

A Unique Approach to Determining the Time Dependent  
In Situ Strength of Coal Pillars

by

K. Biswas  
University of Ballarat  
Ballarat, Victoria 3353, Australia

Christopher Mark  
National Institute for Occupational Safety and Health  
Pittsburgh Research Laboratory  
Pittsburgh, PA 15236

and

Syd. S. Peng  
University of West Virginia  
Morgantown, WV 15060

## ABSTRACT

In general, it cannot be assumed that the strength of coal pillars remains constant over long time periods. Field observations indicate that a coal seam, especially when it contains a parting layer, deteriorates over time, reducing load-bearing capacity of the pillars. This paper discusses a unique approach to determine the time dependent strength of coal pillars in the field. Three coal pillars that were developed 5, 15 and 50 years ago were chosen for the study. Holes were drilled in coal and parting layers in each pillar and the strength profiles were determined for each hole using the Borehole Penetrometer. The strength data were treated statistically to establish time dependent strength equations for different layers. The results can be used to help estimate the loss of pillar capacity over time.

## ACKNOWLEDGMENTS

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## INTRODUCTION

All man-made structures deteriorate over time, and pillars in underground coal mines are no exception. There are numerous examples of coal pillars failing many years after they were developed. Scrutiny of existing pillar design theories indicates that few make any attempt to consider the effect of time. Similarly, there is rarely an attempt to consider the inhomogeneous nature of most coal seams.

For example, the classic pillar design methodology involves the following three steps:

- a. Calculate the vertical stress on the pillar:

$$S_v = \frac{\gamma H (W + W_e)(L + W_e)}{(WL)} \quad (1)$$

where:

- $S_v$  = vertical stress
- $\gamma$  = unit weight of the overburden
- $H$  = depth of the seam
- $W$  = pillar width (minimum pillar dimension)
- $L$  = pillar length (maximum pillar dimension)
- $W_e$  = entry width

- b. Calculate the pillar strength, using Bieniawski's formula (Bieniawski, 1992)

$$s_p = S_i \left( 0.64 + \left( 0.36 \frac{(W - W_e)}{h} \right) \right) \quad (2)$$

where:

- $S_p$  = pillar strength
- $S_i$  = in situ seam strength
- $h$  = seam height

- c. Calculate the stability factor (SF) as:

$$SF = \frac{\text{Pillar Strength}}{\text{Pillar Stress}} = \frac{s_p}{S_v} \quad (3)$$

The stability factor that is calculated using equations 1-3 assumes that:

- The coal strength is constant and does not deteriorate over time, and;
- Coal seams are homogenous.

Back-analyses of subsidence above abandoned mines using the classic methodology have found that pillar failures have occurred over a broad range of stability factors (Marino, 1989; Craft and Crandall, 1988). The implication is that over time, the standard pillar design methodology loses its ability to accurately predict the strength of coal pillars.

One recent South African study focused on the phenomenon of pillar scaling over time (van der Merwe, 1998). Twenty-seven case histories of pillar failure, occurring as long as 15 years after mining, were included in the data base. Three parameters were found to be statistically significant: Coal seam, pillar height, and time-to-failure. The study concluded that the scaling rate decreases exponentially over time, and further hypothesized that "the inner portions of the pillar, being protected from the atmosphere, would then weather at a lower rate."

The present paper describes a detailed study of the time dependent structural deterioration of coal pillars, and proposes a means to estimate the strength reduction of the coal seam in-situ by taking into account the seam heterogeneity.

## FIELD OBSERVATIONS

A survey conducted by Department of Mining Engineering, West Virginia University, of the room-and pillar mines in eastern Appalachian region, found that some of the coal seams contain one or more mudstone or claystone layers with variable thicknesses (Tsang et al., 1996). For example, the Pittsburgh and Twin Freeport seams contain parting layers in the coal seam. During field visits to several coal mines developed in these seams, the authors had the opportunity to visually inspect the conditions of many pillars in worked out districts, some as much as 100 years old. Most of the pillars that the authors inspected did not show any apparent sign of instability, owing to their large size compared to their depth (stability factors ranged from 2 - 12).

