.75	68.61	68.47	68.34	68.21	68.10	67.99	67.88	67.78	67.69	67.60	67.52	67.45	67.38	67.31	67.25	67.19
67.14	67.09	67.05	67.01	66.98	66.95	66.93	66.90	66.89	66.87	66.87	66.86	66.86	66.86	66.86	66.86	66.86	66.86	66.86	66.86
78.64	78.04	77.07	76.10	75.23	74.48	73.83	73.26	72.75	72.30	71.89	71.52	71.18	70.87	70.58	70.32	70.07	69.83	69.61	69.41
69.21	69.03	68.86	68.69	68.54	68.39	68.25	68.12	67.99	67.87	67.76	67.65	67.55	67.46	67.36	67.28	67.20	67.13	67.05	66.99
66.93	66.88	66.82	66.78	66.74	66.71	66.67	66.65	66.63	66.61	66.60	66.59	66.59	66.59	66.59	66.59	66.59	66.59	66.59	66.59
81.56	79.80	73.05	76.66	75.58	74.71	73.99	73.37	72.84	72.36	71.94	71.55	71.20	70.88	70.59	70.31	70.05	69.81	69.58	69.37
69.17	68.98	68.80	68.62	68.46	68.30	68.16	68.02	67.88	67.75	67.63	67.51	67.41	67.30	67.20	67.11	67.02	66.93	66.86	66.78
66.71	66.65	66.59	66.54	66.49	66.45	66.42	66.38	66.36	66.34	66.33	66.32	66.32	66.32	66.32	66.32	66.32	66.32	66.32	66.32
88.00	81.56	78.64	76.92	75.72	74.79	74.04	73.41	72.86	72.38	71.94	71.55	71.19	70.87	70.56	70.28	70.02	69.77	69.54	69.32
69.11	68.92	68.73	68.55	68.38	68.22	68.06	67.91	67.77	67.63	67.50	67.37	67.25	67.14	67.03	66.93	66.83	66.74	66.65	66.57
66.49	66.42	66.35	66.30	66.24	66.20	66.15	66.12	66.09	66.07	66.05	66.04	66.04	66.04	66.04	66.04	66.04	66.04	66.04	66.04
81.56	79.80	78.04	76.66	75.58	74.70	73.98	73.36	72.82	72.34	71.91	71.52	71.16	70.83	70.53	70.24	69.97	69.72	69.49	69.26
69.05	68.84	68.65	68.46	68.29	68.11	67.95	67.79	67.65	67.50	67.36	67.23	67.10	66.97	66.86	66.74	66.64	66.54	66.44	66.35
66.27	66.18	66.11	66.04	65.99	65.93	65.88	65.84	65.81	65.78	65.77	65.75	65.75	65.75	65.75	65.75	65.75	65.75	65.75	65.75
78.64	78.05	77.07	76.10	75.22	74.47	73.81	73.23	72.71	72.25	71.83	71.45	71.09	70.77	70.46	70.18	69.91	69.66	69.42	69.19
68.97	68.76	68.56	68.37	68.19	68.01	67.84	67.68	67.52	67.36	67.22	67.08	66.94	66.81	66.68	66.56	66.44	66.33	66.22	66.13
66.03	65.95	65.86	65.79	65.72	65.66	65.61	65.56	65.52	65.50	65.47	65.46	65.46	65.46	65.46	65.46	65.46	65.46	65.46	65.46
76.92	76.66	76.10	75.43	74.76	74.13	73.56	73.03	72.56	72.12	71.72	71.35	71.01	70.68	70.38	70.10	69.83	69.58	69.34	69.10
68.88	68.67	68.47	68.27	68.08	67.90	67.72	67.55	67.38	67.22	67.07	66.92	66.77	66.63	66.50	66.36	66.24	66.12	66.01	65.89
65.79	65.70	65.61	65.52	65.45	65.38	65.33	65.27	65.23	65.20	65.18	65.16	65.16	65.16	65.16	65.16	65.16	65.16	65.16	65.16
75.72	75.58	75.23	74.76	74.25	73.75	73.25	72.79	72.36	71.96	71.58	71.23	70.89	70.58	70.29	70.01	69.74	69.49	69.24	69.01
68.79	68.57	68.36	68.16	67.97	67.78	67.60	67.42	67.24	67.08	66.91	66.76	66.60	66.45	66.30	66.17	66.03	65.90	65.78	65.66
65.55	65.44	65.34	65.26	65.17	65.10	65.03	64.98	64.93	64.90	64.87	64.85	64.85	64.85	64.85	64.85	64.85	64.85	64.85	64.85
74.80	74.71	74.48	74.14	73.75	73.34	72.93	72.52	72.13	71.76	71.41	71.08	70.76	70.46	70.18	69.90	69.64	69.39	69.15	68.91
68.69	68.47	68.26	68.05	67.85	67.66	67.47	67.28	67.10	66.93	66.76	66.59	66.43	66.27	66.11	65.96	65.82	65.68	65.55	65.42
65.30	65.18	65.08	64.98	64.89	64.80	64.73	64.67	64.62	64.58	64.55	64.53	64.53	64.53	64.53	64.53	64.53	64.53	64.53	64.53
74.05	73.99	73.82	73.58	73.27	72.94	72.58	72.24	71.89	71.55	71.23	70.92	70.61	70.33	70.05	69.78	69.52	69.28	69.03	68.80
68.58	68.36	68.14	67.93	67.73	67.53	67.33	67.14	66.95	66.77	66.59	66.42	66.24	66.08	65.91	65.76	65.60	65.45	65.31	65.17
65.04	64.91	64.80	64.69	64.59	64.50	64.42	64.36	64.30	64.25	64.22	64.20	64.19	64.19	64.19	64.19	64.19	64.19	64.19	64.19
73.43	73.38	73.26	73.06	72.82	72.54	72.25	71.94	71.64	71.33	71.03	70.74	70.46	70.18	69.92	69.65	69.40	69.16	68.92	68.69
68.46	68.24	68.02	67.81	67.60	67.40	67.20	67.00	66.81	66.61	66.43	66.24	66.06	65.88	65.71	65.54	65.38	65.22	65.06	64.91
64.77	64.64	64.51	64.39	64.29	64.19	64.10	64.03	63.96	63.91	63.88	63.86	63.85	63.85	63.85	63.85	63.85	63.85	63.85	63.85
72.88	72.85	72.75	72.60	72.40	72.17	71.92	71.65	71.38	71.11	70.83	70.56	70.29	70.03	69.77	69.52	69.27	69.03	68.80	68.57
68.34	68.12	67.90	67.68	67.47	67.26	67.05	66.85	66.65	66.45	66.26	66.07	65.87	65.69	65.50	65.33	65.15	64.98	64.81	64.65
64.50	64.36	64.22	64.09	63.97	63.86	63.77	63.69	63.62	63.56	63.52	63.50	63.49	63.49	63.49	63.49	63.49	63.49	63.49	63.49
72.41	72.39	72.31	72.18	72.02	71.82	71.61	71.37	71.13	70.88	70.62	70.37	70.12	69.87	69.62	69.38	69.14	68.90	68.67	68.44
68.22	67.99	67.77	67.55	67.34	67.12	66.91	66.70	66.50	66.29	66.09	65.88	65.69	65.49	65.30	65.10	64.92	64.73	64.56	64.39
64.22	64.06	63.91	63.77	63.65	63.53	63.42	63.33	63.26	63.19	63.15	63.12	63.12	63.12	63.12	63.12	63.12	63.12	63.12	63.12
71.99	71.97	71.91	71.80	71.66	71.50	71.31	71.10	70.88	70.65	70.42	70.18	69.94	69.71	69.47	69.24	69.00	68.77	68.54	68.31
68.09	67.86	67.64	67.42	67.20	66.98	66.77	66.55	66.34	66.12	65.91	65.70	65.49	65.29	65.08	64.88	64.68	64.49	64.30	64.11
63.93	63.76	63.60	63.45	63.31	63.18	63.06	62.96	62.88	62.81	62.76	62.74	62.72	62.72	62.72	62.72	62.72	62.72	62.72	62.72
71.62	71.60	71.55	71.46	71.34	71.19	71.03	70.84	70.64	70.43	70.22	70.00	69.77	69.55	69.32	69.09	68.86	68.64	68.41	68.18
67.96	67.73	67.51	67.29	67.06	66.84	66.62	66.40	66.18	65.96	65.74	65.52	65.30	65.08	64.87	64.65	64.44	64.23	64.03	63.83
63.64	63.45	63.28	63.11	62.96	62.81	62.69	62.58	62.49	62.41	62.36	62.32	62.31	62.31	62.31	62.31	62.31	62.31	62.31	62.31
71.28	71.27	71.22	71.14	71.04	70.91	70.76	70.59	70.41	70.22	70.02	69.81	69.60	69.39	69.17	68.95	68.72	68.50	68.28	68.05
67.83	67.60	67.38	67.15	66.93	66.70	66.47	66.25	66.02	65.79	65.56	65.33	65.10	64.88	64.65	64.42	64.20	63.98	63.76	63.55
63.34	63.14	62.95	62.77	62.59	62.44	62.30	62.18	62.07	61.99	61.93	61.89	61.88	61.88	61.88	61.88	61.88	61.88	61.88	61.88

