

Optimized Impingement with Reduced Splatter

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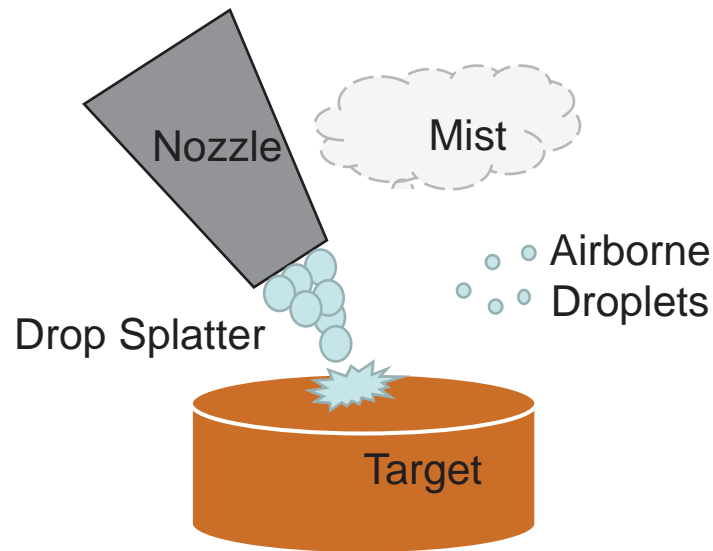
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Presentation Outline

- Purpose of Study
- Past Literature
- Set-up (Experimental & Numerical)
- Results
- Conclusions and Future Direction

Purpose of study



Spray applications: Cooling, lubricating, spreading, coatings industries

Consequences: small airborne droplets and mists that present occupational risk factors for workers. (inhaled & ingested by workers)

Hazard Evidence: asthma, hypersensitive pneumonitis, lung cancer, cancer of esophagus, pancreas, larynx, colon and rectum due to prolonged exposure to aerosols.

Purpose of study contd.

Permissible Exposure Limits

OSHA : 5 mg/m³ for oil-mists.

NIOSH : 0.5 mg/m³ for total suspended particulates.

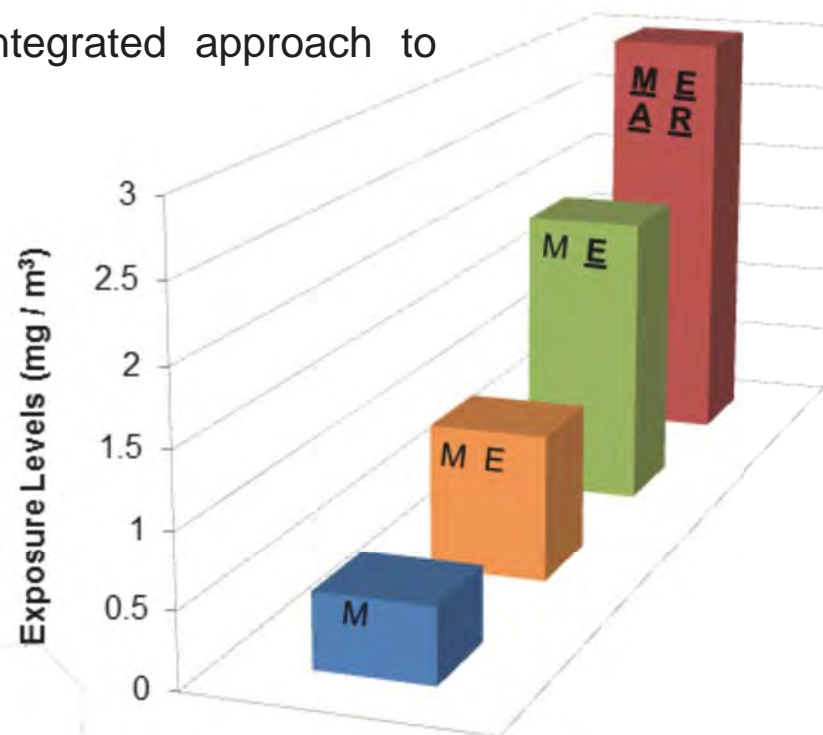
Study by Coehn et al.^[1] proposed an integrated approach to minimize exposure by incorporating:

A: administrative controls (e.g. job rotation)

E: engineering control and

R: provision respiratory protection.

