

Hadnot Point, Camp Lejeune, NC

Reconstruction of Historical Contaminant Concentrations: A Computational Method

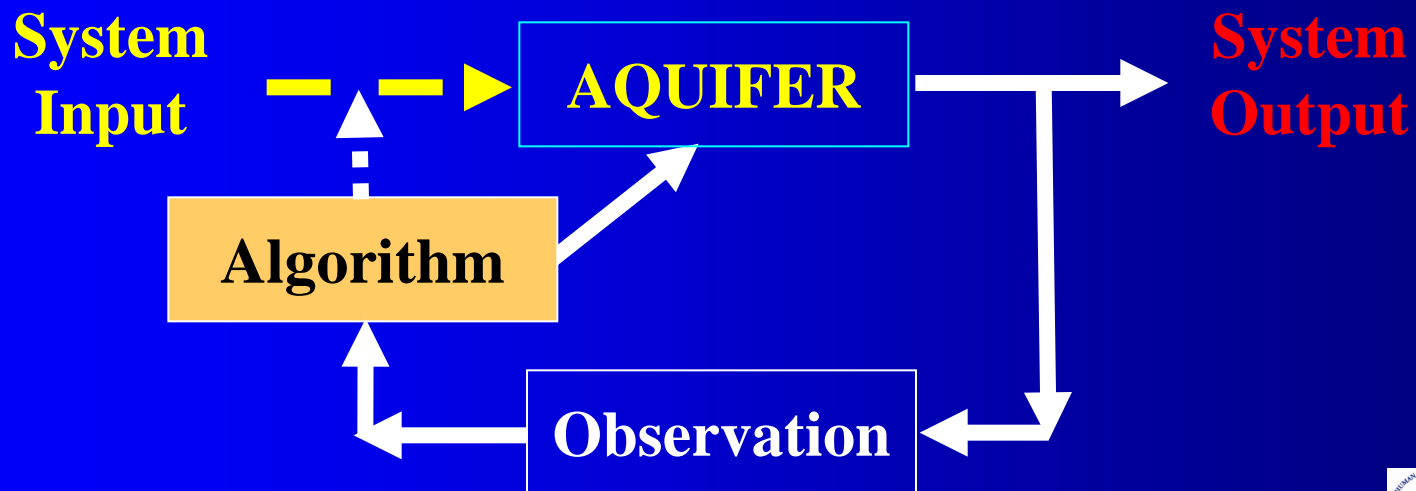
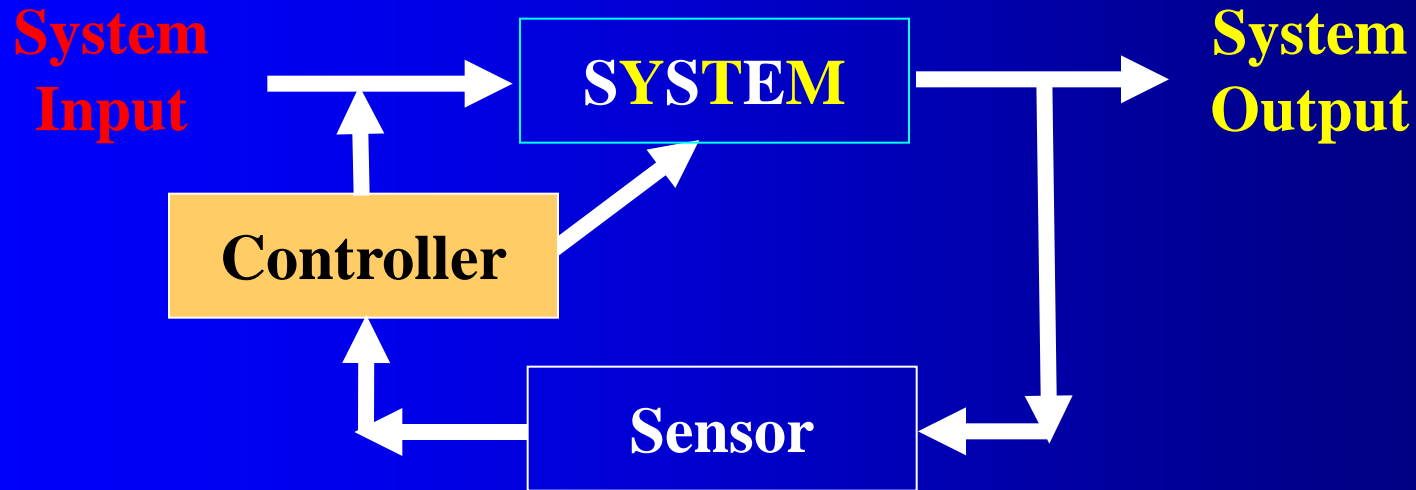
M. M. Aral and J. Guan

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ATSDR/CDC***

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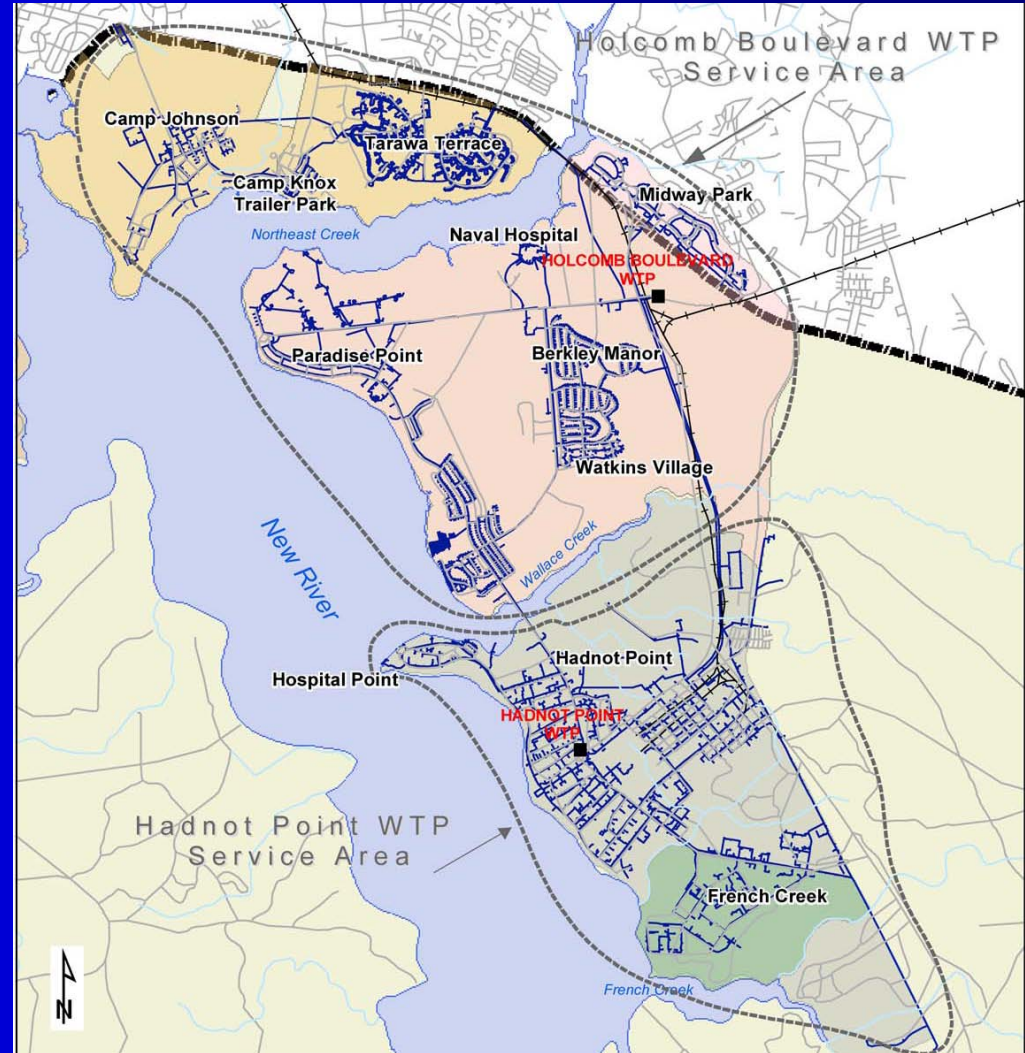
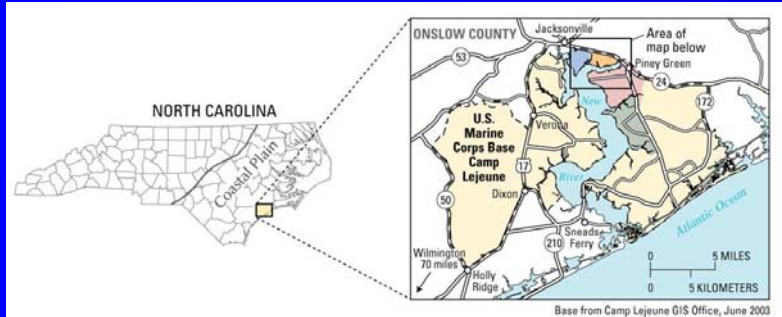
Control Theory Based Time Series Analysis