TABLE 12. - Pressure input data for isopressure program--Continued

70.98	70.97	70.93	70.86	70.77	70.65	70.51	70.36	70.20	70.02	69.83	69.63	69.43	69.23	69.02	68.80	68.59	68.37	68.15	67.92
67.70	67.47	67.25	67.02	66.79	66.56	66.33	66.09	65.86	65.62	65.39	65.15	64.91	64.67	64.43	64.19	63.96	63.72	63.49	63.25
63.03	62.81	62.60	62.40	62.22	62.04	61.89	61.75	61.64	61.54	61.48	61.44	61.42							
70.71	70.70	70.66	70.60	70.51	70.41	70.28	70.15	69.99	69.83	69.65	69.47	69.27	69.07	68.87	68.66	68.45	68.24	68.02	67.80
67.57	67.35	67.12	66.89	66.65	66.42	66.18	65.94	65.70	65.46	65.21	64.97	64.71	64.47	64.21	63.96	63.71	63.46	63.21	62.96
62.72	62.48	62.25	62.03	61.83	61.64	61.46	61.31	61.18	61.08	61.00	60.95	60.94							
70.46	70.45	70.41	70.36	70.28	70.18	70.07	69.94	69.80	69.64	69.48	69.30	69.12	68.92	68.73	68.52	68.32	68.10	67.89	67.67
67.45	67.22	66.99	66.76	66.52	66.28	66.04	65.79	65.55	65.29	65.04	64.78	64.52	64.26	64.00	63.73	63.46	63.19	62.93	62.66
62.40	62.14	61.89	61.65	61.42	61.21	61.02	60.84	60.70	60.58	60.49	60.44	60.42							
70.23	70.22	70.19	70.14	70.07	69.98	69.87	69.75	69.62	69.47	69.31	69.15	68.97	68.78	68.59	68.39	68.19	67.98	67.77	67.55
67.32	67.10	66.87	66.63	66.39	66.15	65.90	65.65	65.39	65.14	64.87	64.60	64.33	64.06	63.78	63.50	63.21	62.93	62.64	62.36
62.07	61.79	61.52	61.25	61.00	60.76	60.54	60.35	60.18	60.05	59.95	59.89	59.87							
70.03	70.01	69.99	69.94	69.87	69.79	69.69	69.58	69.45	69.31	69.16	69.00	68.83	68.65	68.46	68.27	68.07	67.86	67.65	67.43
67.21	66.98	66.75	66.51	66.27	66.02	65.77	65.51	65.25	64.98	64.71	64.43	64.15	63.86	63.57	63.27	62.97	62.66	62.36	62.05
61.74	61.44	61.14	60.84	60.56	60.30	60.05	59.83	59.64	59.49	59.37	59.30	59.28							
69.84	69.83	69.80	69.76	69.70	69.62	69.52	69.42	69.30	69.16	69.02	68.86	68.70	68.52	68.34	68.15	67.95	67.75	67.53	67.32
67.09	66.87	66.63	66.39	66.15	65.90	65.64	65.37	65.10	64.83	64.55	64.26	63.96	63.66	63.36	63.04	62.72	62.40	62.07	61.74
61.41	61.08	60.75	60.43	60.11	59.81	59.53	59.28	59.06	58.89	58.75	58.67	58.64							
69.67	69.66	69.64	69.59	69.54	69.46	69.37	69.27	69.16	69.03	68.89	68.73	68.57	68.40	68.23	68.04	67.84	67.64	67.43	67.21
66.99	66.76	66.52	66.28	66.03	65.77	65.51	65.24	64.97	64.68	64.39	64.09	63.79	63.48	63.16	62.82	62.49	62.14	61.80	61.44
61.08	60.72	60.36	60.00	59.65	59.31	58.99	58.70	58.45	58.24	58.08	57.98	57.95							
69.52	69.51	69.49	69.45	69.39	69.32	69.24	69.14	69.02	68.90	68.76	68.62	68.46	68.29	68.12	67.93	67.74	67.54	67.33	67.11
66.89	66.66	66.42	66.18	65.92	65.66	65.40	65.12	64.84	64.55	64.25	63.94	63.62	63.30	62.96	62.62	62.26	61.90	61.52	61.14
60.75	60.36	59.96	59.56	59.17	58.79	58.42	58.08	57.78	57.54	57.34	57.23	57.19							
69.39	69.38	69.35	69.31	69.26	69.19	69.11	69.02	68.91	68.79	68.66	68.51	68.36	68.19	68.02	67.84	67.65	67.45	67.24	67.02
66.80	66.57	66.33	66.08	65.82	65.56	65.29	65.01	64.72	64.42	64.11	63.79	63.47	63.13	62.78	62.41	62.04	61.65	61.26	60.85
60.43	60.00	59.56	59.12	58.68	58.24	57.82	57.43	57.07	56.77	56.54	56.40	56.35							
69.27	69.26	69.24	69.20	69.15	69.08	69.00	68.91	68.80	68.69	68.56	68.42	68.26	68.10	67.93	67.75	67.56	67.36	67.15	66.94
66.71	66.48	66.24	65.99	65.73	65.47	65.19	64.90	64.61	64.30	63.98	63.66	63.32	62.97	62.60	62.23	61.83	61.43	61.00	60.57
60.11	59.65	59.17	58.68	58.18	57.69	57.20	56.73	56.31	55.94	55.65	55.47	55.41							
69.16	69.15	69.13	69.10	69.05	68.98	68.91	68.81	68.71	68.60	68.47	68.33	68.18	68.02	67.85	67.67	67.49	67.29	67.08	66.86
66.64	66.40	66.16	65.91	65.65	65.38	65.10	64.81	64.51	64.19	63.87	63.53	63.19	62.82	62.44	62.05	61.64	61.21	60.77	60.30
59.82	59.31	58.79	58.24	57.69	57.12	56.55	56.00	55.48	55.02	54.66	54.42	54.34							
69.07	69.07	69.04	69.01	68.96	68.90	68.82	68.73	68.63	68.52	68.39	68.26	68.11	67.95	67.78	67.61	67.42	67.22	67.01	66.80
66.57	66.34	66.09	65.84	65.57	65.30	65.02	64.72	64.42	64.10	63.77	63.42	63.06	62.69	62.30	61.89	61.46	61.02	60.55	60.06
59.54	58.99	58.42	57.82	57.20	56.55	55.89	55.24	54.60	54.02	53.54	53.22	53.11							
69.00	68.99	68.97	68.93	68.89	68.83	68.75	68.66	68.57	68.45	68.33	68.19	68.05	67.89	67.73	67.55	67.36	67.16	66.96	66.74
66.52	66.28	66.03	65.78	65.51	65.24	64.95	64.65	64.34	64.02	63.68	63.33	62.96	62.58	62.18	61.75	61.31	60.84	60.35	59.83
59.28	58.70	58.08	57.43	56.73	56.00	55.24	54.45	53.66	52.91	52.27	51.81	51.65							
68.94	68.93	68.91	68.88	68.83	68.77	68.69	68.61	68.51	68.40	68.28	68.15	68.00	67.85	67.68	67.50	67.31	67.12	66.91	66.70
66.47	66.23	65.98	65.73	65.46	65.18	64.89	64.59	64.27	63.95	63.60	63.25	62.87	62.48	62.07	61.64	61.18	60.70	60.18	59.64
59.06	58.45	57.78	57.07	56.31	55.48	54.60	53.66	52.68	51.70	50.80	50.12	49.85							
68.89	68.88	68.86	68.83	68.78	68.72	68.65	68.56	68.47	68.36	68.24	68.10	67.96	67.80	67.64	67.46	67.28	67.08	66.88	66.66
66.43	66.19	65.95	65.69	65.42	65.14	64.85	64.54	64.23	63.89	63.55	63.18	62.80	62.40	61.99	61.54	61.07	60.58	60.05	59.49
58.89	58.23	57.53	56.77	55.94	55.02	54.02	52.91	51.70	50.40	49.11	48.02	47.51							
68.86	68.85	68.83	68.80	68.75	68.69	68.62	68.54	68.44	68.33	68.21	68.08	67.93	67.78	67.61	67.44	67.25	67.06	66.85	66.63
66.40	66.17	65.92	65.66	65.39	65.11	64.81	64.51	64.19	63.85	63.50	63.14	62.75	62.35	61.92	61.47	61.00	60.49	59.95	59.37
58.75	58.08	57.34	56.54	55.65	54.66	53.54	52.27	50.80	49.11	47.22	45.33	44.17							
68.84	68.83	68.81	68.78	68.73	68.67	68.60	68.51	68.42	68.31	68.19	68.06	67.92	67.76	67.60	67.42	67.24	67.04	66.83	66.61
66.39	66.15	65.90	65.64	65.37	65.09	64.80	64.49	64.17	63.83	63.48	63.11	62.72	62.31	61.89	61.43	60.95	60.44	59.89	59.30
58.67	57.98	57.23	56.39	55.47	54.42	53.22	51.81	50.12	48.02	45.33	41.92	38.50							
68.83	68.82	68.80	68.77	68.72	68.67	68.59	68.51	68.41	68.31	68.18	68.05	67.91	67.76	67.59	67.42	67.23	67.04	66.83	66.61
66.38	66.15	65.90	65.64	65.36	65.08	64.79	64.48	64.16	63.82	63.47	63.10	62.71	62.30	61.87	61.42	60.93	60.42	59.87	59.28
58.64	57.95	57.19	56.35	55.41	54.34	53.11	51.65	49.85	47.51	44.17	38.50	26.00							