A more detailed inspection gave evidence of several kinds of weathering actions on the different layers of the coal seam with varying degree of severity. The following structural deteriorations were noticed on older pillars:

- Conversion of mudstone/claystone layer to clay due to prolonged exposure to the mine moisture;
- Squeezing of the softer parting layer by the top and bottom portion of the coal;
- Major peeling of the parting layer;
- Separation of the parting from the host coal along the slick interfaces (could be the result of differential slippage), and;
- Minor peeling of the top and bottom portion of the coal.

Figure 1 illustrates a schematic of this deterioration in the structure of a pillar.

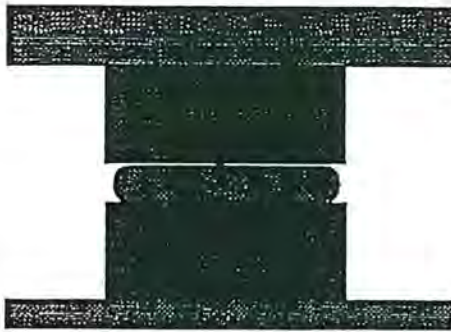


Figure 1. Schematic of peeling of weathered parting in coal seam.

From the field observations, it was concluded that the structural deteriorations in both coal and parting are dependent on time. From these observations, aided by some laboratory studies and finite element modeling (Biswas, 1997), it was possible to postulate a conceptual model of the time dependent strength profiles in the coal and parting layers. The model is illustrated in figures 2 and 3, and its assumptions are:

- The pillars are not affected by any mining activity in their vicinity, and;
- The majority of the yield zones depicted in figures 2 and 3 are the result of the weathering action on the different layers in the pillar.

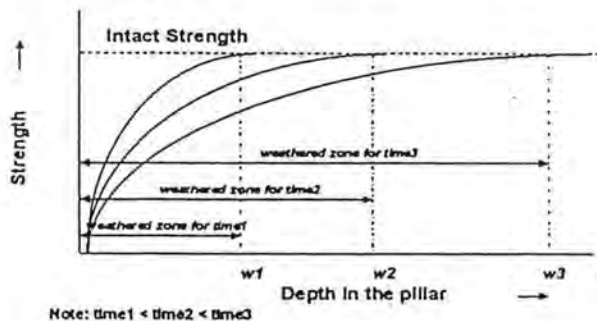


Figure 2. Conceptualization for strength deterioration for parting.

#### IN-SITU DETERMINATION OF TIME DEPENDENT STRENGTH

The goal of this study was to determine one set of time dependent strength profiles under in situ conditions. A detailed testing program was designed to establish the strength reduction in various layers of a pillar in-situ over time.

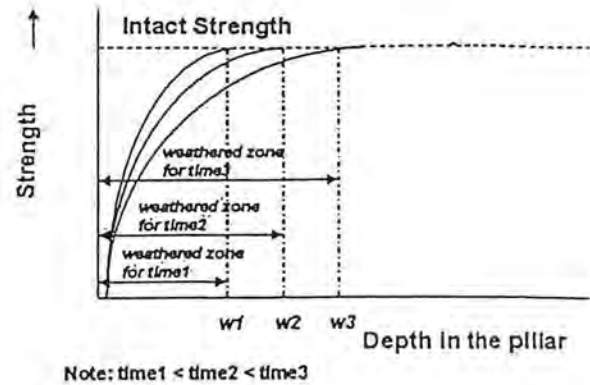


Figure 3. Conceptualization for strength deterioration for coal

#### The Study Site

The study was conducted at the Safety Research Coal Mine (SRCM) at the Pittsburgh Research Laboratory (PRL) of the National Institute for Occupational Safety and Health (NIOSH). The SRCM was selected for the following reasons:

1. The overburden depth is very shallow, ranging from 15 to 18m (50-60 ft), so any deterioration of the pillars is attributable to the effect of weathering rather than stress;
2. The mine is developed in the Pittsburgh seam and it contains a parting of varying thickness from 0.15 to 0.31m (6-12 in);
3. The mine has accessible pillars developed as recently as 1991 and as long ago as the 1940's, and finally;
4. The mine remains more or less inactive in terms of mining activities.