Recommend (M) medical surveillance for all levels of exposure.



Thus, it is crucial to minimize splash from impinging drops and thus reduce human contact.

Past Literature

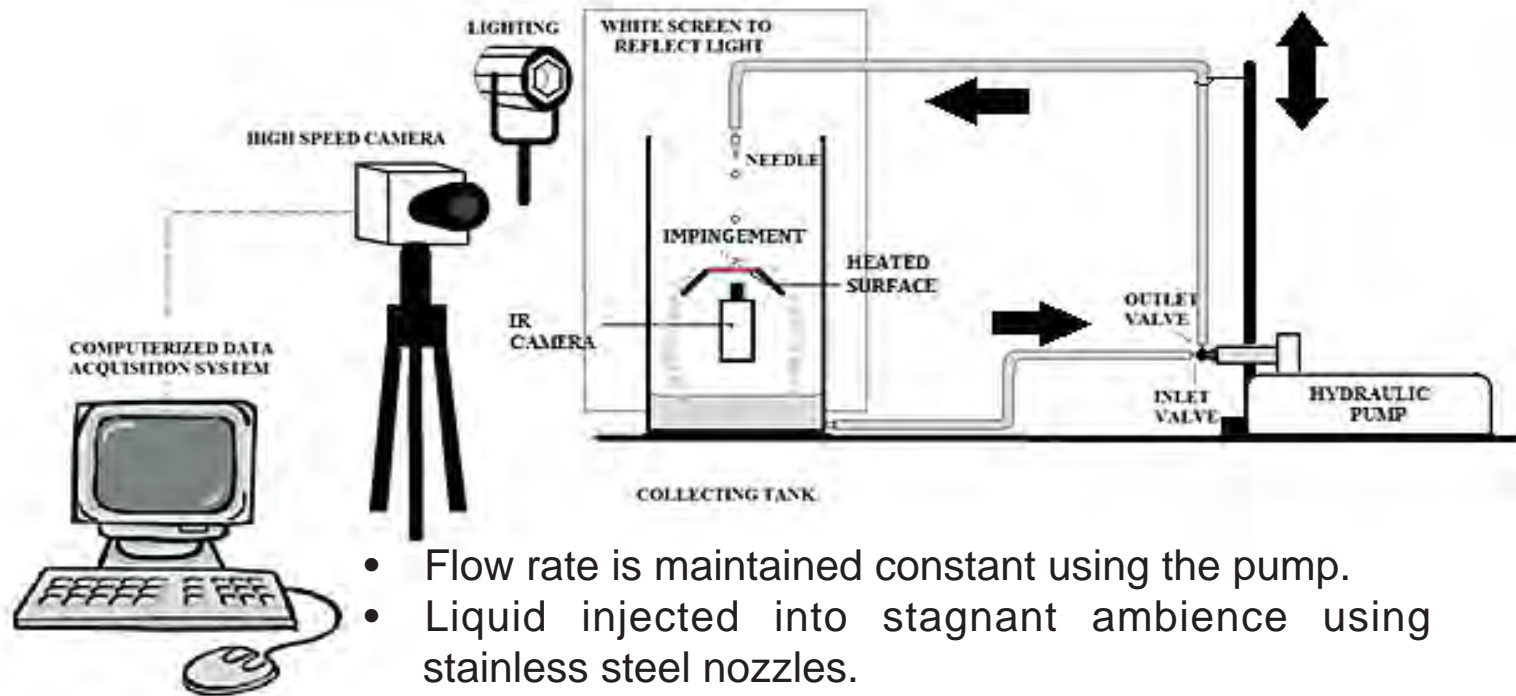
- Studies on reducing splash look at eliminating or reducing impingement:
 - Cryogenic studies ^[1]:
 - requires increased safety measures
 - can cause physical burn on contact
 - Others studies are application specific
 - minimizing fluid usage^[3]
 - optimizing heat transfer while minimizing drop size ^[4]
- Need to look at minimizing splash due to impact.
 - Most drop impact studies: impact on dry surface or on deep pools
 - More studies required on impact on thin film surface