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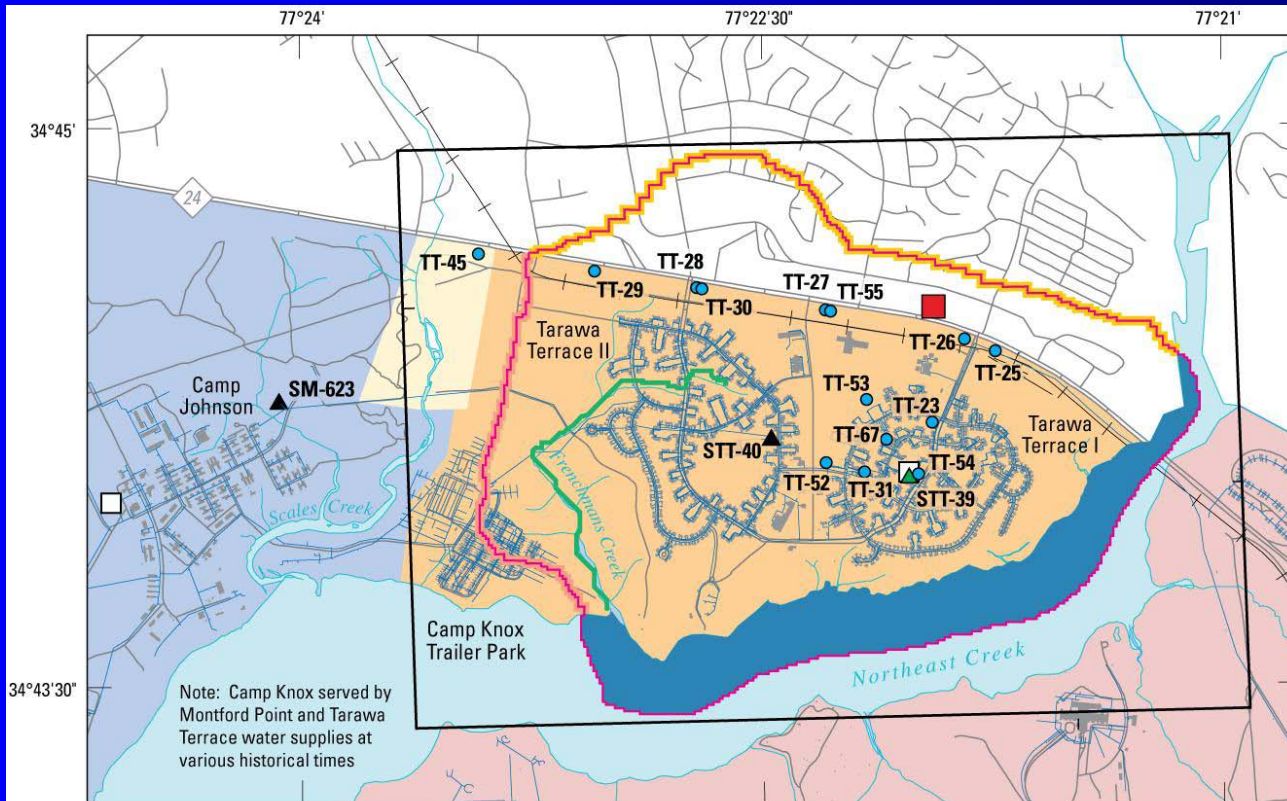
Camp Lejeune, NC Site:



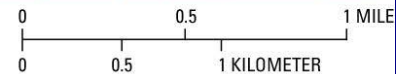
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Tarawa Terrace Study:



Base from U.S. Marine Corps and U.S. Geological Survey digital data files



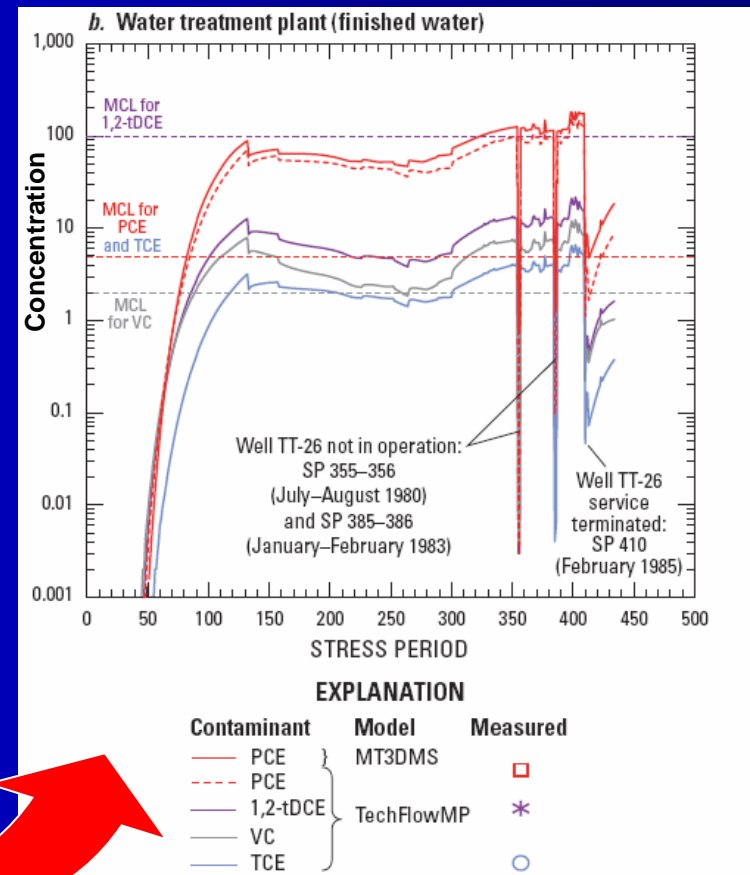
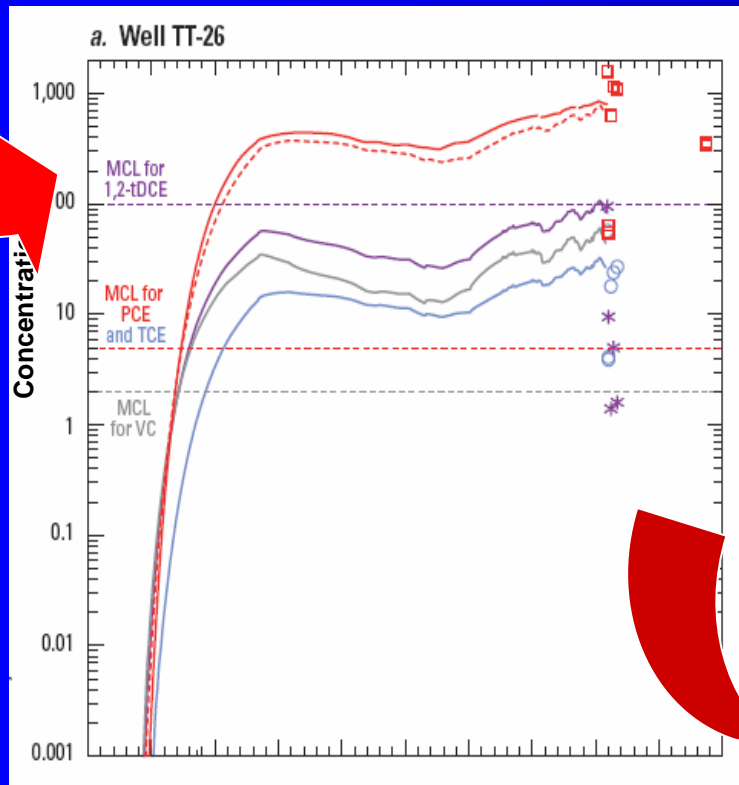
EXPLANATION

- | | | |
|---|---|--|
| <p>Historical water-supply areas of Camp Lejeune Military Reservation</p> <ul style="list-style-type: none"> Montford Point Tarawa Terrace Holcomb Boulevard Hadnot Point Other areas of Camp Lejeune Military Reservation | <p>Water distribution</p> <ul style="list-style-type: none"> Tarawa Terrace water pipeline ▲ SM-623 Elevated storage tank and number ▲ STT-39 Ground storage tank and number Water treatment plant (closed 1987) TT-26 Water-supply well and identification | <p>Groundwater-flow and fate and transport model boundaries</p> <ul style="list-style-type: none"> Domain Active area <p>Boundary conditions for groundwater-flow model</p> <ul style="list-style-type: none"> General head Drain No flow Specified head <p> ABC One-Hour Cleaners</p> |
|---|---|--|



Tarawa Terrace Study:

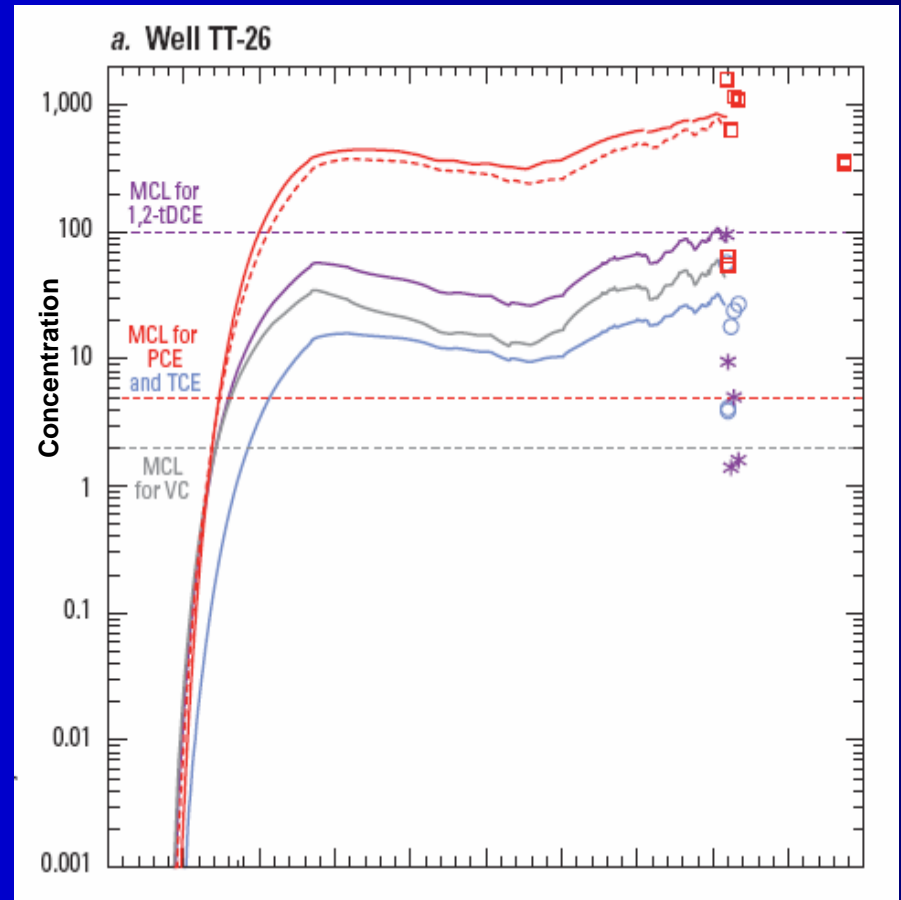
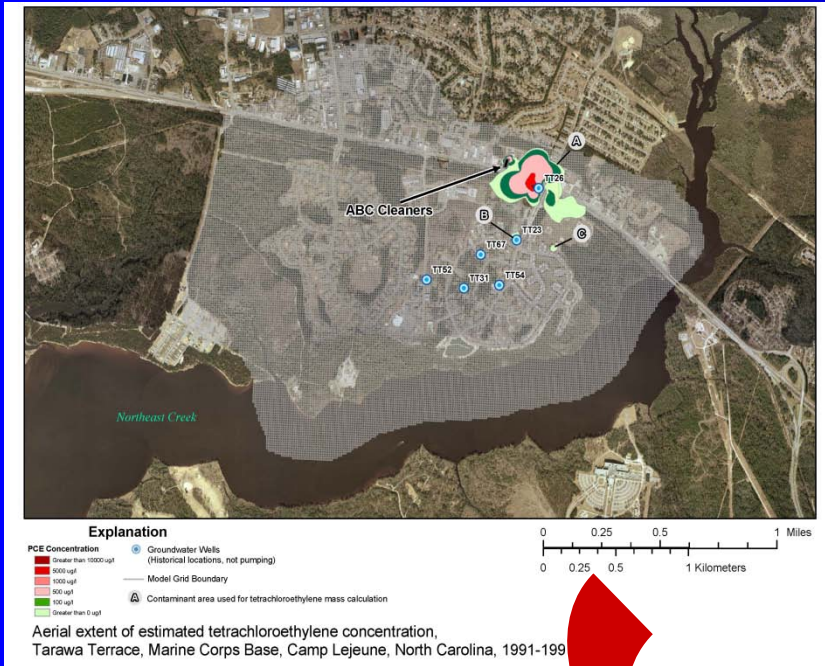
- Site data collection;
- Groundwater flow and contaminant fate and transport modeling;
- Mixing model; and,
- WDS system studies;