Of all the available pillars in the SRCM, three were chosen based on their current conditions and the thickness of the parting. The three pillars were developed 5, 15, and 50 years ago. Due to other technical difficulties more faces could not be chosen for this experiment. Figure 4 shows the mine plan and the location of the study sites.

#### The Apparatus:

The Borehole Penetrometer (BPT) was chosen to measure the strength profiles in the coal and parting layers. The basic principle followed by the BPT is to fracture the borehole wall by means of an indenter, and record the pressure that initiates the first fracture (Hladysz, 1995). The recorded failure pressure is then converted by a formula to determine the uniaxial compressive strength at that location in the borehole. The BPT's big advantages are that the rock strength is tested in situ, and multiple tests can be conducted within a single borehole (Zhang et al., 1995).



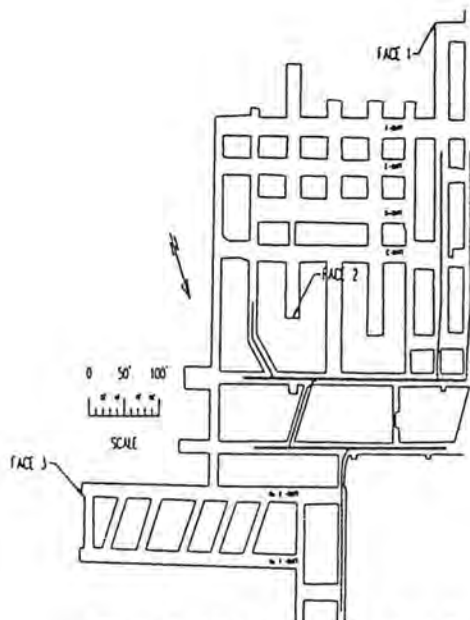


Figure 4. Mine plan showing three faces chosen for the BPT tests.

The BPT consists of the following components:

- i. Head;
- ii. Hydraulic pump w/ oil reservoirs and pressure transducers;
- iii. Displacement indicator;
- iv. Four-wire electric cable;
- v. High pressure hydraulic hose with quick couplers, and;
- vi. Set of extension rods.

The test set-up is illustrated in figure 5. To perform the test, the head of the device is inserted into a standard NX drill hole with the help of a set of extension rods. When the head is positioned at the desired depth, the indenter is forced into the borehole wall utilizing the hydraulic pump. At the critical pressure, the indenter penetrates the rock rapidly making a small crater around the indenter's tip. This event is indicated by a rapid movement of the needle on the displacement indicator, and by a sudden drop in pressure (figure 6). In hard and brittle rock an audible sound is often associated with rock failure. The critical pressure causing the rock to break is a function of rock separation resistance (or penetration resistance). Penetration resistance is proportional to the material properties of rock mass and the state of stresses. By re-positioning the head and repeating the test procedures along the entire length of the hole, a penetration profile (or strength profile) for the tested section of the rock mass can be determined.

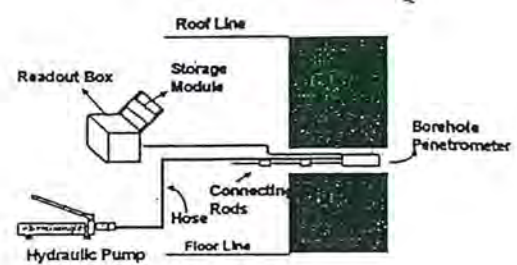


Figure 5. Schematic of borehole penetrometer test set up

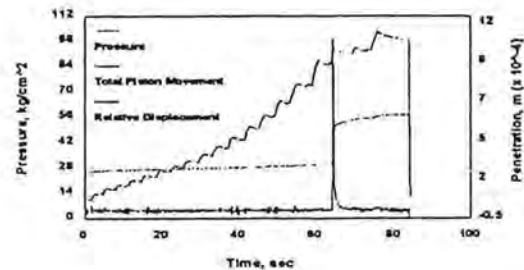


Figure 6. Typical raw BPT test data analysis for parting.