TABLE 13. - Input data for streamline program<sup>1</sup>

RIGHT SIDE										
38.50000	2	53.000	90.000	52.000	91.000					
53.000		90.000	52.000	91.000						
44.17000	3	53.000	89.000	51.000	91.000					
53.000		89.000	52.000	89.365	51.000	91.000				
47.51000	4	53.000	88.000	50.000	91.000					
53.000		88.000	52.000	88.208	51.000	88.853	50.000	91.000		
49.85000	6	53.000	87.000	49.000	91.000					
53.000		87.000	52.000	87.140	51.000	87.578	50.000	88.425	49.578	89.000
49.000		91.000								
51.65000	7	53.000	86.000	48.000	91.000					
53.000		86.000	52.000	86.102	51.000	86.439	50.000	87.040	49.000	88.053
48.439		89.000	48.000	91.000						
53.11000	8	53.000	85.000	47.000	91.000					
53.000		85.000	52.000	85.084	51.000	85.352	50.000	85.827	49.000	86.566
48.000		87.728	47.352	89.000	47.000	91.000				
54.34000	10	53.000	84.000	46.000	91.000					
53.000		84.000	52.000	84.071	51.000	84.298	50.000	84.689	49.000	85.283
48.000		86.139	47.000	87.436	46.689	88.000	46.298	89.000	46.000	91.000
55.41000	11	53.000	83.000	45.000	91.000					
53.000		83.000	52.000	83.060	51.000	83.252	50.000	83.588	49.000	84.082
48.000		84.780	47.000	85.737	46.000	87.144	45.588	88.000	45.252	89.000
45.000		91.000								
56.35000	12	53.000	82.000	44.000	91.000					
53.000		82.000	52.000	82.057	51.000	82.222	50.000	82.515	49.000	82.949
48.000		83.526	47.000	84.305	46.000	85.359	45.000	86.899	44.517	88.000
44.222		89.000	44.000	91.000						
57.19000	13	53.000	81.000	43.000	91.000					
53.000		81.000	52.000	81.051	51.000	81.193	50.000	81.466	49.000	81.835
48.000		82.351	47.000	83.016	46.000	83.879	45.000	85.021	44.000	86.657
43.457		88.000	43.193	89.000	43.000	91.000				
57.95000	15	53.000	80.000	42.000	91.000					
53.000		80.000	52.000	80.042	51.000	80.183	50.000	80.423	49.000	80.755
48.000		81.204	47.000	81.788	46.000	82.527	45.000	83.467	44.000	84.685
43.000		86.417	42.755	87.000	42.407	88.000	42.183	89.000	42.000	91.000
58.64000	17	53.000	79.000	41.000	91.000					
53.000		79.000	52.000	79.045	51.000	79.169	50.000	79.394	49.000	79.694
48.000		80.100	47.000	80.620	46.000	81.278	45.000	82.081	44.000	83.091
43.000		84.402	42.618	85.000	42.000	86.226	41.694	87.000	41.390	88.000
41.169		89.000	41.000	91.000						
59.28000	17	53.000	78.000	40.000	91.000					
53.000		78.000	52.000	78.033	51.000	78.149	50.000	78.358	49.000	78.629
48.000		79.000	47.000	79.468	46.000	80.059	45.000	80.774	44.000	81.636
43.000		82.715	42.000	84.091	41.000	86.000	40.629	87.000	40.358	88.000
40.149		89.000	40.000	91.000						
59.87000	18	53.000	77.000	39.000	91.000					
53.000		77.000	52.000	77.035	51.000	77.142	50.000	77.327	49.000	77.579
48.000		77.925	47.000	78.353	46.000	78.881	45.000	79.524	44.000	80.298
43.000		81.225	42.000	82.368	41.000	83.820	40.000	85.823	39.579	87.000
39.327		88.000	39.142	89.000	39.000	91.000				
60.42000	19	53.000	76.000	38.000	91.000					
53.000		76.000	52.000	76.038	51.000	76.133	50.000	76.308	49.000	76.548
48.000		76.860	47.000	77.247	46.000	77.741	45.000	78.314	44.000	79.024
43.000		79.846	42.000	80.833	41.000	82.031	40.000	83.551	39.000	85.638
38.548		87.000	38.310	88.000	38.133	89.000	38.000	91.000		
60.94600	23	53.000	75.000	36.980	91.000					
53.000		75.000	52.000	75.020	51.000	75.121	50.000	75.288	49.000	75.505
48.000		75.792	47.000	76.173	46.000	76.605	45.000	77.139	44.000	77.758
43.000		78.516	42.000	79.389	41.000	80.424	40.000	81.686	39.000	83.249
38.616		84.000	38.000	85.438	37.742	86.000	37.505	87.000	37.269	88.000
37.122		89.000	37.000	90.333	36.980	91.000				
61.42000	24	53.000	74.000	36.000	91.000					
53.000		74.000	52.000	74.042	51.000	74.128	50.000	74.263	49.000	74.486
48.000		74.752	47.000	75.092	46.000	75.520	45.000	76.000	44.000	76.581
43.000		77.266	42.000	78.056	41.000	78.970	40.000	80.067	39.000	81.376
38.590		82.000	38.000	83.045	37.517	84.000	37.000	85.248	36.752	86.000
36.486		87.000	36.259	88.000	36.108	89.000	36.000	91.000		

<sup>1</sup>First card in each group contains pressure value and x and y coordinates at beginning and ending of isopressure line. Remaining cards contain alternating x and y values for all points on isopressure line.