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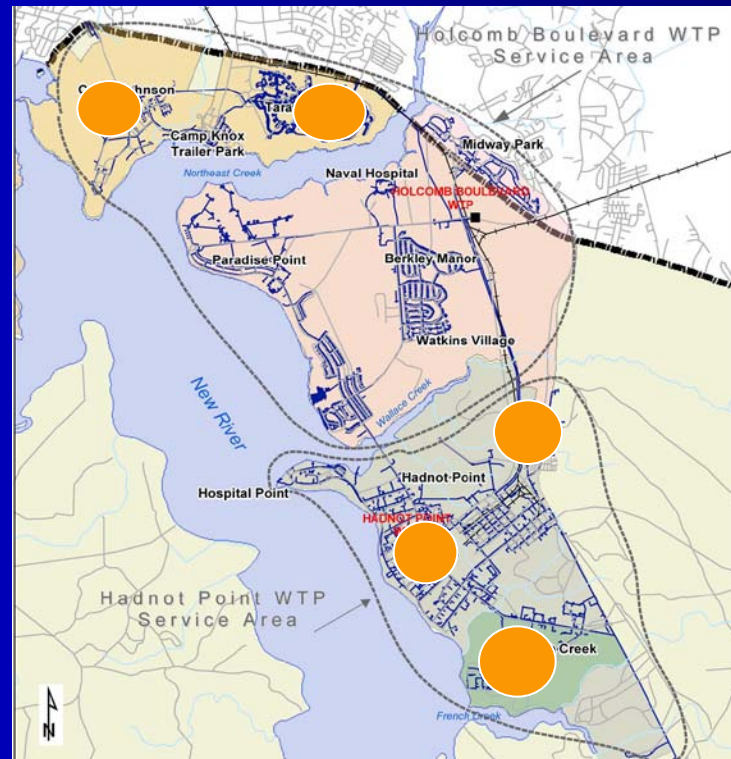
The Purpose of the current study:



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Starting Point and Expectations:

- The proposed method will be a screening level procedure;
- The proposed method is to be used locally (Source, GW Hyd. and fate);
- The accuracy expected from the model is a function of the quality and quantity of the data available at the locale;
- In locations where sufficient data is not available the proposed model cannot be used;
- The proposed model can be used for distinct multiple chemical sources (PCE, Benzene) at a locale by repeating the process for each chemical which shows a different finger print at the observation points.



Our Understanding of GW Modeling:

- Groundwater flow modeling:

$$\frac{\partial(\phi s_f \rho_f)}{\partial t} = \nabla \cdot \left[\frac{\rho_f k_m k_{rf}}{\mu_f} (\nabla P_f + \rho_f g \nabla z) \right] + I_f \quad ; \quad f = w, g$$

- Groundwater fate and transport modeling:

$$\frac{\partial(\phi s_f C_f^i)}{\partial t} = \nabla(\phi s_f D_f^i \nabla C_f^i) - \nabla(q_f C_f^i) \pm I_{f,MT}^i + I_{f,BT}^i + I_{source} \quad ; \quad f = w, g$$

$i = 1, 2, 3, \dots$

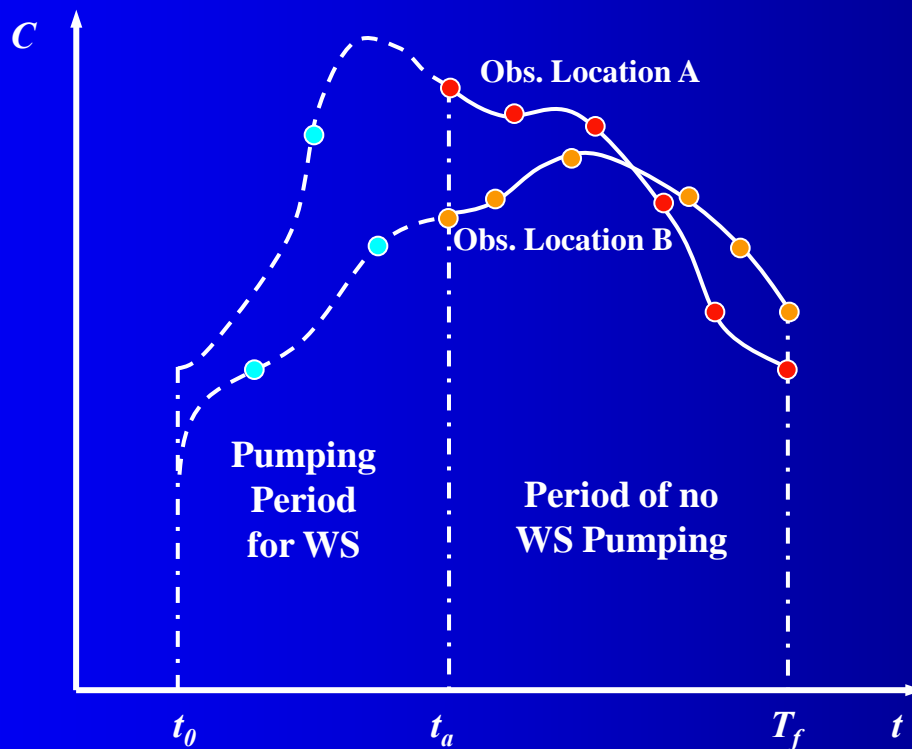
- Matrix equations:

$$[\mathbf{M}] \frac{\partial \{C_f^i\}}{\partial t} = [\mathbf{S}] \{C_f^i\} \pm \sum \{F_f^i\} \quad ; \quad f = w, g$$

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Available Data for Historical Reconstruction:

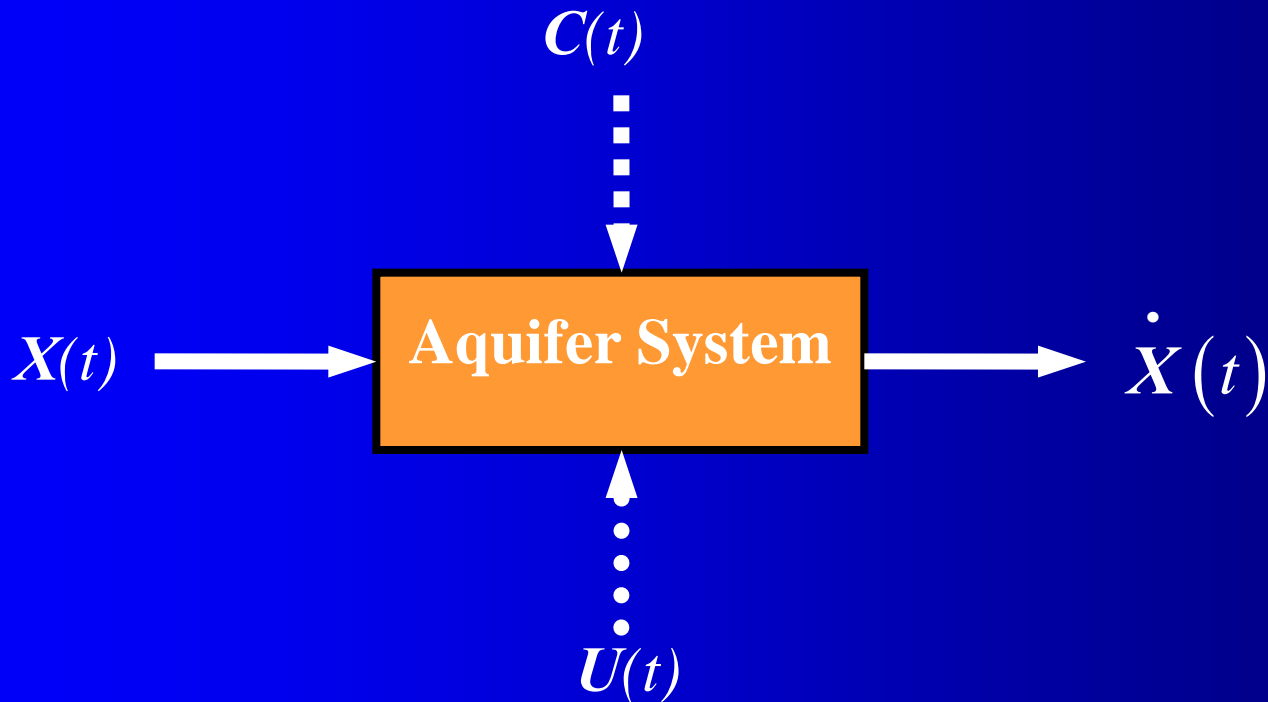


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Idealization of the System:



$$X(t) = [x_1(t), x_2(t), x_3(t), \dots, x_i(t), \dots, x_n(t)]^T$$

Contaminant concentrations at monitoring wells

$$U(t) = [u_1(t), u_2(t), u_3(t), \dots, u_j(t), \dots, u_m(t)]^T$$

Pumping rates at wells

$$C(t) = [C_1(t), C_2(t), C_3(t), \dots, C_i(t), \dots, C_\ell(t)]^T$$

Contaminant concentrations at the source



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The Proposed Method:

$$\left. \begin{aligned} \dot{X}(t) &= \Phi X(t) + \Psi U(t) \\ X(t_0) &= X_0 \end{aligned} \right\}$$

Φ

is the $(n \times n)$ matrix associated with aquifer parameters, BCs, contaminant sources & fate etc.