To achieve accuracy, a pressure transducer, a data acquisition module, and a digital readout unit are used. The failure pressure and ram displacement data recorded at a specified time interval are stored during an individual test and later transferred to a computer to determine the failure pressure. A portable battery operated recorder unit records the collected data. The pressure transducer that is connected to the hydraulic pump generates the pressure signal, while the displacement signal comes from LVDT that is linked to the indenter. The recorded data is stored in the data logger unit memory and later played back using a personal computer driven by application software. The data from a typical BPT test include the pressure, displacement of ram or indenter, time and an identification for the hole number, test depth, test date etc. More details about the instrument, its specifications, principles and testing procedure can be found elsewhere (Hladysz, 1995).

#### The Experiment:

For each Borehole Penetrometer test, the following steps were carried out:

1. Connect the hydraulic hoses to the head and to the pump;
2. Connect the cable to the head and to the data acquisition displacement input terminals;
3. Connect the cable to the pressure transducer and to the data acquisition pressure input terminals;
4. Set up the recording session parameters in the data logger unit (e.g. date, id. no. etc.);

5. Insert the head into the borehole and position the device at desired depth;
6. Close the main valve of the pump;
7. Initiate a data recording session;
8. Increase pressure slowly at a constant rate, continuing to pump until the failure occurs;
9. Open the valve in order to allow the indenter to retract fully and stop recording, and;
10. Reposition the Penetrometer head and repeat the steps 4-9.

Two NX boreholes were drilled in each test pillar, one in coal and one in the parting. The holes were each 3 m (10 ft) long. About 15-20 tests were done along each borehole. The testing frequency was higher in near the pillar edge, as it was postulated that the rib edge would be more disturbed than the intact central portion of the pillar. All the data for each test were collected in the storage module during the tests and later on transferred to a computer for more detailed analysis. The data for each test point were manipulated in a spreadsheet program and finally a graph was plotted for each test point. The graph consists of time on the X-axis, failure pressure on the primary Y-axis, and the relative displacement rate of the indenter on the secondary Y-axis. Typical graphs for the parting and the coal are shown in figures 6 and 7. The failure pressure in the hard rock, in general, is characterized by a distinct jump (increase) in the ram displacement.

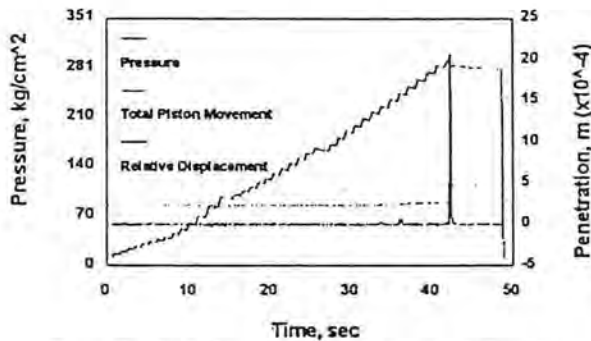


Figure 7. Typical raw BPT test data analysis for coal.

#### Data Analysis

The first step in analyzing the data was to determine the failure pressures at all test points. Then the following conversion formula was used to convert the failure pressure to the unconfined compressive strength

$$UCS = (F_s) P_f \quad (4)$$

Where UCS is the unconfined compressive strength,  $F_s$  is the strength factor and  $P_f$  is the failure pressure from the BPT test. For coal, the value of the strength factor was 1.25 as suggested by Zhang et al (1995). For the parting, a value of 1.00 was used, based on laboratory studies of the cores of the parting obtained from the BPT test holes (Biswas, 1997).