Variation in the few studies that look at drop impact on thin films:

- Mundo ^[5], Cossoli ^[2] and Riobbo ^[7] : viscosity inhibits splash
- Rang and Feuillebois ^[6] : viscosity has no impact
- Vander Wal ^[8] and Xu ^[9]: viscosity promotes splashing

**Requires a physical understanding of splash
and means to predict it**

Experimental Setup

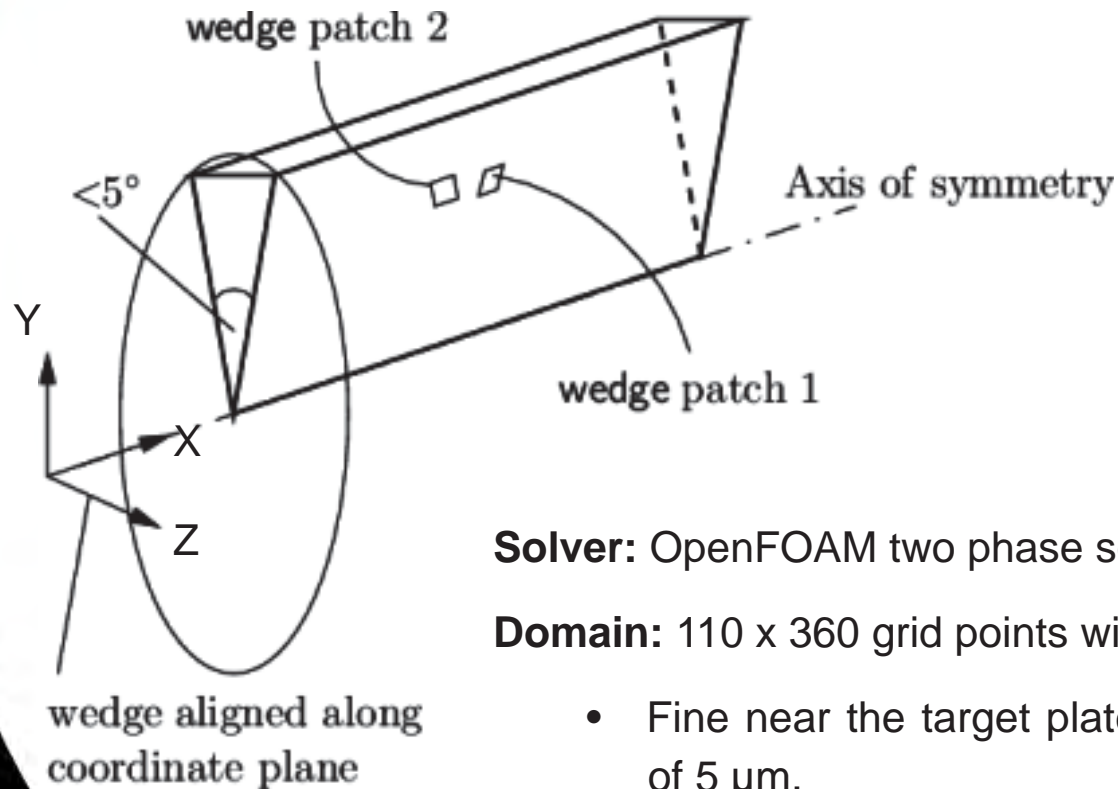


- Flow rate is maintained constant using the pump.
- Liquid injected into stagnant ambience using stainless steel nozzles.
- Liquid is impinged on a copper plate that has heaters at the bottom. The IR Camera (FLIR E60) is placed under the copper plate.