Ψ

is the $(n \times m)$ matrix associated with pumping rates at extraction wells

$\dot{X}(t)$

is the time derivative of the contaminant concentration vector at observation points

X_0

is the initial contaminant concentration vector at the observation locations

$U(t)$

is the pumping rate vector at pumping locations



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The Proposed Method:

- If we use forward time integration:

$$\left. \begin{aligned} X(k+1) &= [\Phi \Delta t + \mathbf{I}] X(k) + \Delta t \Psi U(k) \\ X(t_0) &= X_0 \end{aligned} \right\}$$

$$\mathbf{A} = [\Phi \Delta t + \mathbf{I}]; \quad \mathbf{B} = \Psi \Delta t$$

$$\left. \begin{aligned} X(k+1) &= \mathbf{A} X(k) + \mathbf{B} U(k) \\ X(t_0) &= X_0 \end{aligned} \right\}$$

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The Proposed Method:

- If we use backward time integration:

$$\left. \begin{aligned} X(k) &= A^{-1}X(k+1) - A^{-1}BU(k) \\ X(T_f) &= X_f \end{aligned} \right\}$$

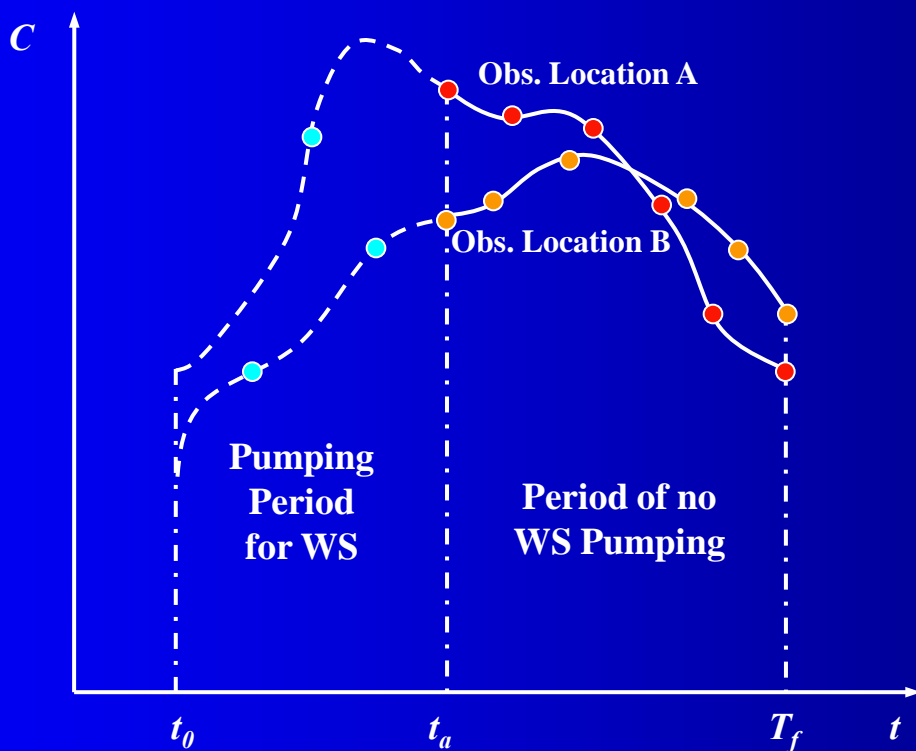
$$A_b = AB^1; \quad B_b = -A^{-1}$$

$$\left. \begin{aligned} X(k) &= A_b X(k+1) + B_b U(k) \\ X(T_f) &= X_f \end{aligned} \right\}$$

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Data Available for Historical Reconstruction:



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The Proposed Method: First Step

$$\left. \begin{aligned} X(k+1) &= \mathbf{A}X(k) + \mathbf{B}U(k) \\ X(t_0) &= X_0 \end{aligned} \right\}$$

- For the period we have data from MW, we have $U(k) = 0$:

$$X(k+1) = \mathbf{A}X(k)$$

- Least squares method can be used to determine the coefficients of the matrix \mathbf{A}



The Proposed Method: Second Step

- Given the matrix **A** optimization methods can be used to determine the coefficients of the matrix **B**

$$\mathbf{X}(k+1) = \mathbf{A}\mathbf{X}(k) + \mathbf{B}U(k) \quad c$$

$$\mathbf{X}(t_0) = 0$$

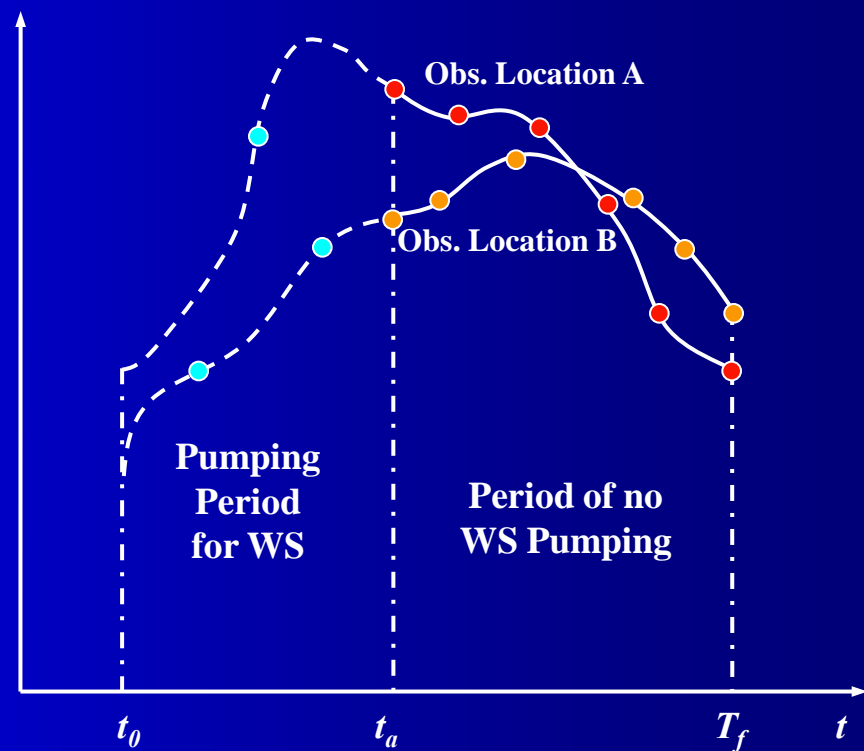
$$f = \min_{\mathbf{B}} \left\{ \frac{1}{2} \sum_{i=1}^n (x_i(t_a) - x_i^*(t_a))^2 \right\}$$

subject to:

$$\mathbf{X}(k+1) = \mathbf{A}\mathbf{X}(k) + \mathbf{B}U(k)$$

$$\mathbf{X}(k) \geq 0$$

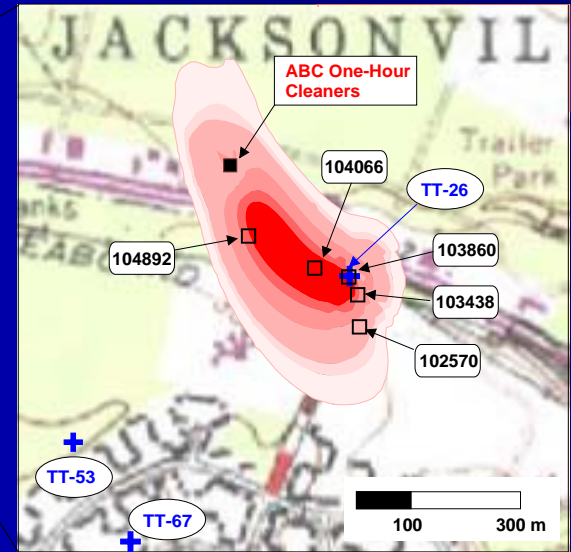
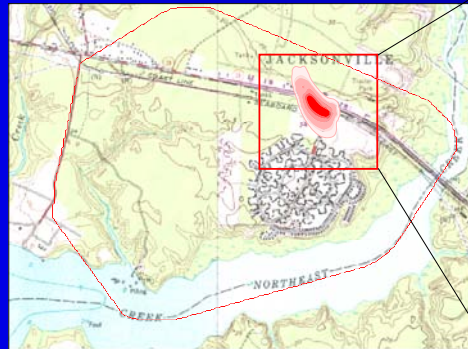
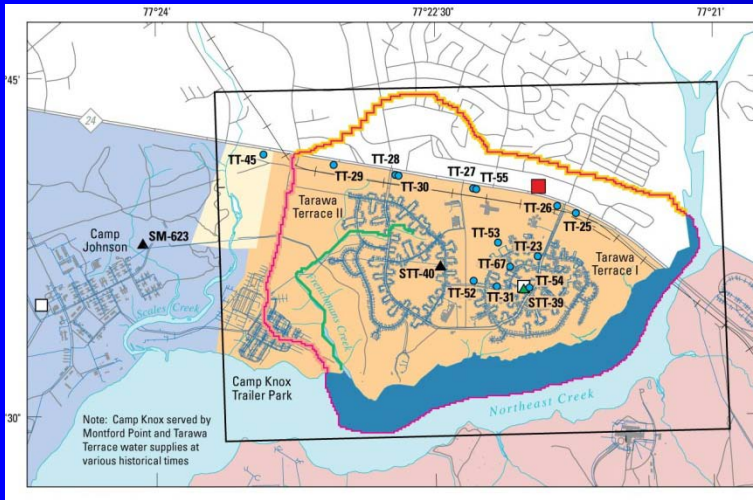
$$\mathbf{X}(t_0) = 0$$



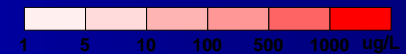
- The proposed method is based on these principles and algorithms

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Verification Study: Tarawa Terrace Data