The scatter plots of the converted strength values were obtained for each hole in each face. Since these scatter plots

showed considerable variability in the trend of the strength deterioration, which is a typical characteristic of any experiment conducted in situ, a curve fitting program called "Curve Expert" was used to fit the best curve with the highest correlation coefficient. Figures 8 to 10 illustrate the best fit curves for the parting, and Figures 11 to 13 illustrate the best fit curves for the coal for all three faces.

The general form of all the best fit equations for both coal and parting is as follows:

$$y = a(1.01 - e^{-bx}) \quad (5)$$

Where:

- a and b are the coefficients;
- y is the failure pressure or the strength, and
- x is the depth (in this case the range is from 0.06-3m or 0.2-10 ft).

The negative exponential and its negative power give the best fit curves their asymptotic form. The correlation coefficients for the best fit equations for the parting and coal for each age group are 0.84, 0.85, 0.89 and 0.96, 0.88, 0.94 respectively.

For the parting, the gradient in the weathered zone for the younger face is initially steeper, but the slope flattens as the age increases. This change in strength gradient before it reaches the intact or stabilized strength is considerable. The weathered zone apparently expands from 1 to 3m (3.5 and 10 ft) over the fifty years. For coal, the strength gradient for all the age groups is steeper compared to parting's, and the expansion of the weathered zone is much less (from 0.2 to 1 m (0.7 to 3.2 ft)). These findings fit the conceptual model of the strength degradation for parting and coal over time described earlier.

Figures 8-13 also indicate that there is some borehole-to-borehole variability in the intact strength measured in the interior of the pillars for both the coal and the parting. This variability may be attributed to natural variability between the three different faces. In order to generalize the results, the data from each borehole were normalized to the measured intact strength. The normalized strength curves are illustrated in figures 14 and 15.

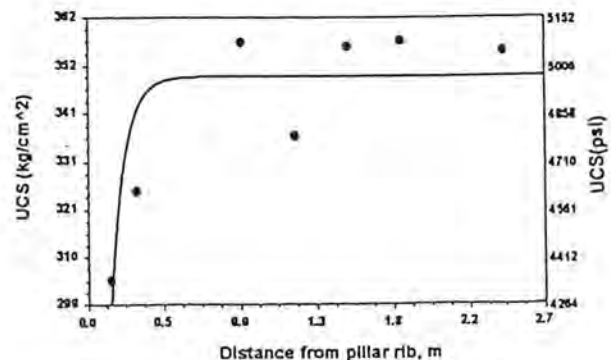


Figure 8. Best fit curve for five-year-old coal.

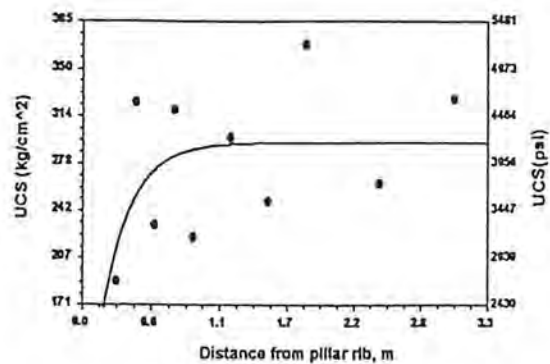


Figure 9. Best fit curve for fifteen-year-old coal.

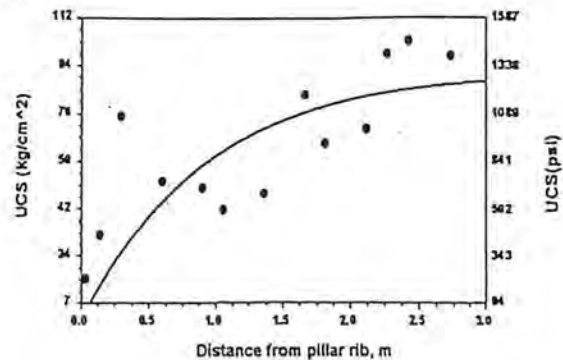


Figure 12. Best fit curve for fifteen-year-old parting.