IMAGE CAPTURE:

- A high speed camera (NAC Image technology) at 2000 fps is used.
- Image processing – Image-Pro Plus 4.0
- Calibration: a standard SS needle.

Numerical Setup

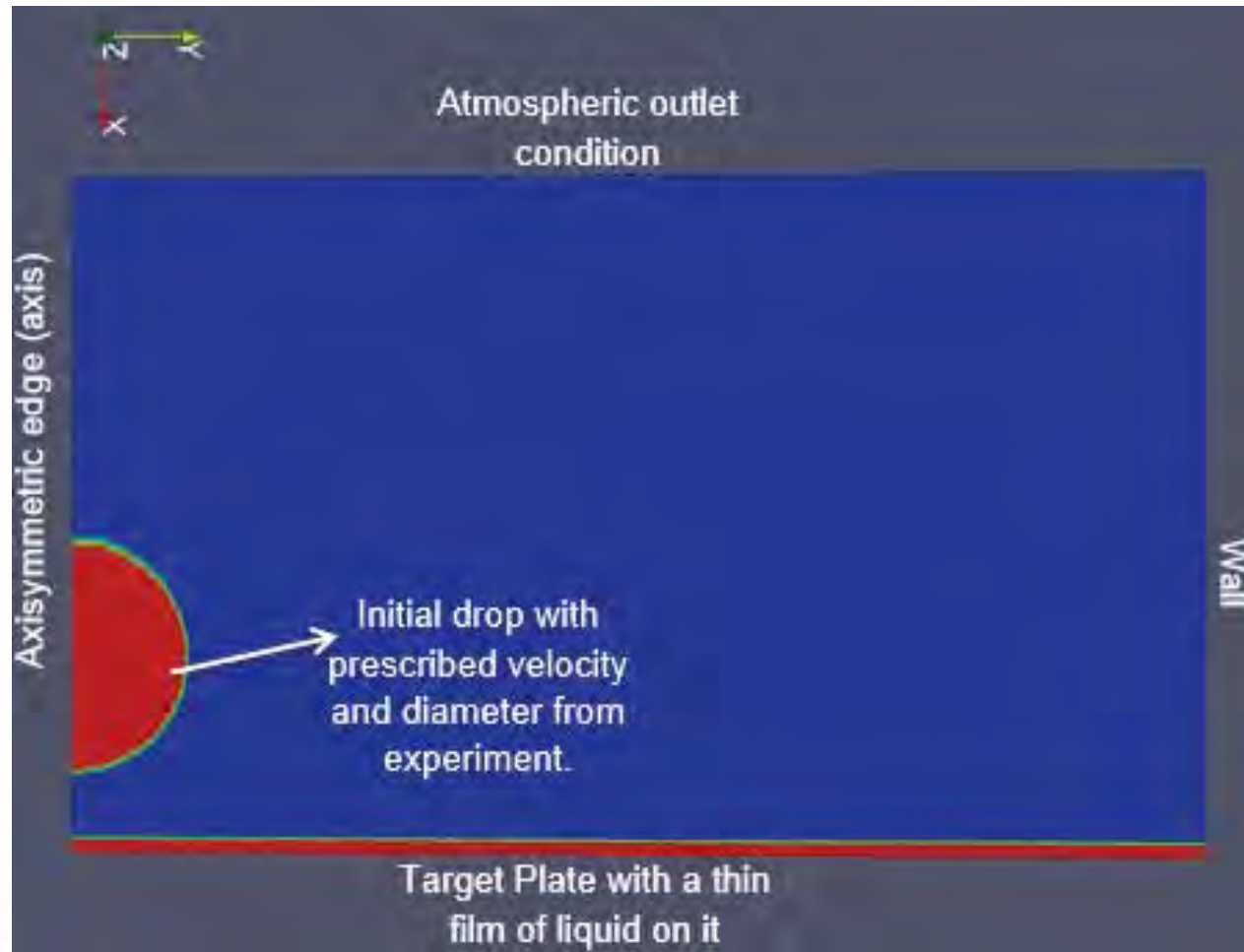


Solver: OpenFOAM two phase solver using VOF technique

Domain: 110 x 360 grid points with a total of 39,600 cells.