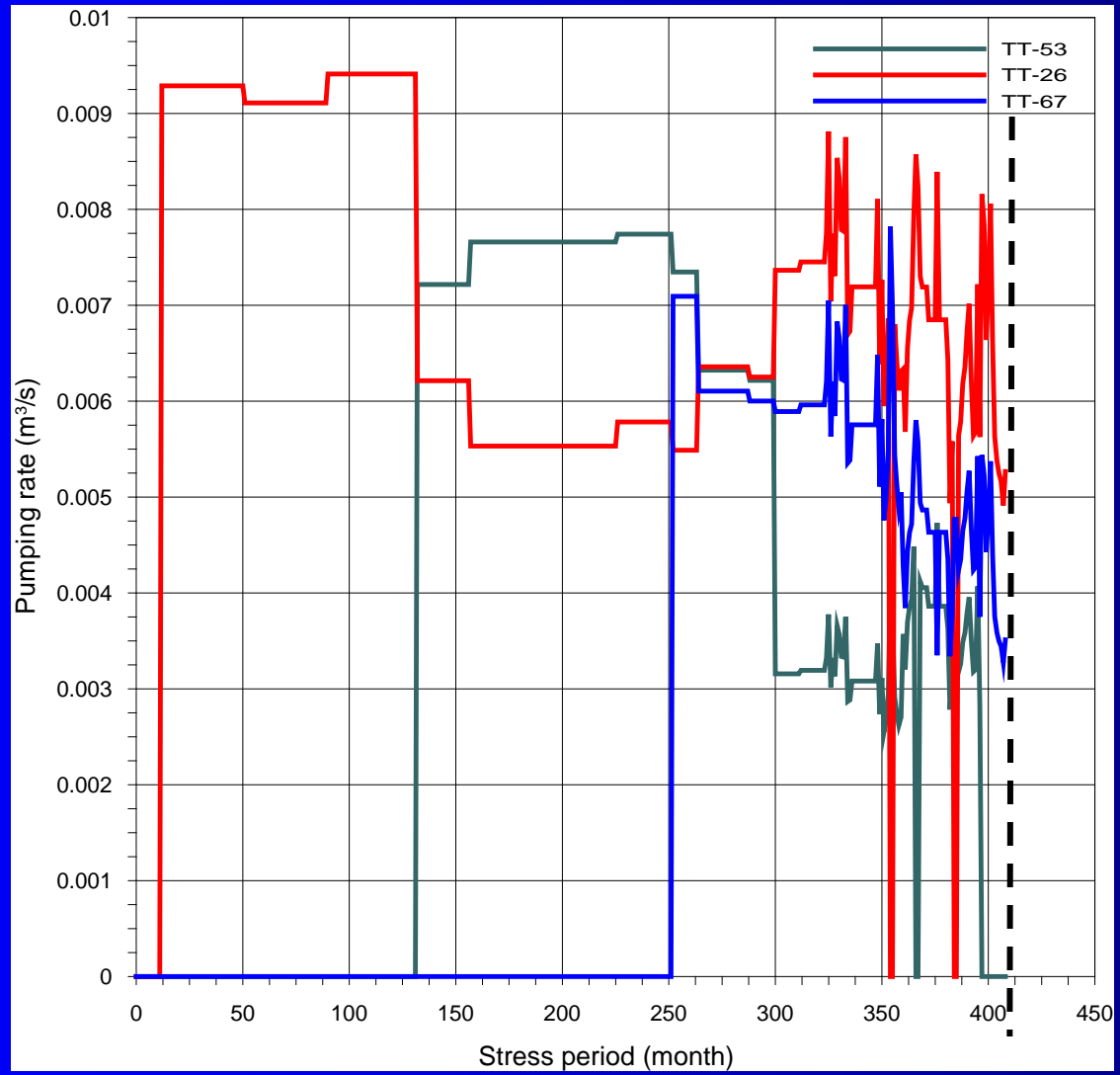
- Three pumping wells: TT-26, TT-53, and TT-67
- Five monitoring points.



PCE concentration distribution in December 1984 (stress period=408) at z = -24 m.

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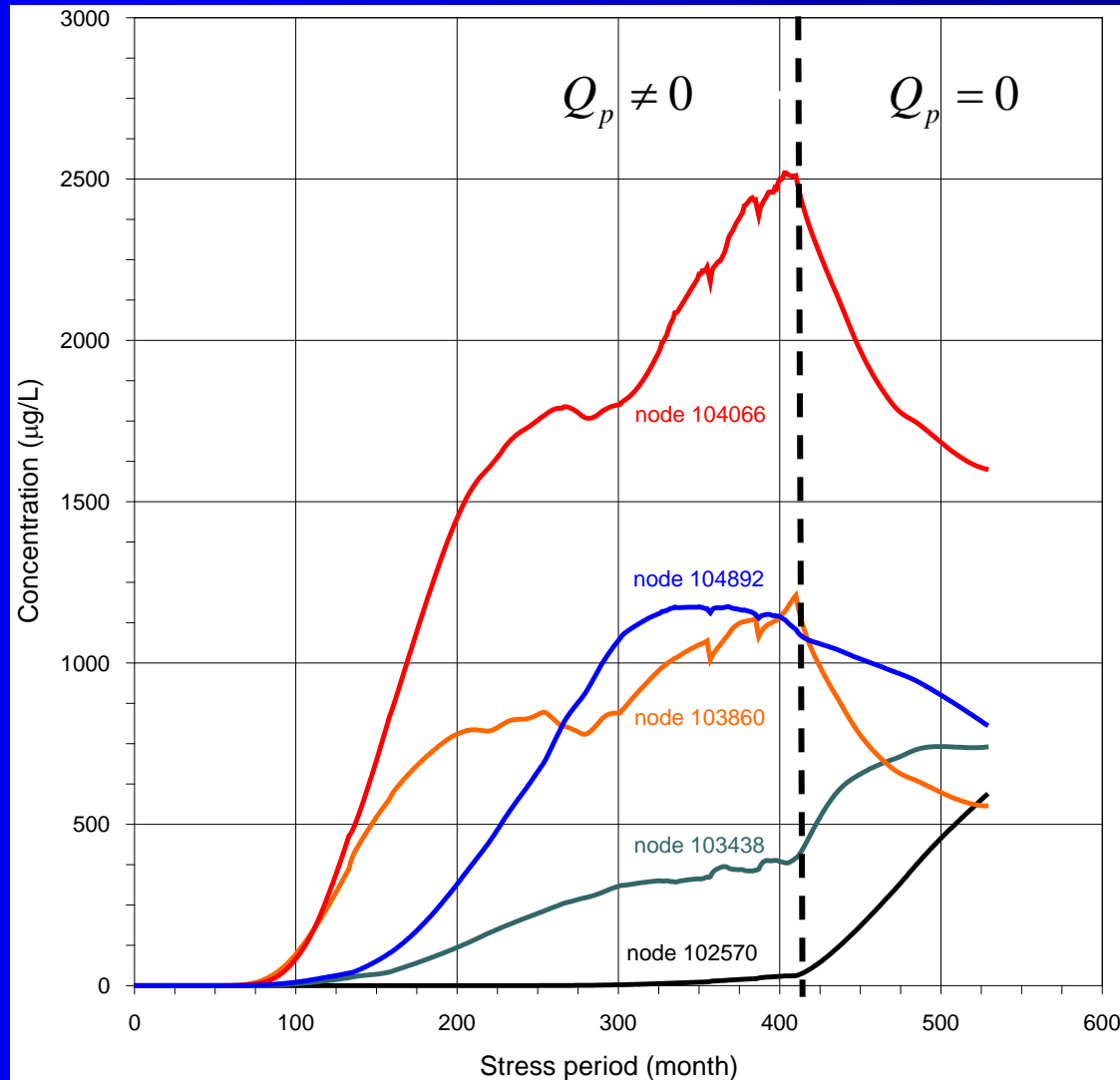
Tarawa Terrace Pumping Schedule:



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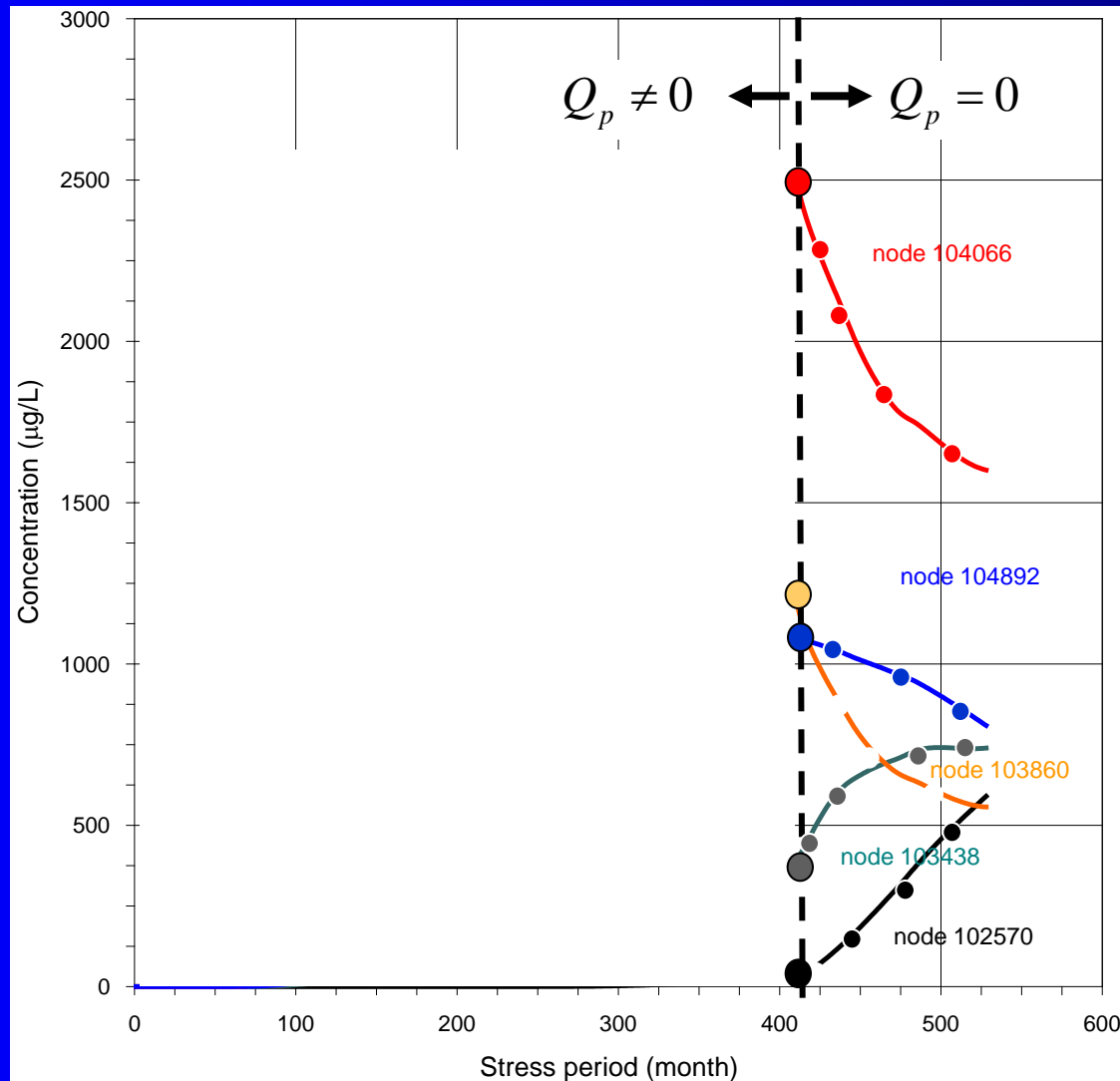
Tarawa Terrace Data:



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Tarawa Terrace Data:

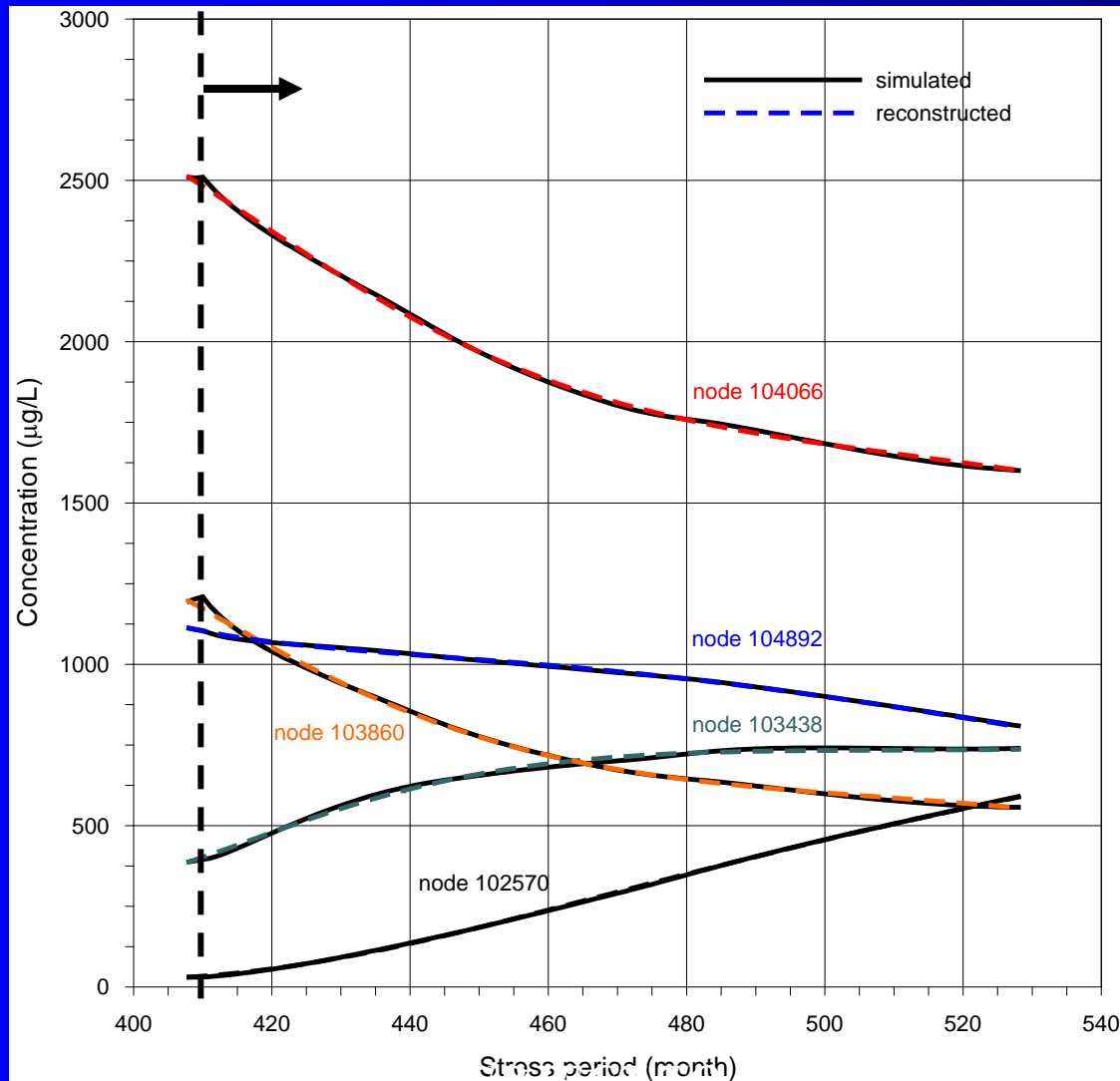


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Tarawa Terrace Outcome: LSM

$$X(k+1) = \mathbf{A} X(k)$$



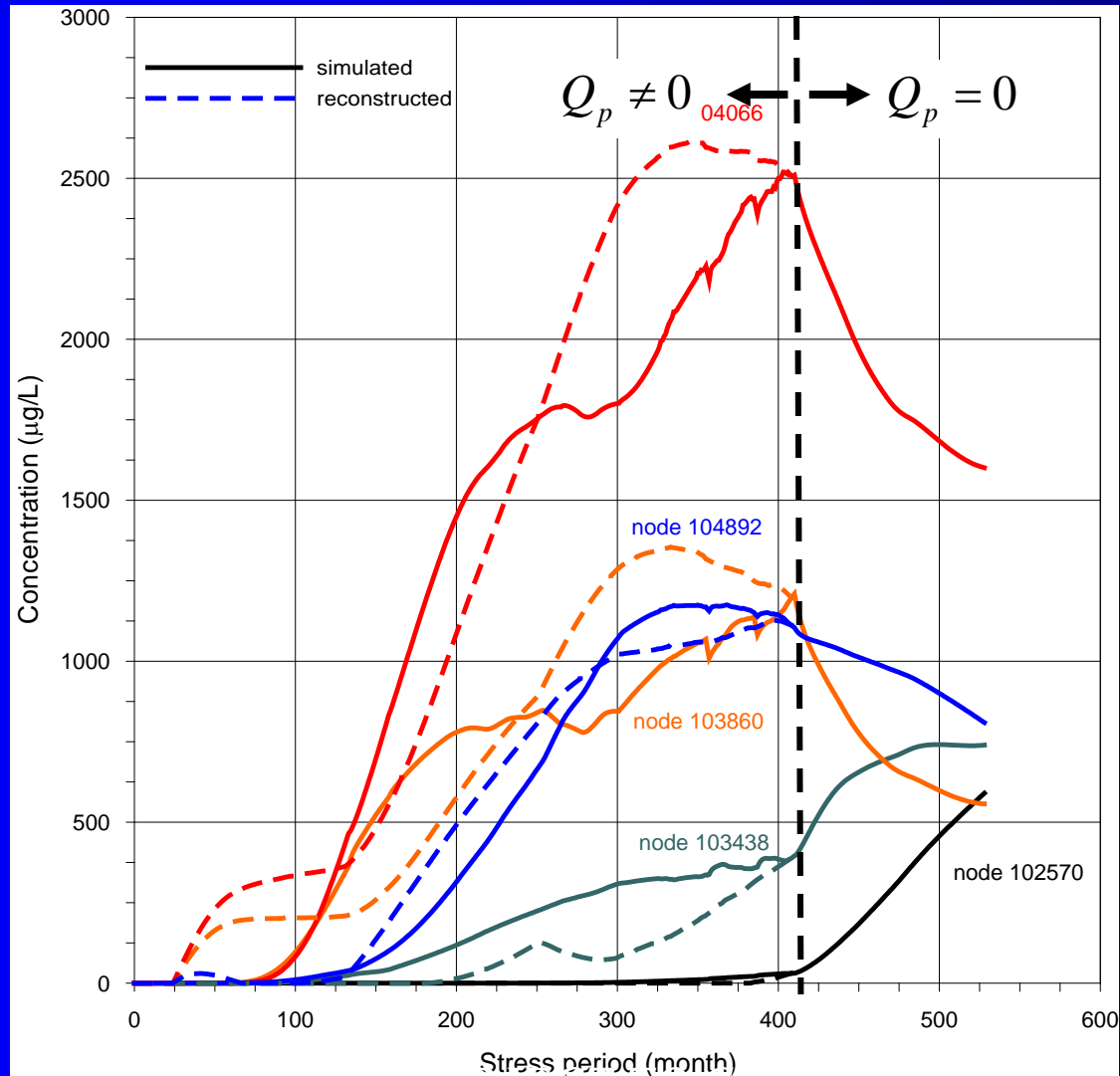
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Tarawa Terrace Outcome (FW - 0 Int. points):

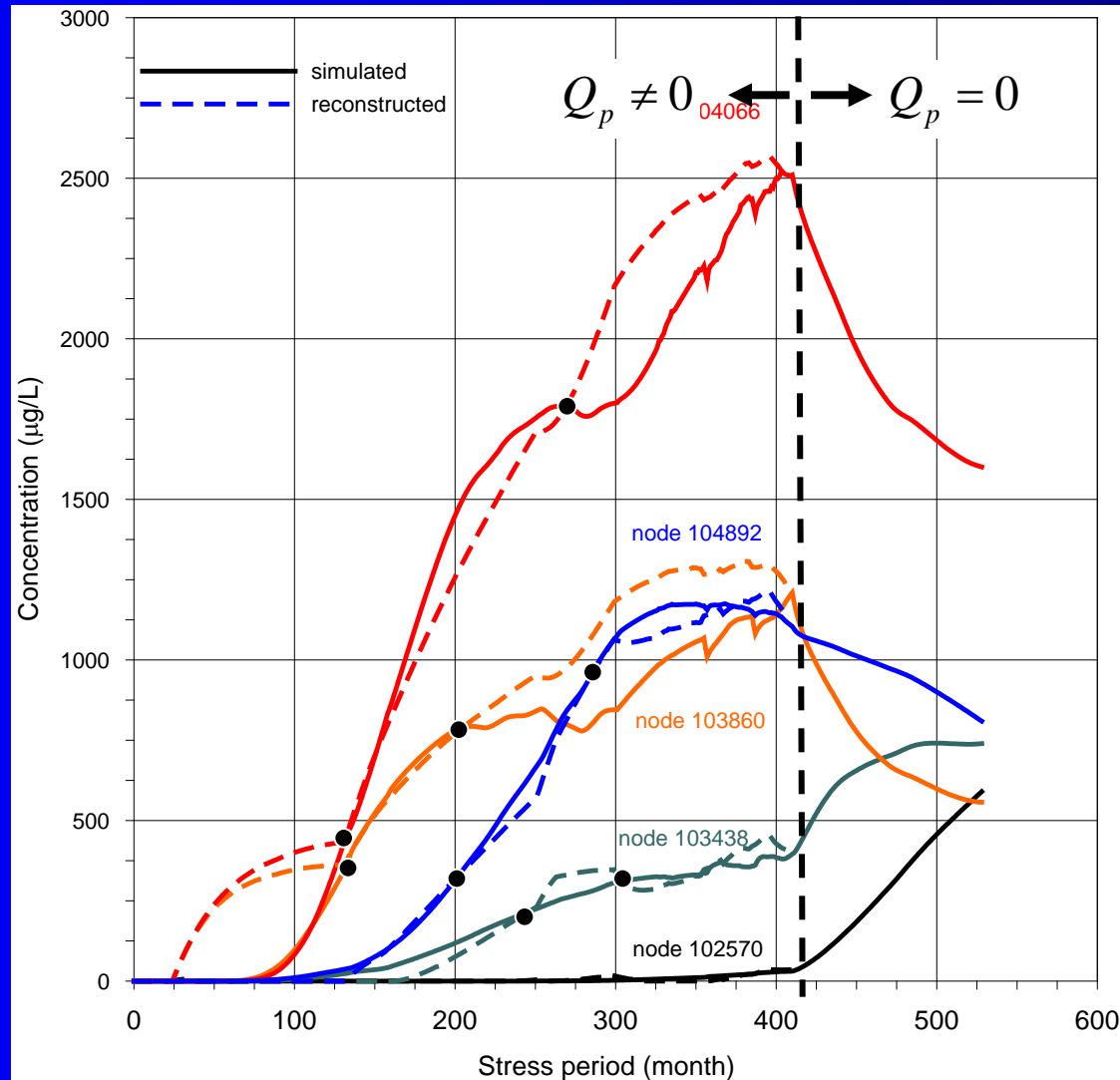
$$X(k+1) = \mathbf{A}X(k) + \mathbf{B}U(k)$$