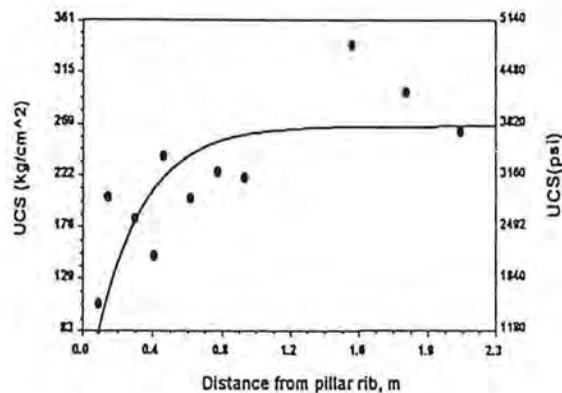


Figure 10. Best fit curve for fifty-year-old coal.

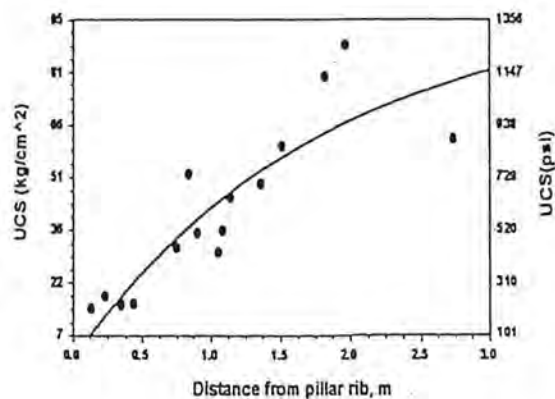


Figure 13. Best fit curve for fifty-year-old parting.

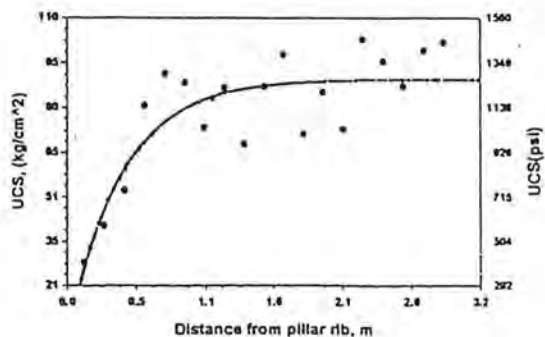


Figure 11. Best fit curve for five-year-old parting.

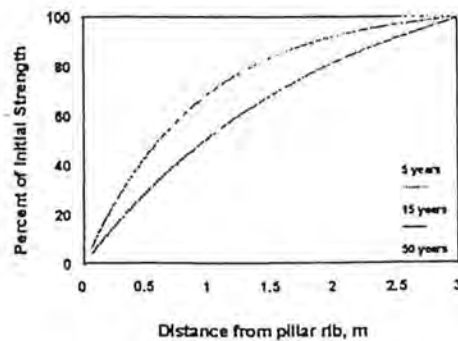


Figure 14. Time dependent strength deterioration for parting.



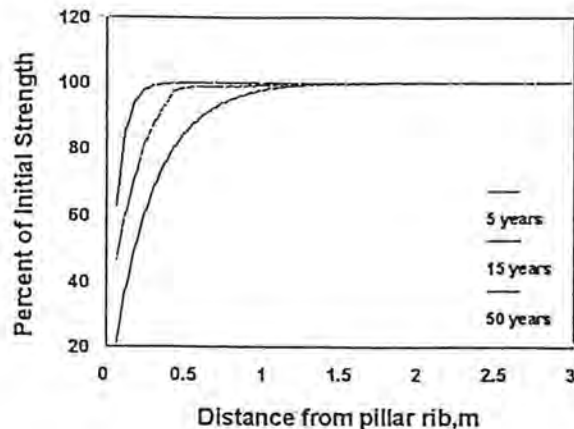


Figure 15. Time dependent strength deterioration for coal.