- Fine near the target plate with a minimum grid size of 5 μm .
- The aspect ratio of the mesh is maintained close to one near the target plate.

Initial Case Configuration



Results

The most common forms of correlations developed in the past are:

$$We \downarrow c = C = \text{constant}^{[8, 5]} \quad (\text{equation 1})$$

$$We \cdot Oh \uparrow^{-0.4} = K = \text{constant}^{[2, 7]} \quad (\text{equation 2})$$

Reason for variation in correlation:

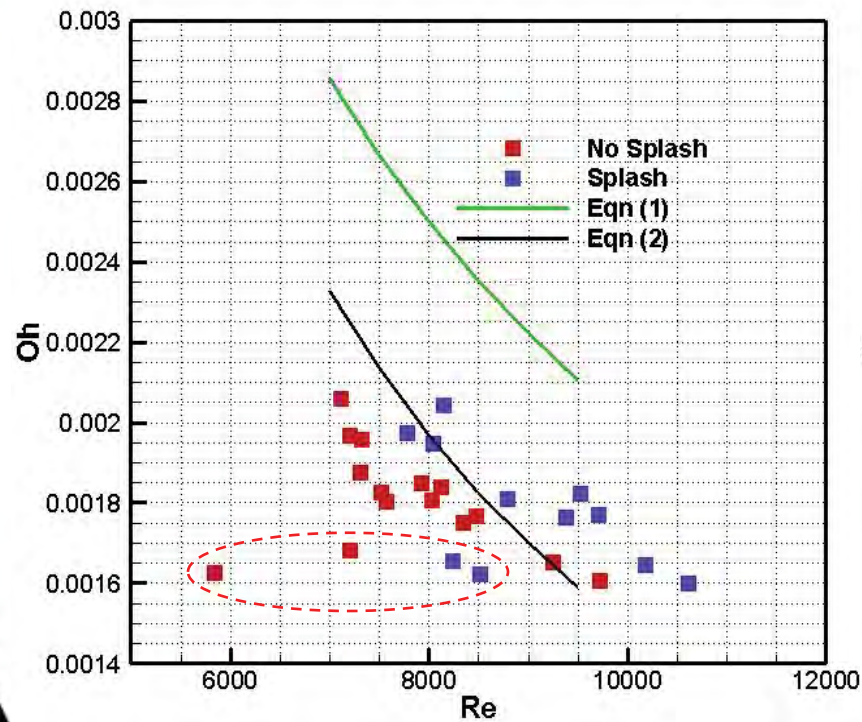
- Liquid properties
 - Viscosity Effect
 - Surface Tension
- Film thickness

Current Experimental parameters:

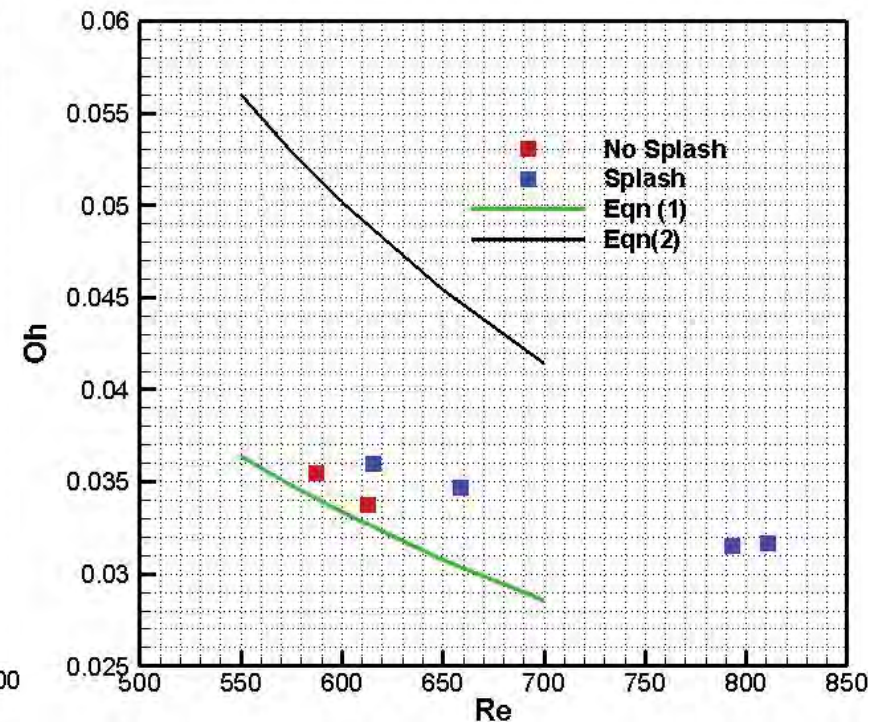
- Film thickness: 0.02 – 0.15 times drop diameter
- Needle diameters: 0.8284 mm to 1.5 mm
- Working liquids: Water and Ethylene glycol
 - Viscosity : 1 and 16.1cP
 - Surface tension : 72.8 and 48.4 dynes/cm
 - Density: 1000 and 1113.2 kg/m³

Results contd.