TABLE 13. - Input data for streamline program--Continued

65.46000	38	53.000	63.000	24.651	91.000				
53.000	63.000	52.000	63.000	51.000	63.034	50.000	63.137	49.000	63.207
48.000	63.349	47.000	63.540	46.000	63.718	45.000	63.963	44.000	64.227
43.000	64.565	42.000	64.924	41.000	65.365	40.000	65.836	39.000	66.380
38.000	66.957	37.000	67.636	36.000	68.375	35.000	69.196	34.000	70.150
33.000	71.154	32.000	72.322	31.000	73.581	30.000	75.000	29.000	76.570
28.000	78.357	27.671	79.000	27.000	80.432	26.769	81.000	26.375	82.000
26.000	83.111	25.798	84.000	25.407	85.000	25.000	87.000	24.854	88.000
24.744	89.000	24.671	90.000	24.651	91.000				
65.75000	39	53.000	62.000	23.582	91.000				
53.000	62.000	52.000	62.000	51.000	62.069	50.000	62.105	49.000	62.210
48.000	62.321	47.000	62.481	46.000	62.667	45.000	62.892	44.000	63.153
43.000	63.440	42.000	63.806	41.000	64.167	40.000	64.603	39.000	65.130
38.000	65.682	37.000	66.323	36.000	67.048	35.000	67.800	34.000	68.678
33.000	69.660	32.000	70.717	31.000	71.940	30.000	73.235	29.000	74.688
28.000	76.279	27.600	77.000	27.000	78.154	26.582	79.000	26.000	80.169
25.654	81.000	25.000	82.768	24.620	84.000	24.342	85.000	24.000	86.576
23.776	88.000	23.658	89.000	23.582	90.000	23.582	91.000		
66.04000	39	53.000	61.000	22.450	91.000				
53.000	61.000	52.000	61.000	51.000	61.036	50.000	61.107	49.000	61.181
48.000	61.293	47.000	61.407	46.000	61.601	45.000	61.800	44.000	62.000
43.000	62.284	42.000	62.603	41.000	62.960	40.000	63.385	39.000	63.854
38.000	64.369	37.000	64.953	36.000	65.630	35.000	66.356	34.000	67.204
33.000	68.108	32.000	69.165	31.000	70.283	30.000	71.492	29.000	72.875
28.000	74.326	27.000	76.000	26.000	77.846	25.000	79.917	24.548	81.000
24.000	82.431	23.803	83.000	23.485	84.000	23.000	85.821	22.764	87.000
22.625	88.000	22.530	89.000	22.445	90.000	22.450	91.000		
66.32000	41	53.000	60.000	21.261	91.000				
53.000	60.000	52.000	60.000	51.000	60.036	50.000	60.074	49.000	60.148
48.000	60.227	47.000	60.379	46.000	60.515	45.000	60.680	44.000	60.917
43.000	61.125	42.000	61.422	41.000	61.773	40.000	62.136	39.000	62.551
38.000	63.048	37.000	63.600	36.000	64.206	35.000	64.904	34.000	65.722
33.000	66.592	32.000	67.562	31.000	68.654	30.000	69.812	29.000	71.125
28.000	72.533	27.000	74.069	26.000	75.714	25.000	77.573	24.000	79.626
23.417	81.000	23.000	82.111	22.671	83.000	22.333	84.000	22.000	85.333
21.839	86.000	21.630	87.000	21.464	88.000	21.348	89.000	21.300	90.000
21.261	91.000								
66.59000	43	53.000	59.000	20.089	91.000				
53.000	59.000	52.000	59.000	51.000	59.037	50.000	59.075	49.000	59.151
48.000	59.229	47.000	59.316	46.000	59.471	45.000	59.605	44.000	59.795
43.000	60.000	42.000	60.261	41.000	60.545	40.000	60.905	39.000	61.286
38.000	61.755	37.000	62.255	36.000	62.829	35.000	63.500	34.000	64.222
33.000	65.059	32.000	66.000	31.000	67.000	30.000	68.125	29.000	69.392
28.000	70.733	27.000	72.200	26.000	73.786	25.000	75.452	24.713	76.000
24.000	77.324	23.671	78.000	23.000	79.353	22.713	80.000	22.000	81.768
21.522	83.000	21.000	84.714	20.682	86.000	20.489	87.000	20.309	88.000
20.177	89.000	20.091	90.000	20.089	91.000				
66.86000	44	53.000	58.000	18.863	91.000				
53.000	58.000	52.000	58.000	51.000	58.038	50.000	58.038	49.000	58.115
48.000	58.157	47.000	58.277	46.000	58.370	45.000	58.500	44.000	58.647
43.000	58.826	42.000	59.091	41.000	59.323	40.000	59.625	39.000	60.000
38.000	60.362	37.000	60.846	36.000	61.375	35.000	62.000	34.000	62.681
33.000	63.478	32.000	64.375	31.000	65.326	30.000	66.445	29.000	67.635
28.000	68.935	27.000	70.357	26.000	71.857	25.000	73.509	24.000	75.231
23.565	76.000	23.000	77.083	22.522	78.000	22.000	79.091	21.571	80.000
21.000	81.321	20.727	82.000	20.000	84.000	19.714	85.000	19.466	86.000
19.238	87.000	19.000	88.667	18.860	90.000	18.863	91.000		
67.12000	43	53.000	57.000	17.579	91.000				
53.000	57.000	52.000	57.038	51.000	57.038	50.000	57.077	49.000	57.117
48.000	57.156	47.000	57.205	46.000	57.324	45.000	57.422	44.000	57.552
43.000	57.700	42.000	57.866	41.000	58.095	40.000	58.350	39.000	58.656
38.000	59.052	37.000	59.444	36.000	59.941	35.000	60.478	34.000	61.121
33.000	61.463	32.000	62.740	31.000	63.674	30.000	64.714	29.000	65.857
28.000	67.143	27.000	68.550	26.000	70.000	25.000	71.571	24.000	73.224
23.000	75.000	22.000	76.827	21.000	78.758	20.000	80.895	19.551	82.000
19.000	83.394	18.813	84.000	18.482	85.000	18.000	87.000	17.808	88.000
17.684	89.000	17.612	90.000	17.579	91.000				
67.39000	47	53.000	56.000	16.165	91.000				
53.000	56.000	52.000	56.000	51.000	56.000	50.000	56.000	49.000	56.040
48.000	56.080	47.000	56.122	46.000	56.212	45.000	56.261	44.000	56.358
43.000	56.506	42.000	56.619	41.000	56.800	40.000	57.000	39.000	57.263
38.000	57.556	37.000	57.941	36.000	58.360	35.000	58.817	34.000	59.453
33.000	60.132	32.000	60.857	31.000	61.792	30.000	62.792	29.000	63.931
28.000	65.220	27.000	66.580	26.000	68.074	25.000	69.615	24.000	71.231
23.000	72.923	22.000	74.657	21.000	76.471	20.700	77.000	20.000	78.353
19.661	79.000	19.000	80.400	18.719	81.000	18.000	82.667	17.512	84.000
17.000	85.479	16.846	86.000	16.585	87.000	16.389	88.000	16.274	89.000
16.167	90.000	16.165	91.000						