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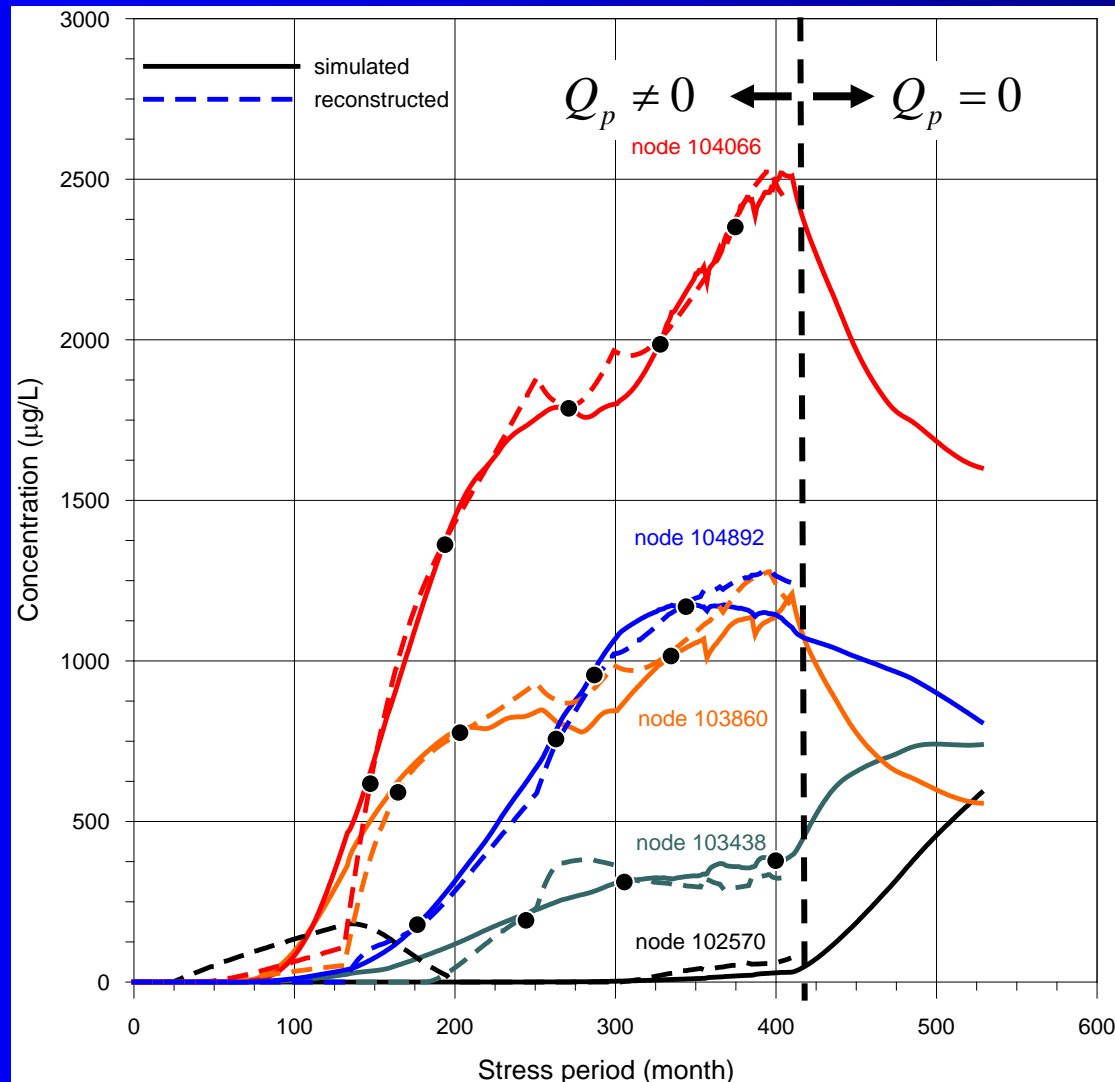
Tarawa Terrace Outcome (FW – 8 Int. Points):



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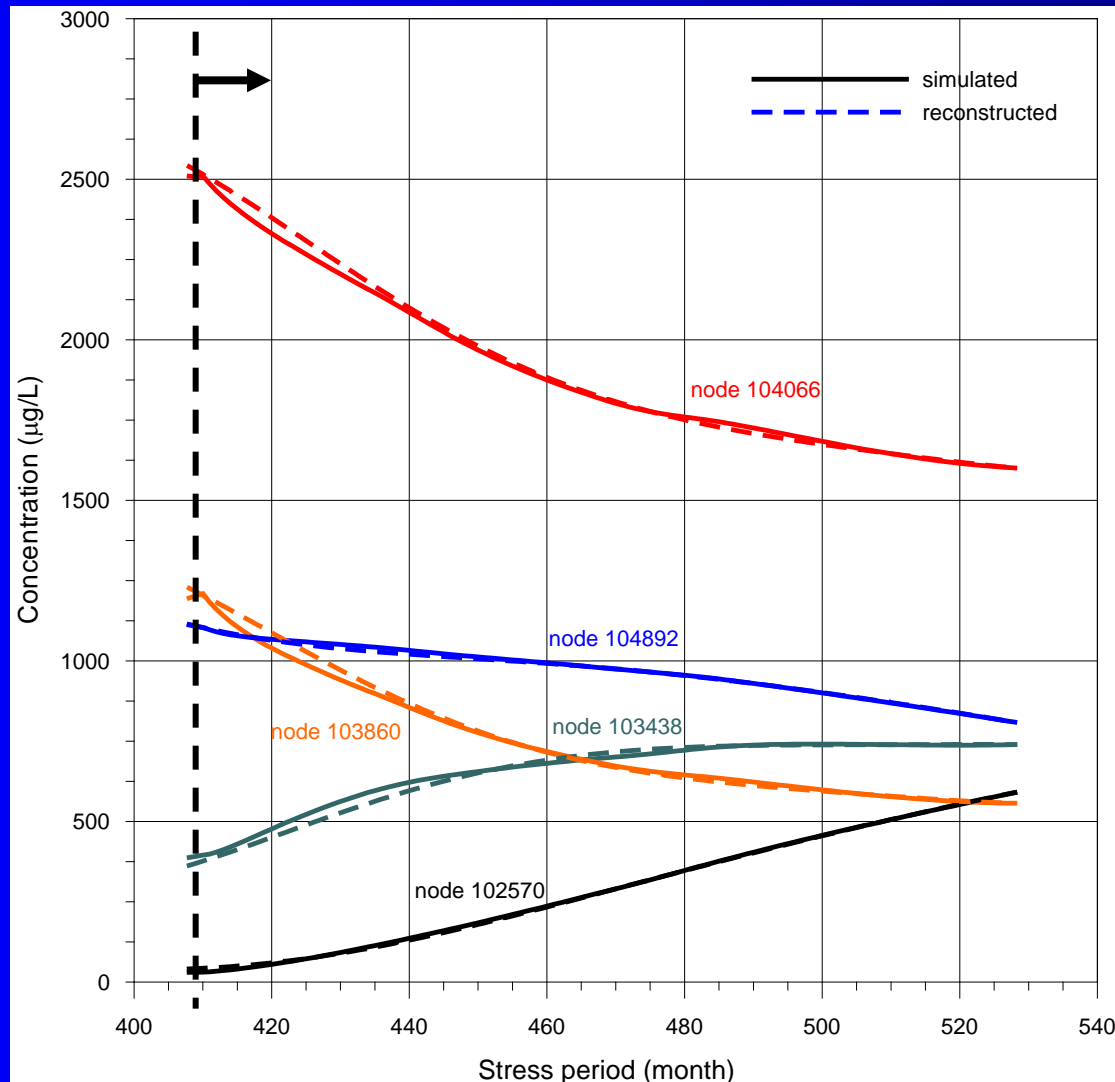


Tarawa Terrace Outcome (FW – 15 Int. Points):