Water



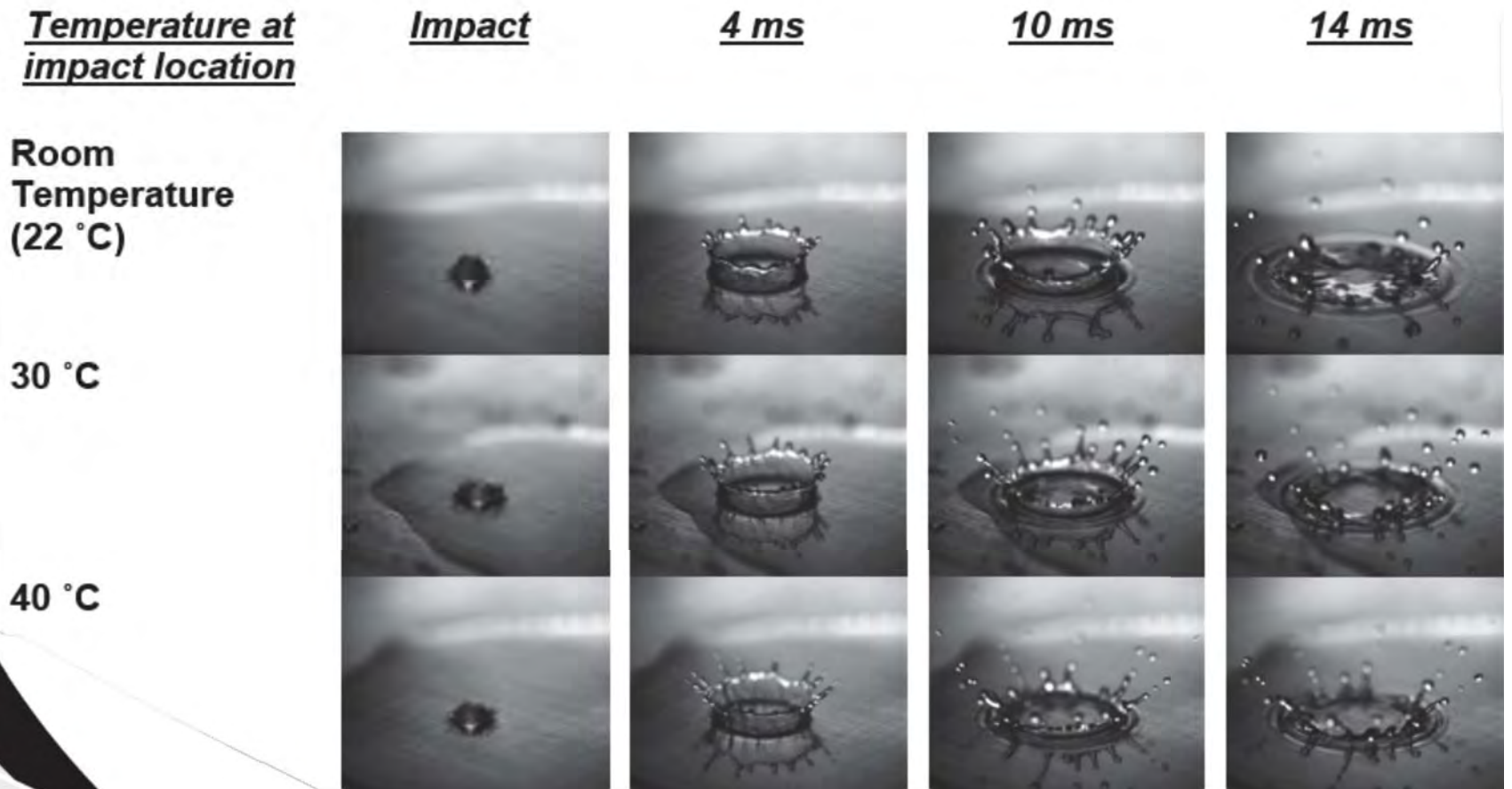
Ethylene Glycol



- Suggested correlations are not consistent.
- Large diameter drops behavior differently.
when Drop diameter > capillary length the pattern is different : suggests significance of gravitational force

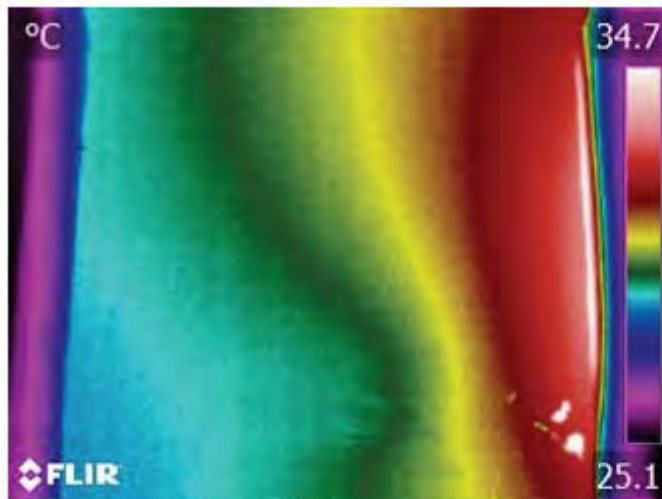
Results contd.

Influence of surface temperature on splash pattern



Results contd.

Instantaneous Surface Temperature Profile during splash



Impact location initial temperature = 30 °C



Impact location initial temperature = 40 °C

Nusselt number (a measurement of convective heat transfer to conductive heat transfer) is higher for impact temperature of 30 °C.

A steady state thermal analysis is required: continuous drop impact on the constant heat flux surface will help determine the thermal behavior at steady state.

Numerical model validated

Time

Experimental

Numerical

Impact



4 ms



14 ms



18 ms



24 ms



Drop diameter: 4.146 mm
Impact Velocity: 2.303 m/s
Re: 9530

Conclusions and Future Direction

- Past scaling analyses are unable to predict onset of splash.
 - Effect of gravitational force has been identified.
 - Effect of target surface temperature has been noted.
- Computational modeling and validation for existing model has been performed.
- Current numerical two phase models for viscous liquid are not good. A better way to model this using better numerical interface tracking has been developed. Experimental validation is being conducted. (results not presented)

Conclusions and Future Direction

- More liquids (wider range of properties) needs to be tested to understand physical phenomena.
- Predictive correlation from experimental observation with numerical understanding to be developed
- Steady state drop impingement heat transfer: experimental and numerical study.
- Array of droplets splashing: optimal distance between droplets impacting.

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