#### Formulation of Time Dependent Strength Deterioration

The borehole penetrometer data can be used to derive a time dependent strength formula for the pillars in the study. Using the best-fit equations shown in figures 14-15, data sets were generated for each material for all three ages. The data sets were generated for the depth ranges between 0.06 and 3m (0.2 and 10 ft). No data could be generated right at the ribline, because no BPT tests were conducted there. A non-linear regression analysis was carried out on these data sets separately for the coal and for the parting with two independent variables (time and depth) and one dependent variable (strength). A freeware software called NLREG34 was used to perform the non-linear regression. Equation (6) is the stress gradient for the parting, and (7) is the final equation for coal:

$$\% \text{ Parting Strength} = 100 (1.01 - e^{-0.3 D}) - 0.45t \quad (6)$$

$$\% \text{ Coal Strength} = 100 (1.01 - e^{-3.5 D}) - 0.13t \quad (7)$$

Where:

D = Depth into the rib, ft

t = time after mining, years

In these equations, the strength is defined as a percent of the original intact compressive strength that is assumed to be constant in the core of the pillar. Near the rib, the strength is a function of the distance from the rib (depth) and the time after mining. The relationship between the strength and the depth is a negative exponential, but that between strength and time is linear.

Unfortunately, applying these time-dependent strength equations to predict the strength of full scale-pillars is not a simple matter. Three issues are foremost:

1. Effect of parting thickness: If the parting is the pillar's weakest layer, as in this study, then a thicker parting would be expected to result in a weaker pillar.
2. Effect of parting on confining stress within the pillar: Most of the load-bearing capacity of a coal pillar is due to the development of confining stress within the pillar's core. Studies have shown that many pillars contain weak layers of clay or friable coal, but their effect on overall pillar strength is ambiguous (Mark and Barton, 1996).

3. Non-linear effect of time: In reality, the rate of strength degradation probably decreases with time, as suggested by van der Merwe (1998). Since this study included only three pillars, it was difficult to quantify the non-linear relationship between time and strength.

None the less, if the limitations of the necessary assumptions are kept in mind, it is possible to use the strength gradient equations to shed light on the possible effects of time on coal pillar stability. The following example illustrates one possible approach. The key assumption is that:

*"at any particular time, the distance from the actual pillar rib and the depth at which the strength is 60% of the intact strength will be considered as the width of the portion of the weathered zone which is not capable of carrying any load and thus transfers the load on the intact portion of the pillar"*

The effect of this assumption is that pillar's strength is decreased over time as the width-to-height ratio diminishes, while the applied stress increases as the pillar's load-bearing area is reduced.

For the calculation of the time-dependent stability factor the following steps are followed:

- a. Calculate the original stability factor using equations 1-3.
- b. Determine the strength profile at a specified time using equation 3 or 4, and determine the depth of weathering (where the strength is 60% of the intact).
- c. Calculate the resultant pillar width by subtracting the depth of weathering from the original pillar width.
- d. Recalculate the applied stress using equation 1 and the new pillar dimensions.
- e. Use equation 2 to determine the new pillar strength, and equation 3 to calculate the reduced stability factor at the specified time.
- e. Repeat this process to determine the approximate life span of the pillar.

For example, assume the following parameters:

1. The overburden depth is 243m (800 ft).
2. The pillar is a square pillar with 18.2m (50 ft) dimension.
3. The seam height is 1.8m (6 ft).
4. The entry width is 6.2 m (20 ft).
5. The in situ seam strength is 6.2 MPa (900 psi).