TABLE 13. - Input data for streamline program--Continued

67.65000	46	53.000	55.000	14.660	91.000				
53.000	55.000	52.000	55.000	51.000	55.000	50.000	55.000	49.000	55.000
48.000	55.040	47.000	55.041	46.000	55.085	45.000	55.130	44.000	55.221
43.000	55.281	42.000	55.341	41.000	55.500	40.000	55.690	39.000	55.889
38.000	56.114	37.000	56.419	36.000	56.756	35.000	57.130	34.000	57.674
33.000	58.293	32.000	59.000	31.000	59.851	30.000	60.833	29.000	62.000
28.000	63.245	27.000	64.583	26.000	66.080	25.000	67.624	24.000	69.231
23.000	70.923	22.000	72.615	21.000	74.385	20.657	75.000	20.000	76.161
19.000	78.000	18.000	79.909	17.000	82.000	16.533	83.000	16.000	84.298
15.765	85.000	15.458	86.000	15.000	87.725	14.775	89.000	14.688	90.000
14.660	91.000								
67.91000	48	53.000	54.000	13.000	91.000				
53.000	54.000	52.000	54.000	51.000	54.000	50.000	54.000	49.000	54.000
48.000	54.000	47.000	54.000	46.000	54.000	45.000	54.000	44.000	54.045
43.000	54.093	42.000	54.146	41.000	54.204	40.000	54.272	39.000	54.451
38.000	54.595	37.000	54.817	36.000	55.067	35.000	55.429	34.000	55.846
33.000	56.308	32.000	57.000	31.000	57.758	30.000	58.636	29.000	59.727
28.000	61.000	27.000	62.364	26.000	63.913	25.000	65.510	24.000	67.167
23.000	68.917	22.000	70.615	21.000	72.385	20.631	73.000	20.000	74.080
19.000	75.846	18.000	77.583	17.000	79.353	16.656	80.000	16.000	81.204
15.618	82.000	15.000	83.239	14.654	84.000	14.000	85.648	13.600	87.000
13.326	88.000	13.133	89.000	13.000	91.000				
68.17000	51	53.000	53.000	11.077	91.000				
53.000	53.000	52.000	53.000	51.000	52.962	50.000	52.962	49.000	52.960
48.000	52.920	47.000	52.917	46.000	52.913	45.000	52.872	44.000	52.866
43.000	52.860	42.000	52.850	41.000	52.842	40.000	52.889	39.000	52.943
38.000	53.000	37.000	53.133	36.000	53.286	35.000	53.538	34.000	53.833
33.000	54.258	32.000	54.736	31.000	55.400	30.000	56.200	29.000	57.222
28.000	58.444	27.000	59.889	26.000	61.489	25.673	62.000	25.000	63.189
24.000	64.913	23.000	66.765	22.000	68.583	21.000	70.394	20.631	71.000
20.000	72.077	19.000	73.846	18.000	75.509	17.000	77.161	16.000	78.833
15.000	80.545	14.000	82.213	13.563	83.000	13.000	84.135	12.616	85.000
12.000	86.409	11.851	87.000	11.518	88.000	11.316	89.000	11.159	90.000
11.077	91.000								
68.43000	55	53.000	52.000	8.815	91.000				
53.000	52.000	52.000	52.000	51.000	51.961	50.000	51.962	49.000	51.919
48.000	51.880	47.000	51.830	46.000	51.779	45.000	51.723	44.000	51.661
43.000	51.594	42.000	51.556	41.000	51.474	40.000	51.451	39.000	51.368
38.000	51.382	37.000	51.349	36.000	51.446	35.000	51.500	34.000	51.636
33.000	51.904	32.000	52.208	31.000	52.679	30.000	53.359	29.000	54.262
28.000	55.405	27.000	56.772	26.000	58.516	25.000	60.375	24.700	61.000
24.000	62.333	23.678	63.000	23.000	64.385	22.661	65.000	22.000	66.374
21.682	67.000	21.000	68.250	20.609	69.000	20.000	70.077	19.000	71.846
18.000	73.529	17.000	75.149	16.000	76.684	15.000	78.242	14.000	79.742
13.000	81.290	12.000	82.877	11.000	84.484	10.708	85.000	10.000	86.354
9.736	87.000	9.385	88.000	9.000	89.438	8.889	90.000	8.815	91.000
68.69000	53	53.000	51.000	5.600	91.000				
53.000	51.000	52.000	51.000	51.000	50.963	50.000	50.961	49.000	50.885
48.000	50.837	47.000	50.764	46.000	50.667	45.000	50.565	44.000	50.455
43.000	50.333	42.000	50.206	41.000	50.108	40.000	49.941	39.000	49.813
38.000	49.674	37.000	49.529	36.000	49.394	35.000	49.273	34.000	49.200
33.000	49.111	32.000	49.125	31.000	49.301	30.000	49.521	29.000	50.000
28.000	51.000	27.000	52.250	26.610	53.000	26.000	54.250	25.678	55.000
25.000	56.623	24.000	59.000	23.611	60.000	23.000	61.516	22.000	63.787
21.000	66.000	20.000	68.000	19.000	69.851	18.000	71.615	17.000	73.224
16.000	74.780	15.000	76.286	14.000	77.684	13.000	79.077	12.000	80.343
11.000	81.667	10.000	83.000	9.000	84.239	8.000	85.554	7.000	87.000
6.000	89.000	5.685	90.000	5.600	91.000				
68.96000	58	53.000	50.000	53.000	5.352				
53.000	50.000	52.000	50.000	51.000	49.962	50.000	49.926	49.000	49.844
48.000	49.773	47.000	49.662	46.000	49.542	45.000	49.391	44.000	49.227
43.000	49.048	42.000	48.839	41.000	48.611	40.000	48.353	39.000	48.128
38.000	47.810	37.000	47.490	36.000	47.173	35.000	46.710	34.000	46.250
33.000	45.728	32.000	45.000	31.000	44.000	30.576	43.000	30.301	42.000
30.262	41.000	30.222	40.000	30.300	39.000	30.427	38.000	30.624	37.000
31.000	35.250	31.313	34.000	31.588	33.000	32.000	31.628	32.211	31.000
32.583	30.000	33.000	28.889	33.369	28.000	34.000	26.488	35.000	24.353
36.000	22.462	37.000	20.714	38.000	19.069	39.000	17.608	40.000	16.273
41.000	14.931	42.000	13.721	43.000	12.538	44.000	11.481	45.000	10.455
46.000	9.466	47.000	8.556	48.000	7.761	49.000	7.000	50.000	6.421
51.000	5.844	52.000	5.521	53.000	5.352				
69.23000	57	53.000	49.000	53.000	8.657				
53.000	49.000	52.000	49.000	51.000	48.964	50.000	48.925	49.000	48.815
48.000	48.712	47.000	48.555	46.000	48.417	45.000	48.217	44.000	48.000
43.000	47.745	42.000	47.456	41.000	47.111	40.000	46.744	39.000	46.333
38.000	45.865	37.000	45.264	36.000	44.600	35.000	43.750	34.000	42.576
33.679	42.000	33.000	40.562	32.844	40.000	32.667	39.000	32.624	38.000
32.571	37.000	32.639	36.000	32.750	35.000	33.000	33.500	33.105	33.000
33.305	32.000	33.583	31.000	34.000	29.536	34.177	29.000	34.552	28.000
35.000	26.870	35.333	26.000	36.000	24.573	36.292	24.000	37.000	22.684
37.375	22.000	38.000	20.935	39.000	19.400	40.000	18.000	41.000	16.733
42.000	15.533	43.000	14.475	44.000	13.483	45.000	12.500	46.000	11.700
47.000	10.928	48.000	10.325	49.000	9.736	50.000	9.282	51.000	8.916
52.000	8.753	53.000	8.657						