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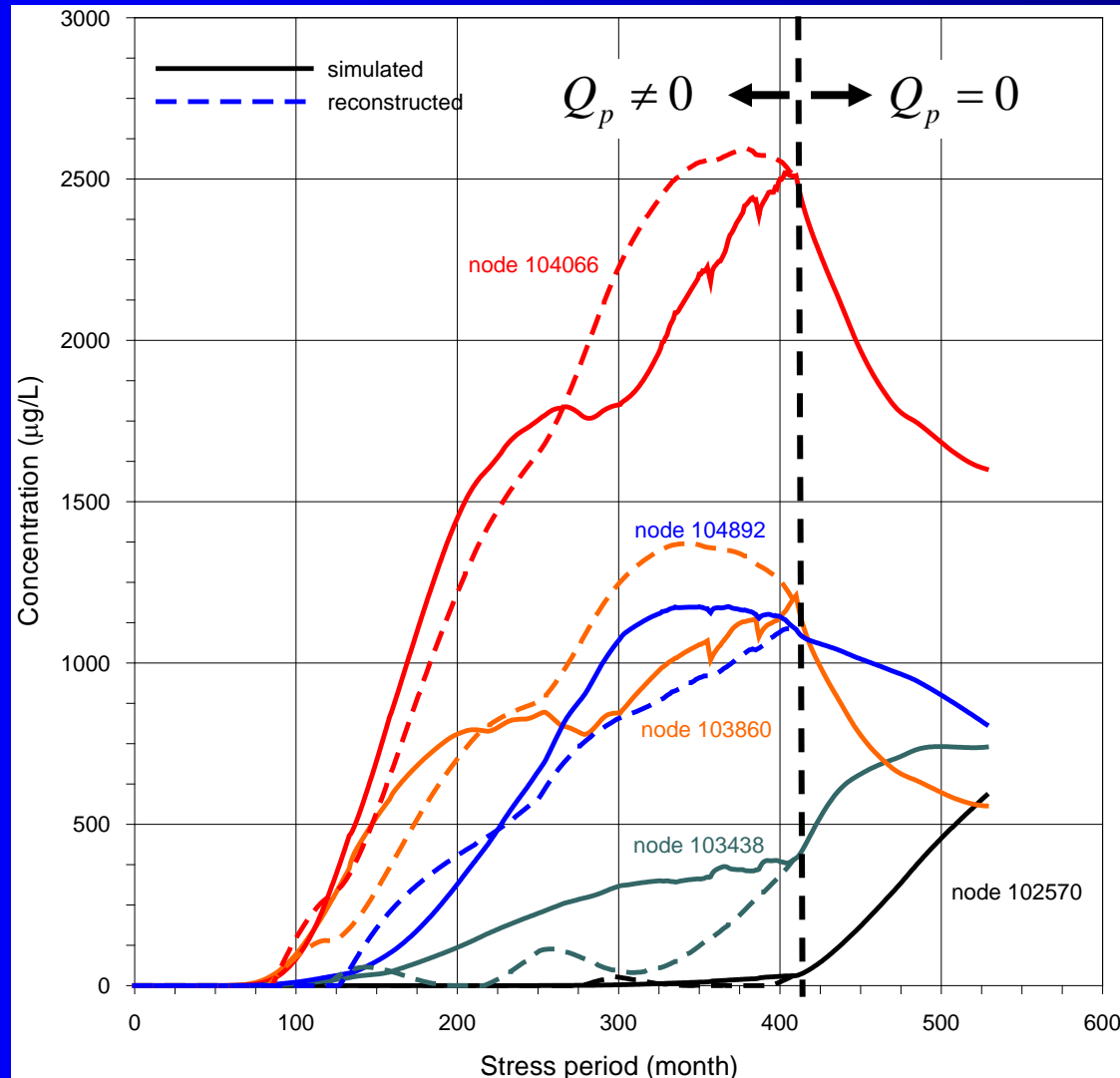
Tarawa Terrace Outcome (BW):



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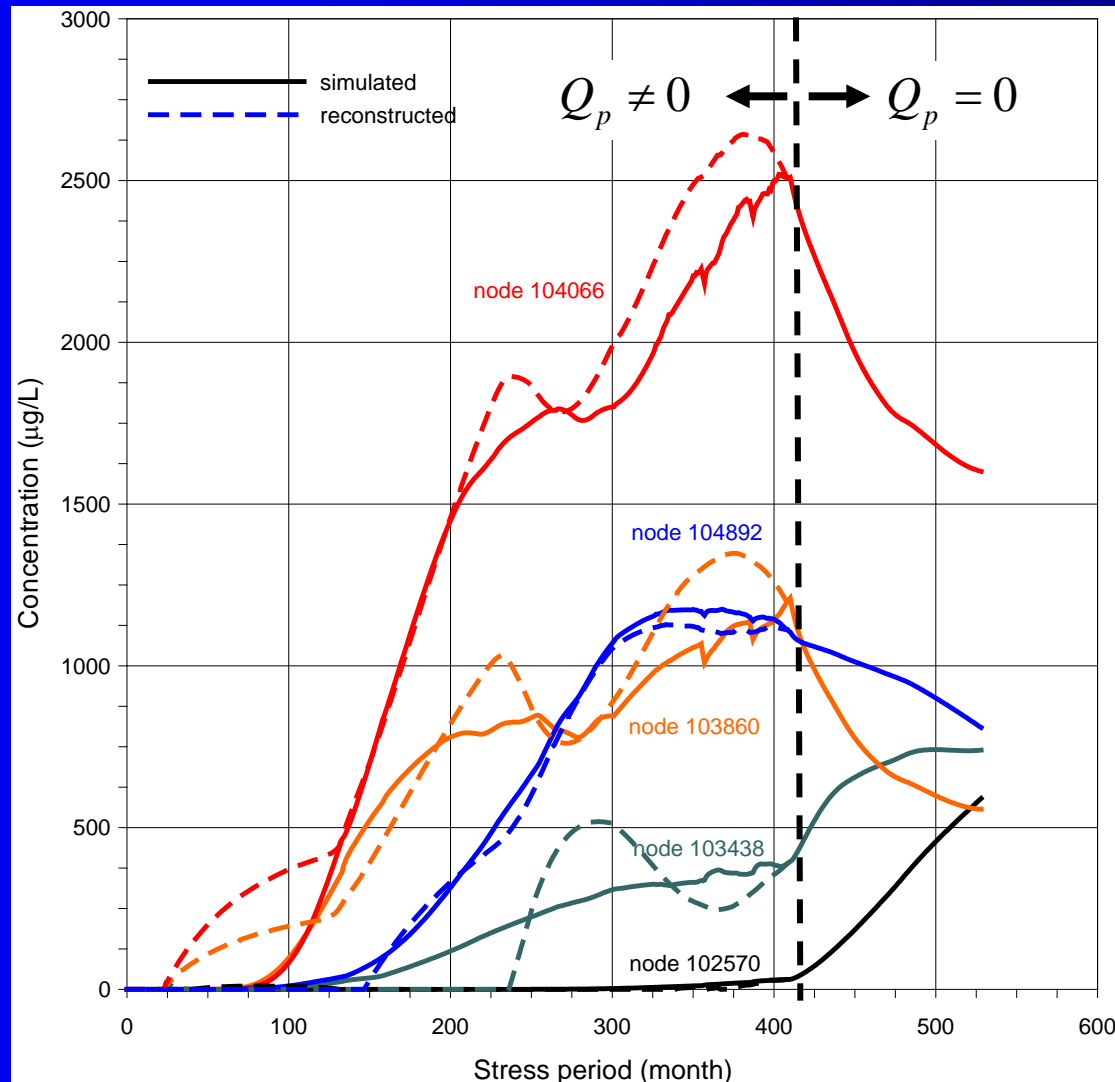
Tarawa Terrace Outcome (BW – 0 Int. Points):



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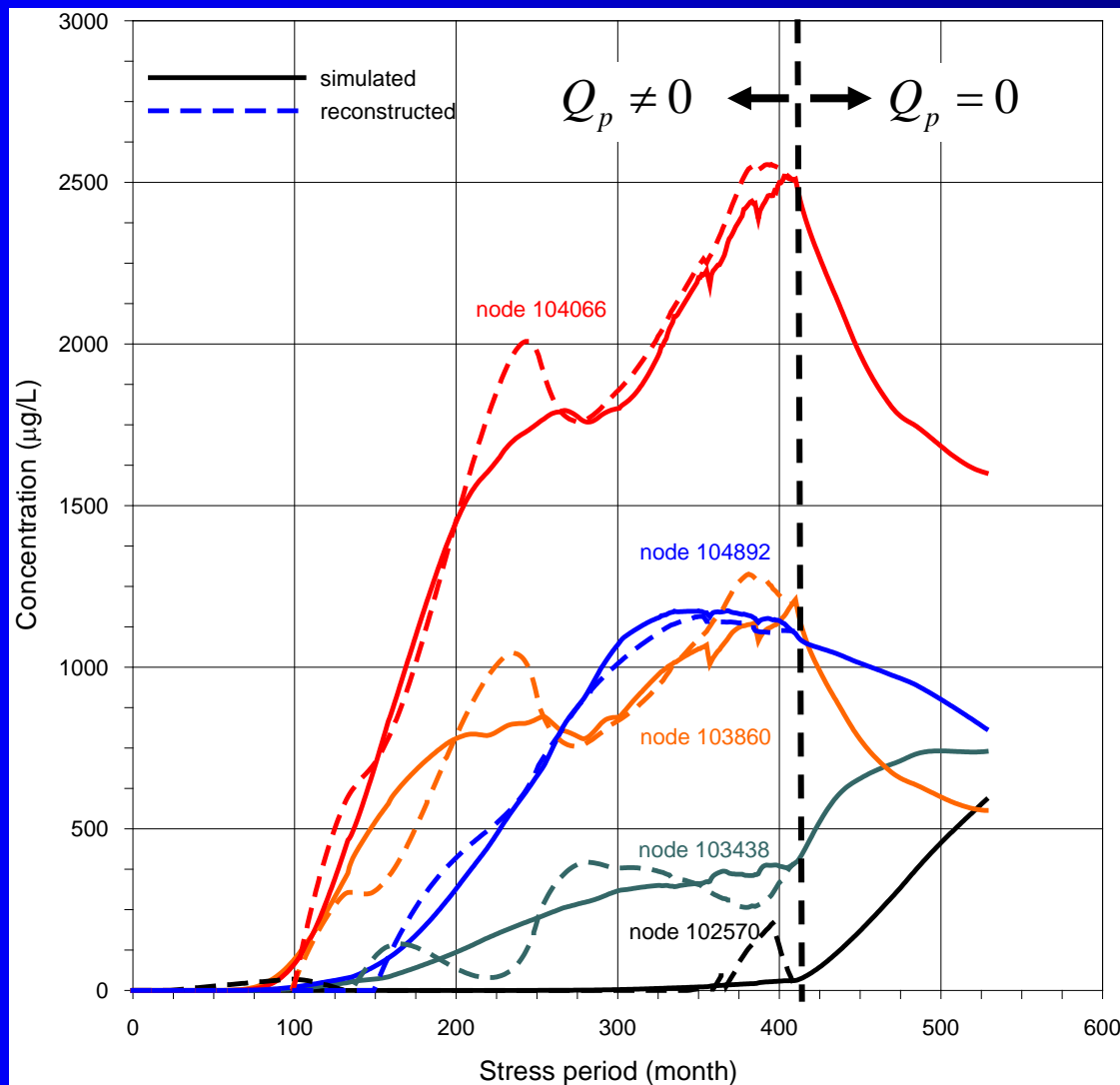
Tarawa Terrace Outcome (BW – 8 Int. Points):



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Tarawa Terrace Outcome (BW – 15 Int. Points):



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Extended procedures:

- **The use of FW and BW procedures iteratively to improve on solution;**
- **Introduction of Kalman filtering method to evaluate the effect of data and computational algorithm error on the solution and establish confidence bands on the solutions obtained; and,**
- **Application of the method to Hadnot Point aquifers.**



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