Since the parting is the weakest layer of the seam in this case, to be on the conservative side, the equation 6 (for the parting) is used to determine the strength profile and also the width of yielded zone due to the weathering process. Note that from the statistical point of view, it is recommended that equations 6 and 7 be used within the same time range as the original field data used in their development, namely 5 to 50 years (Myers, 1990).

Figure 16 illustrates the changes in strength and applied stress over time. Where the two curves meet, at time=35 years, the stability factor is 1.0, meaning that the pillar has a 50% chance of failing before that time.

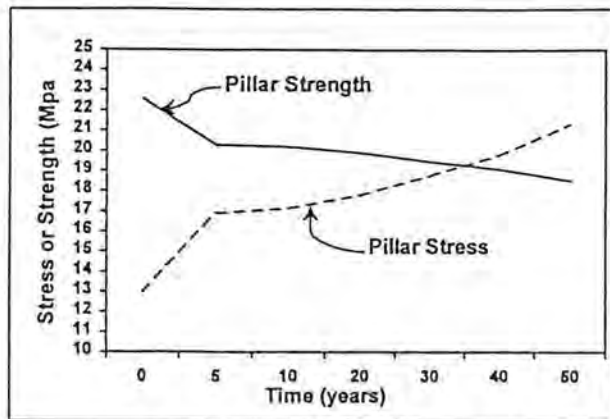


Figure 16. Safety factor reduction over time.

### CONCLUSION

The use of Borehole Penetrometer to measure the in situ time dependent strength is the unique feature of this study. It generated a set of in situ strength data in a relatively simple field-testing program. The in situ data were used to develop time dependent strength equations for coal and parting layers. An example case is used to demonstrate the use of these equations in predicting the change of stability factor over the years.

Another significant conclusion is that in this case the parting material weathered much more rapidly than the coal did. This implies that much of the observed between-seam variability in long-term pillar strength may be due to the presence or absence of partings in the coal. However, this study only addressed a single type of parting material within a single coal seam. Much work remains before the effect of time on coal pillar strength is fully understood.

### REFERENCES

- Bieniawski, Z.T., "A Method Revisited: Coal Pillar Strength Formula Based on Field Investigations," Paper in Proceedings of the Workshop on Coal Pillar Mechanics and Design, USBM IC 9315, 1992, pp. 158-165.
- Biswas, K., "Study of Weathering Actions on Partings and Its Effects on Long Term Stability of Coal Pillar," Ph. D. Dissertation, West Virginia University, 1997, 118 pp.
- Craft, J.L., and Crandall, T.M., "Mine Configuration and Its Relationship to Surface Subsidence," Paper in Proceedings, Mine Drainage and Surface Mine Reclamation, USBM IC 9184, 1988, Vol. 3, pp. 373-382.
- Hladysz, Z. "Borehole Rock Strength Tester Manual," Hladysz Rock Testers and Consulting, Rapid City, South Dakota, 1995.
- Marino, G.G. and Bauer, R.A., "Behavior of Abandoned Room and Pillar Mines in Illinois," SME Preprint 89-3, 1989, 8 pp.
- Mark C, and T. M. Barton. "The Uniaxial Compressive Strength of Coal: Should it be Used to Design Pillars?" Proceedings, 15th International Conference on Ground Control in Mining. Golden, CO, August 13-15, 1996, pp. 61-78.
- Myers, R. H., "Classical and Modern Regression with Applications," PWS-KENT Publishing Co., 1990, MA, pp 424-449.
- Tsang, P., Peng, S.S. and Biswas, K., "Current Practice of Pillar Design in U.S. Coal Mines," Mining Engineering, December 1996, pp 55-60.
- Van der Merwe, J.N., *Practical Coal Mining Strata Control*. ITASCA Africa (Pty) Ltd., Second Edition, 1998, Appendix B.
- Zhang, Y.J., Unrug, K.F and Thompson, E.D., "A New Approach to Determine In-Situ Strength of Coal Pillar," Mining Engineering, Oct. 1996, pp. 49-53.