TABLE 13. - Input data for streamline program--Continued

69.52000	47		53.000	48.000	53.000	11.000				
53.000	48.000	52.000	47.965	51.000	47.926	50.000	47.855	49.000	47.737	
48.000	47.593	47.000	47.423	46.000	47.205	45.000	46.956	44.000	46.682	
43.000	46.339	42.000	45.947	41.000	45.507	40.000	45.000	39.000	44.357	
38.000	43.633	37.000	42.710	36.000	41.390	35.000	39.424	34.600	38.000	
34.438	37.000	34.402	36.000	34.389	35.000	34.462	34.000	34.550	33.000	
34.719	32.000	35.000	30.551	35.130	30.000	35.422	29.000	36.000	27.321	
37.000	25.000	38.000	23.000	39.000	21.333	40.000	19.813	41.000	18.537	
42.000	17.306	43.000	16.235	44.000	15.300	45.000	14.426	46.000	13.632	
47.000	13.000	48.000	12.390	49.000	11.874	50.000	11.500	51.000	11.205	
52.000	11.071	53.000	11.000							
69.80000	46		53.000	47.000	53.000	12.775				
53.000	47.000	52.000	47.000	51.000	46.932	50.000	46.860	49.000	46.711	
48.000	46.551	47.000	46.346	46.000	46.080	45.000	45.750	44.000	45.409	
43.000	44.952	42.000	44.474	41.000	43.882	40.000	43.192	39.000	42.308	
38.000	41.189	37.000	39.639	36.694	39.000	36.346	38.000	36.056	37.000	
35.897	36.000	35.820	35.000	35.813	34.000	35.869	33.000	36.000	31.725	
36.124	31.000	36.329	30.000	36.565	29.000	37.000	27.654	37.229	27.000	
38.000	25.161	39.000	23.200	40.000	21.563	41.000	20.176	42.000	18.947	
43.000	17.837	44.000	16.849	45.000	16.000	46.000	15.274	47.000	14.618	
48.000	14.055	49.000	13.595	50.000	13.227	51.000	13.000	52.000	12.832	
53.000	12.775									
70.11000	43		53.000	46.000	53.000	14.406				
53.000	46.000	52.000	45.967	51.000	45.902	50.000	45.797	49.000	45.613	
48.000	45.424	47.000	45.149	46.000	44.846	45.000	44.453	44.000	44.000	
43.000	43.476	42.000	42.829	41.000	42.060	40.000	41.071	39.000	39.825	
38.507	39.000	38.000	37.865	37.710	37.000	37.434	36.000	37.269	35.000	
37.174	34.000	37.163	33.000	37.238	32.000	37.351	31.000	37.528	30.000	
38.000	28.118	38.361	27.000	39.000	25.462	40.000	23.525	40.308	23.000	
41.000	21.946	42.000	20.604	43.000	19.456	44.000	18.456	45.000	17.583	
46.000	16.817	47.000	16.194	48.000	15.656	49.000	15.194	50.000	14.856	
51.000	14.606	52.000	14.494	53.000	14.406					
70.42000	40		53.000	45.000	53.000	15.835				
53.000	45.000	52.000	44.969	51.000	44.904	50.000	44.766	49.000	44.577	
48.000	44.341	47.000	44.036	46.000	43.649	45.000	43.200	44.000	42.652	
43.000	42.000	42.000	41.161	41.000	40.128	40.000	38.758	39.577	38.000	
39.000	36.589	38.832	36.000	38.588	35.000	38.476	34.000	38.389	33.000	
38.401	32.000	38.509	31.000	38.629	30.000	39.000	28.484	39.453	27.000	
40.000	25.675	40.321	25.000	41.000	23.765	42.000	22.263	43.000	21.000	
44.000	19.953	45.000	19.045	46.000	18.269	47.000	17.619	48.000	17.043	
49.000	16.619	50.000	16.258	51.000	16.042	52.000	15.874	53.000	15.835	
70.75000	36		53.000	44.000	53.000	17.153				
53.000	44.000	52.000	43.970	51.000	43.878	50.000	43.732	49.000	43.527	
48.000	43.227	47.000	42.867	46.000	42.403	45.000	41.878	44.000	41.221	
43.000	40.350	42.000	39.300	41.000	37.856	40.547	37.000	40.000	35.446	
39.686	34.000	39.599	33.000	39.556	32.000	39.624	31.000	39.737	30.000	
40.000	28.768	40.220	28.000	40.556	27.000	41.000	25.933	42.000	24.056	
43.000	22.625	44.000	21.440	45.000	20.464	46.000	19.649	47.000	18.961	
48.000	18.394	49.000	17.927	50.000	17.586	51.000	17.342	52.000	17.191	
53.000	17.153									
71.10000	32		53.000	43.000	53.000	18.412				
53.000	43.000	52.000	42.973	51.000	42.862	50.000	42.705	49.000	42.443	
48.000	42.123	47.000	41.693	46.000	41.141	45.000	40.505	44.000	39.657	
43.000	39.585	42.000	37.136	41.473	36.000	41.135	35.000	40.870	34.000	
40.748	33.000	40.697	32.000	40.722	31.000	41.000	29.135	41.268	28.000	
42.000	26.130	43.000	24.350	44.000	22.957	45.000	21.882	46.000	21.000	
47.000	20.253	48.000	19.686	49.000	19.208	50.000	18.861	51.000	18.595	
52.000	18.446	53.000	18.412							
71.48000	29		53.000	42.000	53.000	19.602				
53.000	42.000	52.000	41.974	51.000	41.839	50.000	41.652	49.000	41.358	
48.000	40.969	47.000	40.469	46.000	39.828	45.000	39.000	44.000	37.954	
43.000	36.453	42.347	35.000	42.060	34.000	41.887	33.000	41.807	32.000	
41.814	31.000	42.000	29.378	42.361	28.000	43.000	26.405	44.000	24.682	
45.000	23.389	46.000	22.397	47.000	21.575	48.000	20.938	49.000	20.445	
50.000	20.060	51.000	19.798	52.000	19.647	53.000	19.602			
71.89000	27		53.000	41.000	53.000	20.738				
53.000	41.000	52.000	40.952	51.000	40.807	50.000	40.588	49.000	40.234	
48.000	39.781	47.000	39.183	46.000	38.414	45.000	37.375	44.000	35.899	
43.569	35.000	43.000	33.000	42.877	32.000	42.876	31.000	42.951	30.000	
43.149	29.000	43.434	28.000	44.000	26.644	45.000	25.000	46.000	23.830	
47.000	22.905	48.000	22.207	49.000	21.652	50.000	21.247	51.000	20.947	
52.000	20.793	53.000	20.738							
72.34000	25		53.000	40.000	53.000	21.841				
53.000	40.000	52.000	39.935	51.000	39.778	50.000	39.514	49.000	39.119	
48.000	38.573	47.000	37.853	46.000	36.861	45.000	35.446	44.368	34.000	
44.093	33.000	43.954	32.000	43.914	31.000	44.000	30.000	44.203	29.000	
44.511	28.000	45.000	26.911	46.000	25.349	47.000	24.273	48.000	23.466	
49.000	22.846	50.000	22.392	51.000	22.071	52.000	21.887	53.000	21.841	





TABLE 14. - Streamline coordinates calculated by stream program

STREAMLINE 1		STREAMLINE 2		STREAMLINE 3		STREAMLINE 4	
XS	YS	XS	YS	XS	YS	XS	YS
53.000	91.000	53.000	91.000	53.000	91.000	53.000	91.000
53.000	80.000	52.000	80.042	51.000	80.183	50.000	80.423
53.000	79.000	51.912	79.052	50.806	79.207	49.734	79.464
53.000	78.000	51.827	78.047	50.606	78.224	49.467	78.491
53.000	77.000	51.741	77.055	50.413	77.243	49.199	77.522
53.000	76.000	51.655	76.062	50.226	76.263	48.931	76.567
53.000	75.000	51.565	75.056	50.038	75.281	48.661	75.592
53.000	74.000	51.476	74.081	49.842	74.295	48.401	74.637
53.000	73.000	51.384	73.073	49.648	73.312	48.132	73.667
53.000	72.000	51.287	72.090	49.463	72.341	47.869	72.715
53.000	71.000	51.198	71.085	49.272	71.359	47.600	71.744
53.000	70.000	51.115	70.068	49.080	70.360	47.321	70.743
53.000	69.000	51.031	69.079	48.901	69.385	47.059	69.788
53.000	68.000	50.961	68.088	48.711	68.383	46.804	68.807
53.000	67.000	50.900	67.095	48.520	67.422	46.551	67.842
53.000	66.000	50.826	66.074	48.331	66.393	46.278	66.825
53.000	65.000	50.739	65.088	48.162	65.400	46.016	65.834
53.000	64.000	50.661	64.085	47.980	64.383	45.768	64.837
53.000	63.000	50.577	63.082	47.790	63.390	45.529	63.831
53.000	62.000	50.506	62.078	47.612	62.380	45.289	62.823
53.000	61.000	50.452	61.075	47.469	61.344	45.065	61.787
53.000	60.000	50.394	60.055	47.335	60.330	44.828	60.723
53.000	59.000	50.352	59.057	47.201	59.293	44.601	59.679
53.000	58.000	50.322	58.030	47.090	58.267	44.415	58.582
53.000	57.000	50.296	57.065	46.965	57.210	44.263	57.516
53.000	56.000	50.270	55.996	46.840	56.139	44.116	56.344
53.000	55.000	50.270	56.000	46.760	55.051	44.028	55.220
53.000	54.000	50.270	55.000	46.759	55.000	43.978	54.046
53.000	53.000	50.270	52.962	46.753	52.919	43.954	52.866
53.000	52.000	50.275	51.966	46.777	51.819	44.005	51.661
53.000	51.000	50.288	50.969	46.855	50.750	44.122	50.469
53.000	50.000	50.321	49.943	46.965	49.658	44.290	49.276
53.000	49.000	50.367	48.947	47.103	48.570	44.513	48.116
53.000	48.000	50.432	47.891	47.284	47.476	44.798	46.906
53.000	47.000	50.504	46.906	47.482	46.452	45.126	45.792
53.000	46.000	50.592	45.869	47.742	45.356	45.533	44.670
53.000	45.000	50.705	44.869	48.014	44.345	45.949	43.628
53.000	44.000	50.834	43.858	48.310	43.326	46.402	42.597
53.000	43.000	50.952	42.857	48.617	42.333	46.881	41.632
53.000	42.000	51.087	41.853	48.941	41.338	47.378	40.673
53.000	41.000	51.247	40.850	49.296	40.349	47.883	39.719
53.000	40.000	51.411	39.855	49.653	39.393	48.388	38.803
53.000	39.000	51.576	38.881	50.016	38.437	48.891	37.916
53.000	38.000	51.752	37.889	50.385	37.498	49.416	37.017
53.000	37.000	51.932	36.897	50.764	36.558	49.930	36.145
53.000	36.000	52.116	35.910	51.146	35.623	50.448	35.273
53.000	35.000	52.301	34.932	51.527	34.699	50.966	34.414
53.000	34.000	52.500	33.938	51.925	33.758	51.502	33.538
53.000	33.000	52.713	32.956	52.323	32.831	52.033	32.680
53.000	31.000	53.000	31.000	53.000	31.000	53.000	31.000

TABLE 14. - Streamline coordinates calculated by stream program--Continued

STREAMLINE 5		STREAMLINE 6		STREAMLINE 7a <sup>1</sup>		STREAMLINE 7b <sup>1</sup>	
XS	YS	XS	YS	XS	YS	XS	YS
53.000	91.000	53.000	91.000	53.000	91.000	22.000	48.911
49.000	80.755	48.000	81.204	47.183	81.664	26.692	46.198
48.638	79.829	47.548	80.319	46.690	80.812	30.920	43.856
48.270	78.891	47.087	79.423	46.187	79.941	33.789	42.209
47.907	77.961	46.630	78.536	45.685	79.072	35.757	41.005
47.545	77.024	46.173	77.650	45.182	78.201	37.258	40.102
47.185	76.099	45.708	76.753	44.676	77.326	38.666	39.287
46.809	75.170	45.256	75.868	44.181	76.469	39.891	38.576
46.434	74.225	44.808	74.968	43.676	75.594	41.030	37.907
46.080	73.302	44.358	74.058	43.172	74.723	42.091	37.297
45.710	72.355	43.922	73.178	42.670	73.853	43.135	36.693
45.340	71.412	43.452	72.248	42.158	72.967	44.124	36.119
44.991	70.481	43.002	71.346	41.650	72.087	45.074	35.575
44.633	69.508	42.546	70.416	41.134	71.195	45.998	35.038
44.283	68.560	42.101	69.525	40.631	70.324	46.900	34.518
43.919	67.567	41.633	68.569	40.099	69.403	47.792	34.003
43.566	66.613	41.170	67.623	39.569	68.485	48.684	33.489
43.210	65.615	40.708	66.681	39.045	67.578	49.556	32.981
42.871	64.607	40.240	65.716	38.509	66.651	50.412	32.484
42.526	63.614	39.745	64.735	37.962	65.705	51.256	31.991
42.155	62.551	39.244	63.735	37.390	64.715	53.000	31.000
41.795	61.493	38.734	62.678	36.809	63.709		
41.450	60.408	38.236	61.642	36.222	62.694		
41.144	59.285	37.694	60.505	35.601	61.619		
40.858	58.128	37.181	59.366	34.957	60.504		
40.587	56.875	36.645	58.086	34.255	59.289		
40.345	55.623	36.120	56.714	33.497	57.977		
40.137	54.256	35.588	55.210	32.667	56.540		
40.028	52.888	35.088	53.518	31.726	54.912		
40.081	51.462	34.747	51.522	30.590	52.946		
40.301	49.987	34.711	49.254	28.986	50.169		
40.610	48.506	35.303	46.838				
41.030	47.121	36.390	44.878				
41.562	45.762	37.623	43.319				
42.142	44.548	38.792	42.100				
42.812	43.363	39.939	41.007				
43.470	42.327	40.968	40.091				
44.155	41.335	41.970	39.262				
44.860	40.398	42.920	38.489				
45.576	39.500	43.846	37.757				
46.272	38.646	44.756	37.067				
46.964	37.822	45.628	36.406				
47.638	37.035	46.479	35.775				
48.329	36.234	47.319	35.155				
49.000	35.473	48.149	34.540				
49.685	34.708	48.977	33.930				
50.355	33.963	49.789	33.335				
51.046	33.197	50.589	32.736				
51.665	32.451	51.368	32.152				
53.000	31.000	53.000	31.000				

<sup>1</sup>Results for streamline 7a - 7b were determined using modifications described in text.

## CONCLUDING STATEMENT

Computer methods are presented to calculate the coordinates of isopressure lines and streamlines for a field using pressures at grid intersections. The resulting flow nets agree well with those obtained using other methods, especially for the 7-spot pattern used as an example calculation in this paper. The methods have been tested on a wide range of flow geometries and should work for any field.

## REFERENCES

1. Higgins, R. V., D. W. Boley, and A. J. Leighton. Aids To Forecasting the Performance of Water Floods. Trans. AIME, v. 231, September 1964, pp. 1076-1082.
2. \_\_\_\_\_. Computer Techniques for Calculating Shape Factors and Channel Volumes From a Potentiometric Model for Use in Waterflood Performance Calculations. BuMines Rept. of Inv. 6760, 1966, 49 pp.
3. Higgins, R. V., and A. J. Leighton. Computer Techniques for Predicting Three-Phase Flow In Five-Spot Waterfloods. BuMines Rept. of Inv. 7011, August 1967, 45 pp.
4. \_\_\_\_\_. Improved Method for Calculating Areas and Shape Factors of Flow Nets. BuMines Rept. of Inv. 7111, April 1968, 32 pp.
5. \_\_\_\_\_. Quick Way To Find Reservoir Pressure Distribution. Oil and Gas J., v. 67, No. 1, Jan. 6, 1969, pp. 67-70.
6. Hurst, W., and A. F. van Everdingen. Performance of Distillate Reservoirs in Gas Cycling. Trans. AIME, v. 165, 1946, pp. 36-51.
7. Le Blanc, J. L., and B. H. Caudle. A Streamline Model for Secondary Recovery. Soc. Petrol. Eng. J., v. 11, No. 1, March 1971, pp. 7-12.
8. Muskat, M. Physical Principles of Oil Production. McGraw-Hill Book Co., Inc., New York, 1949, pp. 656-682.
9. Prats, M., P. Hazebroek, and E. E. Allen. Effect of Off-Pattern Wells On the Performance of a Five-Spot Water Flood. Trans. AIME, v. 225, 1962, pp. 173-178.

## APPENDIX A.--NOMENCLATURE FOR ISOPRESSURE PROGRAM

A	=	Term used in solving quadratic equation in subroutine POLCON for location of point on extended pressure line.
AQUI	=	Name assigned to labeled common block containing grid pressures and other data.
AVP	=	Value of pressure for a given line.
B	=	Term used in solving quadratic equation.
BPOR	=	Term used in solving quadratic equation.
C	=	Term used in solving quadratic equation.
D	=	Term used in solving quadratic equation.
DR1, DR2	=	Terms used in solving quadratic equation.
FIT	=	Logical variable used to route program according to whether proper grid location has been found for an extended pressure line.
FORK	=	Logical variable used to route program according to whether lookup is in x or y direction.
I	=	Index of vertical grid line, goes with x.
IADD	=	Set of parameters used to calculate spread of lookup locations for first extended point.
IB	=	Starting index for successive lookup between pairs of vertical grid lines.
ICALL	=	Set of parameters used to aid routing to x or y lookup depending upon which vector the model applies.
IE	=	Ending index for successive lookup between pairs of vertical lines.
IGO	=	Routing parameter used in reindexing points on pressure line.
II	=	Additional (substitute) index for columns on vertical grid lines.
IM	=	Index of vertical grid line near possible point on pressure line.

IPLUS	= Set of parameters used to calculate spread of lookup locations for various vector models.
IP3	= Index of vertical grid line located by lookup near pressure line.
IT	= Index of vertical grid line in subroutine LOOKUP.
ITAL	= Number of points on a pressure line which have been determined, also cumulative index of the points.
ITALM2	= ITAL - 2.
ITTAL	= Temporary storage for ITAL.
J	= Index of horizontal grid line.
JB	= Starting index for successive lookup between pairs of horizontal grid lines.
JE	= Ending index for successive lookup between pairs of horizontal grid lines.
JJ	= Additional (substitute) index for rows or horizontal grid lines.
JM	= Index of horizontal grid line near possible point on pressure line.
JP3	= Index of horizontal grid line located by lookup near pressure line.
JT	= Index of horizontal grid line in subroutine LOOKUP.
K	= Index or counter for points on pressure lines originating on an edge.
KK	= Index denoting origin of pressure line at a particular edge or interior.
L	= Index denoting to which vector model pressure line is conforming.
L1D	= Index indicating number of grid lines passed.
LOOKUP	= Name of subroutine which looks up location of grid lines closest to extended pressure line.
M	= Index controlling orientation of grid locations to enter lookup.

MP	=	Name of IP3 or JP3 in subroutine LOOKUP.
NEND	=	Total number of grid lines on an edge to be scanned for starting pressure lines.
P	=	Pressure at a grid point.
P1, P2, P3	=	Pressure values in subroutine POLCON.
POLCON	=	Name of subroutine which solves quadratic equation.
PP	=	Term used in solving quadratic equation.
Q	=	Term used in solving quadratic equation.
R1, R2	=	Roots of quadratic equation; usually one of them is fractional distance along grid line to where pressure line crosses.
TEST	=	Integer at a grid point indicating whether a pressure line passes close enough for proper density.
WORD	=	Storage for labels of groups of lines originating at different edges or interior.
X	=	Distance in horizontal direction, goes with I. Also abscissas of points on pressure line.
XSAVE	=	Temporary storage for abscissas of pressure lines.
XUP	=	Number of vertical grid lines (horizontal extent of pattern).
XX	=	Fractional distance along horizontal grid line to where pressure line crosses.
Y	=	Distance in vertical direction, goes with J. Also ordinates of points on pressure line.
YSAVE	=	Temporary storage for ordinates of pressure lines.
YUP	=	Number of horizontal grid lines (vertical extent of pattern).
YY	=	Fractional distance along vertical grid line to where pressure line crosses.

## APPENDIX B.--NOMENCLATURE FOR STREAMLINE PROGRAM

- A, A1, A2 = Constant in circle equation for segment of isopressure line in subroutine QUAD, and for preceding and succeeding isopressure lines in MAIN program, respectively.
- ACTN1, ACTN2 = Intercept on x axis of cotangent line for preceding and next pressure lines, respectively. (See CTN1, CTN2.)
- AS = Function to calculate intercept of a line.
- AS1, AS2 = Intercept on x axis of line tangent to preceding and succeeding pressure lines, respectively.
- ASC = Sum of ASD1 and ASD2 in subroutine STRM.
- ASD1, ASD2 = Terms used in determinant solution for intersection in subroutine STRM.
- AVP = Value of pressure for an isopressure line.
- B, B1, B2 = Constant in circle equation for segment of isopressure line in subroutine QUAD, and for preceding and succeeding isopressure lines in MAIN program, respectively.
- BOUND = Name of subroutine to process streamlines near a boundary.
- CTN = Function to calculate slope of line normal to isopressure line (cotangent line).
- CTN1, CTN2 = Slope of line normal to isopressure line (cotangent line) for preceding and succeeding isopressures, respectively.
- DEL = Estimated x increment between preceding and succeeding pressure lines.
- DELTA = Difference between streamline ordinate and ordinate of point on diagonal boundary being tracked--used in subroutine BOUND.
- DELX12, DELX23 = Difference in x values used in subroutine QUAD.
- DXSQ12, DXSQ23 = Differences in  $x^2$  used in subroutine QUAD.
- DELY12, DELY23 = Differences in y values used in subroutine QUAD.
- DYSQ12, DYSQ23 = Differences in  $y^2$  used in subroutine QUAD.
- DEM = Term used in determinant solution for coordinates of midpoint in subroutine STRM.

DM1, DM2	=	Terms used in determinant solution for coordinates of midpoint.
FIELD	=	Name assigned to labeled common block containing coordinates of isopressure lines and other data.
IFLAG	=	Index for streamline to route program to normal or boundary calculation.
IN	=	Index to skip unnecessary alternate values when punching streamline coordinates.
IP	=	Index used in printing and punching streamline coordinates.
IPTAL	=	Number of points on a streamline.
IS	=	Index of a point on streamline.
ITER	=	Counter indicating number of iterations completed in converging on correct location of streamline intersection.
JTAG	=	Integer parameter to determine whether estimated abscissa for intersection should be incremented in subroutine LOCATE.
LGO	=	Routing index for terminating calculation of a streamline when trouble occurs.
LOCATE	=	Name of subroutine to find index of intersection of projected streamline with isopressure line.
MLINE	=	Number of isopressure lines used.
MLNM2	=	NLINE - 2.
MP	=	Index of an isopressure line.
MP1	=	Index of succeeding isopressure line.
MSTART	=	Index of pressure line from which streamline calculation starts initially.
N	=	Index for a point on isopressure line.
NB	=	Starting index for lookup along an isopressure line.
NE	=	Ending index for lookup along an isopressure line.
NEM1	=	NE - 1.
NINT	=	Interval between successive streamline starting points.

NITAL	=	Temporary storage for NTAL indexed for subsequent use.
NTAL	=	Number of points on an isopressure line.
NNN	=	Counter for number of times starting point advanced for new lookup in subroutine LOCATE.
NP3	=	Index of point on isopressure line just preceding intersection with streamline.
NSTREAM	=	Number of streamlines to be determined.
NT	=	Index of point on isopressure line used in subroutine LOCATE.
QUAD	=	Name of subroutine to calculate constants for equation of segment of pressure line.
R, R1, R2	=	Constant in circle equation in subroutine QUAD, and for preceding and succeeding isopressure lines in MAIN program, respectively.
STRM	=	Name of subroutine to calculate orthogonals to isopressure lines.
TANC	=	Term used in solving determinant in subroutine STRM.
TAN1, TAN2	=	Slope of pressure line at intersection with streamline for preceding and succeeding lines, respectively.
TAND1, TAND2	=	Terms used in solving determinant in subroutine STRM.
TERM	=	Parameter used in calculating constants for isopressure line equation.
TN	=	Function used to calculate slope of pressure line from equation.
V1, V2	=	Dummy variables for y ordinates in function subprograms.
X	=	Abscissa of a point.
XA	=	Abscissas of points given on pressure line.
XINL	=	Abscissa of midpoint where two projected orthogonal lines meet.
XINT	=	Abscissa of tentative intersection of projected streamline and succeeding pressure line.

XP = Abscissa of intersection calculated using linear equation.

XS = Abscissa of an indexed point on streamline.

XT = Temporary abscissa used in subroutine LOCATE.

X1 = Abscissa of preceding intersection.

X2 = Estimated x coordinate of intersection.

Y = Ordinate of a point.

YA = Ordinates of points given on isopressure line.

YC = Term used in solving determinant.

YD1, YD2 = Term used in solving determinant.

YINL = Ordinate of midpoint where two projected orthogonal lines meet.

YP = Ordinate of intersection calculated using linear equation of orthogonal.

YQ = Ordinate of intersection calculated using circle equation of isopressure line.

YS = Ordinate of an indexed point on streamline.

YTEST = Ordinate calculated from projecting previous ordinate used to check location of possible point in subroutine LOCATE.

YVALUE = Function used to calculate ordinates of pressure line using circle equation.

Y1 = Ordinate of preceding intersection.

Y2 = Ordinate of tentative intersection.